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XVIII. Contributions to Terrestrial Magnetism.—No. VIII. By Lieut.-Colonel Edward Sabine, R.A., For. Sec. R.S.

Received June 15,—Read June 18, 1846.

Containing a Magnetic Survey of the Southern Hemisphere between the Meridians of 0° and 125° East, and Parallels of -20° and -70°.

THE Antarctic Expedition, under Captain Sir James Clark Ross, R.N., has furnished the materials for maps of the three magnetic elements in the high latitudes of the southern hemisphere for nearly two-thirds of its circumference. The first and second portions of the results, comprising between the meridians of 125° and 300°, have already been communicated to the Royal Society, and are contained in the Vth and VIth Numbers of these Contributions*; a third portion, comprehending between the meridians of 300° and 360°, is in preparation and will shortly be laid before the Society. In order to complete the magnetic survey of the high latitudes of the southern hemisphere as far as they are accessible, there remained the portion between the longitudes of 0° and 125°, or thereabouts. The tracks of vessels in the employ of the enterprising merchants, the Messrs. Enderby, had shown that no difficulties of serious importance obstructed the navigation of the ocean in the vicinity of the Antarctic Circle between the meridians specified: and there appeared to be little reason to doubt, that a vessel, despatched from the Cape of Good Hope, might accomplish this remaining portion of the survey in a single season, without encountering any particular risk.

Lieut. CLERK, of the Royal Artillery, had been attached by Lord VIVIAN, Master-General of the Ordnance, to the Magnetic Observatory at the Cape of Good Hope, with the express view of being engaged in a magnetic survey, either of the colony itself, or of such portion of the globe as might be conveniently accessible from it; and on his passage from England to the Cape had had an opportunity of practising with the instruments employed in a magnetic survey conducted on the ocean. The completion of the survey of the high latitudes appeared the most important service which Lieut. Clerk could render to magnetical science; and on its being proposed to him, he most readily undertook it.

In June 1844 the subject was brought under the consideration of the Committee of Physics of the Royal Society, by a letter from myself to Sir John F. W. Herschel, Bart., Chairman of the Committee, accompanied by one addressed by Sir John Herschel to the Committee, expressing his earnest hope that the measures suggested for the

^{*} Philosophical Transactions, 1843, Art. X., and 1844, Art. VII.

completion of the survey might receive the attention which they appeared to him to merit. These letters were submitted by the Committee to the Council of the Royal Society, with a recommendation that an application should be made by the President and Council to the Lords Commissioners of the Admiralty, to authorize the completion of the southern survey in the manner suggested.

The Board of Admiralty having been pleased to accede to this request, the "Pagoda," a bark of 360 tons, was hired at the Cape of Good Hope by the Admiral commanding on the station, and was fitted for a voyage of some months duration, receiving a complement of four officers and thirty-eight seamen from the flag-ship. Lieut. T. E. L. Moore, of the Royal Navy, who had been one of the officers of Her Majesty's ship Terror in the Antarctic Expedition, and was consequently accustomed to the navigation of the high latitudes, as well as practised in magnetic observations, (having taken a very prominent share in those of Her Majesty's ship Terror, recorded in Nos. V. and VI. of these Contributions,) was selected to command the Pagoda, and instructed to cooperate with Lieut. Clerk, and to give him every assistance and support in the execution of the service on which they were jointly employed. At the time of his appointment, Lieut. Moore was serving in the Caledonia at Lisbon, and some little delay occurred in his recall, and also in his subsequent departure from England, in consequence of which he did not join the Pagoda at the Cape until the 4th of January, when she had been some days ready for sea.

It may be useful to officers desirous of making magnetic observations on board ship, to be acquainted with the precautions which, at the period in question, were deemed desirable for the employment of magnetic instruments on board ship under the most advantageous conditions, and for eliminating the disturbing effects of the ship's iron: a copy of the instructions with which Lieut. Clerk was furnished is therefore subjoined:—

Instructions for Lieut. H. Clerk, R.A., on points connected with the Magnetic Observations on Board Ship.

"1. Influence of the Ship's Iron.—Before the ship is fitted, you had better select, in concert with the naval officer appointed to command her, suitable positions for the standard compass and for your Fox. They should both be on the midship line of the ship; the standard compass sufficiently high to see well over the bulwarks when taking azimuths: the Fox lower for the sake of steadiness: it is generally found convenient to use the Fox a few feet in front of the standard. When the positions have been chosen, have any iron that may be near them removed, (as far as can conveniently be done,) and do not let any fresh iron be placed within at least six feet of either of them.

"When the ship is perfectly ready for sea, take a day for the determination of the effect of the ship's iron on the standard compass. You are already acquainted with the usual process of doing this, and are furnished with the printed instructions issued

by the Admiralty; therefore I do not enter into further details on this point, except to suggest that you should be particularly careful that the ship's boats, davits, &c. are all in the positions they will occupy at sea; and that it will be quite sufficient for your purpose that the deviation should be tried on the sixteen principal points of the compass, instead of on thirty-two, as is sometimes done.

"2. Whilst engaged with the standard compass, have a second compass, of which the compass error (meaning thereby the index error) is known, placed in the gimball table of your Fox, and observe generally (by means of the lubber-line) whether the effect of the ship's iron is nearly the same at the two positions, viz. at the position of the standard compass and at that of the Fox. Observe particularly whether the points of no deviation are the same. It simplifies matters greatly that they should be so, and that at both positions the points of no deviation should be nearly the north and south points. This they will most probably be in a vessel which will not have much iron near either position; but it will be advantageous, when first choosing the positions, to try roughly,—by means of a couple of compasses, one in the proposed position of the standard compass, and the other in that of the Fox,—whether they point alike when the ship's head is either north or south. By interchanging the compasses in these positions, you will prevent any deception which might arise from compass errors.

"The observations which have been described will give you the value of the constants a and b, for the corrections of all the declinations observed on board throughout the voyage, and you will probably find that they will give you work enough for one day.

"3. I shall suppose therefore that you take a second day for the determination of the four constants at the position of the Fox. For this you will require the inclination and intensity with the ship's head on the same sixteen points as before, employing a deflector for the intensity on this occasion, in preference to weights, as more convenient. You will find of course that the points of no deviation with the compass become the points of extreme deviation of the inclination and intensity; for convenience I shall suppose them north and south points. Having completed the observations with the Fox, remove it and observe the horizontal intensity with the head successively north, east, south and west, and north again*, placing the apparatus for the horizontal intensity on the gimball stand of the Fox. This will give you a and b for that position more satisfactorily than the observations of the Fox; from these latter, with the shore observations, you will have c and d.

"The formulæ applicable to all the proceedings which have been described, will be found in Mr. Smith's Memorandum in No. V. of the Contributions to Terrestrial Magnetism. But besides the induced magnetism to which these formulæ refer, the

^{* &}quot;These are compass points, the compass being supposed in strictness to be placed on the spot of the gimball table; if a compass placed at this spot has been found to agree with the standard compass, the latter gives directly the required azimuth of the ship's head."

iron of a ship is found sometimes to exercise upon its compasses a magnetic influence of a distinct character, to which it may become in some instances desirable to give a separate consideration. This influence may be either from permanent magnetism strictly so called, or from a polarity which is temporarily retained, and undergoes alterations consequent upon changes in the inducing action in which it originated, but following after them at a greater or less interval of time. This additional magnetic force may be represented by additional symbols, P, Q and R, i. e. the force resolved along the principal section of the ship, transversely to it, and in the vertical direction.

"The alterations which the introduction of this force makes in Mr. Smith's formula are stated in a second memorandum now printing in No. VI. of the Contributions, a copy of which will be in your hands before you sail.

"This memorandum furnishes equations by which all the constants may be determined by observations in different magnetic latitudes,—of the horizontal force on the *four* principal points,—and of the dip on the *two* principal, together with the dip and horizontal force observed on shore or on the ice. These are part of the observations already directed.

- "4. The observations described in No. 3 must be repeated on the return to the Cape at the conclusion of the voyage, before any change has been made in the iron of the ship. If polarity due to the inducing action of a higher magnetic latitude has been retained, the observations on the return will be found to differ from those made before you sailed. If the disturbing influence of the ship's iron be solely the effect either of instantly induced magnetism, or of permanent magnetism strictly so called, the observations will agree with those made before the departure of the vessel.
- "5. If in the course of the voyage you should anchor in any port in a high latitude, at Enderby's Land for example, or at the Adelie Land of d'Urville, it will be extremely desirable to repeat the same observations. Whenever a choice exists between the shore and fixed ice, as a place for observation out of the influence of the ship's iron, always prefer the fixed ice.
- "6. The approximate value of a, the most important of the constants, may be obtained on board at any time during the voyage when the weather is sufficiently favourable, by azimuths at the north or south points and at the east or west points for the position of the standard compass, and by the horizontal intensity observed on the north and south points for the position of the Fox. If Hansteen's needles are used for the latter purpose, and n, s, be the number of vibrations at north and south in a certain time, commencing at the same arc, and performed in a nearly uniform temperature, then $\frac{n}{s} = \tan \lambda$, and $\cos 2 \lambda = a \tan \theta$; also if $\Delta =$ the deviation when $\zeta' = 90^{\circ}$,

$$\Delta = 90^{\circ} - 2\lambda$$
.

[&]quot;7. The horizontal intensity at the north and south points should be observed on

board frequently; those on the north, south, east and west points, occasionally; and the dip and horizontal intensity on shore or on the ice, with corresponding observations on board, as often as possible.

"8. Index Correction.—The most convenient mode of employing Mr. Fox's apparatus at sea being to use it with the face of the circle in one direction only (i. e. east or west, I shall here assume it east), the index correction with the face east must be sought, by a comparison of the Inclinations observed in that position of the instrument on shore and on fixed ice, with the true Inclinations determined with needles whose poles may be reversed and a complete observation made with them. As the index correction is liable to vary as a function of the Inclination, it should be determined in different Inclinations, and for this purpose it will be desirable to obtain at least one determination in a high latitude.

"When observing on shore or on the ice for the index correction with the face east, do not omit to observe with the face west also, as the mean index correction is useful in showing the kind of separation which exists between the centre of gravity and the point of suspension in the needle for which it is determined. Mr. Fox's apparatus is furnished with three needles; one to be used when the poles are required to be reversed; the magnetism of the other two should be preserved from change if possible; it has been found a convenient practice to employ one of the latter always as the mounted needle, and the other as a deflector.

"9. Comparison of the Weights and Deflectors.—Experience has shown that the intensity may be more conveniently and satisfactorily determined on board ship by the use of deflectors than by constant weights.

"It is necessary however that the 'equivalent weights' of the deflectors employed should be carefully ascertained. Besides the table which you will form for this purpose in the manner practised by Mr. Fox, it will be necessary to have comparisons between the angles of deflection produced by the deflectors and the constant weights at the Cape before and after the voyage, and on any opportunity which you may have in a high latitude either on shore or on the ice. You may also get occasional comparisons on board in very favourable weather.

"In the choice of constant weights to be employed during the voyage, use none that give a less angle of deflection than 15°. In the observations at the Cape, as your base station, make a double series (i. e. the same observations repeated on two separate days) both before and after the voyage.

"10. Azimuths.—You will find it a convenient practice to deduce your azimuths from the hour angle, instead of from the altitude, which is the more usual custom. First take the altitudes which will give you the hour angle corresponding to the time by chronometer (at least until you materially change your geographical position); and as soon as you have completed this observation, take the sun's azimuth, noting the time of observation by chronometer; the hour angle will then give you the true azimuth. Blank forms are sent suited to this mode of observation.

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- "11. General Remarks.—You cannot do better than follow the admirable example of the Antarctic Expedition, in observing the three magnetic elements on board every day on which the weather will permit you to use the instruments.
- "12. Frequent reference has been made in these instructions to the importance of at least one opportunity of observing on shore or on the ice in a high latitude, for various objects connected with the reduction and correction of the whole body of magnetic observations made during the voyage. If Enderby's Land, or land connected with it, should not be accessible, it is by no means necessary that the ship should *enter* the ice in order to give you the opportunity of landing on a piece of ice of sufficient magnitude. A favourable day being chosen, she may approach the ice sufficiently near, and remain four or five hours, whilst her boat takes you to make the observations and to return.

"If the ice be not 'fixed' you must be careful to detect an azimuthal motion, should there be any, by which the inclination circle might otherwise be removed from the plane of the magnetic meridian without your being aware of it. You will also take care that the magnetic instruments are sufficiently distant from the boat.

"EDWARD SABINE."

" Woolwich."

The Pagoda sailed from the Cape of Good Hope on the 9th of January, proceeding, pursuant to instructions, towards the Antarctic Circle in the meridian of Greenwich. She crossed the 60th parallel in the longitude of 4° east, and being impeded by ice in her direct progress to the southward, coasted its margin to the south-east, and attained her greatest southing on the 10th of February in latitude -68° 10' and longitude 35°. She was then according to the chart in the vicinity of the western extremity of Enderby's Land, but from strong south-east gales and the position of the ice was unable to approach it sufficiently even to see the land: from thence she continued a general progress to the eastward, keeping in as high a parallel as the ice and weather permitted. On the 10th of March she had obtained the 96th degree of east longitude in about the 60th degree of latitude, when the season was considered to be so far advanced that it would not be prudent to persevere in the completion of the survey in the high latitudes; and a course was therefore taken for King George's Sound in Australia, where the ship arrived on the 1st of April. During the whole of this voyage observations of the three magnetic elements were made twice in each day, except in extreme circumstances of weather, by Lieut. Moore in the afternoon and Lieut. CLERK in the forenoon, each being furnished with a separate (Fox's) apparatus for the Inclination and Force; and on the arrival of the ship at King George's Sound, the two instruments were found to give an almost identical value for the intensity of the force, the results being by Lieut. Moore's Fox 1.680, and by Lieut. CLERK's 1.688.

After remaining a sufficient time to examine the index and other corrections of the instruments, and to obtain the necessary data for eliminating the effects of the ship's iron on the magnetic results obtained during the voyage, the Pagoda quitted King George's Sound on the 27th of April and returned to the Cape of Good Hope, touching at Mauritius by the way for the purpose of repeating the observations on the influence of the ship's iron. She arrived at the Cape on the 20th of June, having continued the practice of observing the magnetic elements daily on the return passage, in the same manner as in the high latitudes.

The voyage was performed without accident or loss of life, and the crew returned in perfect health, due doubtless in great degree to the supplies of warm clothing and preserved meats, which, by direction of the Admiralty, Lieut. Moore had taken with him from England.

No failure occurred in any of the instruments notwithstanding the continual use in which they were kept by the zeal of the observers. If where so much was so well accomplished it is permissible to feel or to express regret on any account, it can be only that circumstances should have prevented the completion of the survey in the high latitudes as far as the 125th degree of longitude according to the original design, whereby the observations of the magnetic force would have been carried up to the principal axis of the isodynamic oval of 2.00.

On the conclusion of the voyage Lieut. CLERK received directions from the Master-General of the Ordnance to return to Woolwich, for the purpose of completing the reduction of his own observations and those of Lieut. Moore. The following pages contain Lieut. CLERK's report; in which he has also embodied a series of observations on the Inclination and Force with a Fox's apparatus, made in 1844 by Lieut. ALEX-ANDER SMITH, R.N., one of the Assistants at the Hobarton Magnetic Observatory, on his passage to Van Diemen Island; and a second series, also of the Inclination and Force, made in 1845 by Lieut. DAYMAN, R.N., of the same observatory, in a passage in the bark "Leander" from Hobarton to the Cape. Both these officers had previously been employed in the Antarctic Expedition under Sir James Clark Ross, and their observations now communicated are a consequence of the zeal which they imbibed, and the practice in the use of instruments which they acquired, in that expedition. Their observations transmitted to the Admiralty were sent to Woolwich for reduction and publication. Lieut. CLERK has also embodied in his report the determinations of the three magnetic elements made by Sir James Ross in the Erebus in 1840 on her passage from the Cape of Good Hope to Kerguelen Island, and thence to Hobarton.

On inspecting the map, it will be seen that the tracks of the Erebus and Prince Regent held about a middle line between the outward and homeward tracks of the Pagoda, and are therefore extremely useful in connecting results which would otherwise have been somewhat too far apart.

Lieut. CLERK has taken the Cape of Good Hope as the base station of the observations of the magnetic force made in the Pagoda. The determinations of the absolute horizontal force made at the observatory at the Cape in February, March, April and May 1845 (page 362 in seq.), which are the last received from that station, give a mean result of 4.482, the mean inclination during the same month being -53° 25'.5. Combining these with the determination at Woolwich in No. VII. of these Contributions *, we have the total force at the Cape in the arbitrary scale 0.993. The ratios determined by Mr. Fox's statical apparatus (page 363 in seq.) by separate needles are 1.000 and 1.006: the value of the total force at the Cape as a base station for the observations of the Pagoda has therefore been taken as 1.000.

As Lieut. Smith did not touch at the Cape on his passage to Hobarton, and as the needle which Lieut. Dayman had employed on his homeward passage was broken at the Cape before observations had been made with it, and consequently before the series between Hobarton and the Cape could be connected with the latter station, it has been necessary to employ Hobarton as the base station of both these series. I have already stated in Nos. V. and VI. of these Contributions, the results of the observations which were made to determine the absolute horizontal force at Hobarton between 1840 and 1844; viz. by Sir James C. Ross in 1840 and 1841, with magnets of fifteen inches in length †; by Lieut. Kay in 1841 and 1842, with magnets of the same length; by Lieut. Kay in 1844 with magnets of twelve inches, and with others of 9·18 and 7·50 inches. I have now to add the results of twenty-four determinations made by Lieut. Kay between November 1844 and September 1845, with magnets of various lengths, as shown in the following table:—

Magnets and	Magnets and their length.		No. of	Horizontal			
Suspended.	Deflecting.	Date.	distances.	force.			
in.	in.	,					
 7·50	9.18	Nov. 7, 1844.	3	4.5108			
 7·50	9.18	Sept. 9, 1845.	3	4.4810			
A 57 3.00	D xv. 3.67	Dec. 7, 1844.	3	4.5316			
A 57 3.00	D xv. 3.67	Dec. 9, 1844.	5	4.5118			
A 57 3.00	D xv. 3.67	Dec. 11, 1844.	5	4.4954			
A 57 3.00	D xv. 3.67	Jan. 12, 1845.	5	4.5058			
A 57 3.00	D xv. 3-67	May 5, 1845.	3	4.4997			
A 57 3.00	D xv. 3.67	Aug. 15, 1845.	5	4.4762			
A 57 3.00	D 9 3.67	Aug. 19, 1845.	5	4.5104			
A 57 3.00	D 9 3-67	May 6, 1845.	3	4.5076			
A 57 3-00	A 19 3.02	Aug. 20, 1845.	5	4.4905			
A 52 3.00	D xvi. 3.67	Jan. 19, 1845.	3	4.4940			
R 1 3.00	D xvi. 3.67	Aug. 28, 1845.	4	4.4970			
I 12 2.45	A 19 3-00	Dec. 13, 1844.	5	4.4954			
I 12 2.45	A 19 3.00	Dec. 13, 1844.	5	4.4899			
I 12 2.45	A 19 3.00	Dec. 15, 1844.	5	4.4865			
I 12 2.45	A 19 3.00	Jan. 14, 1845.	5	4.4809			
I 12 2.45	A 29 3.00	Aug. 26, 1845.	5	4.5016			
I 12 2.45	A 23 3.00	Aug. 22, 1845.	5	4.4994			
I 1 2.45	A 23 3.00	Dec. 20, 1844.	3	4.5046			
I 1 2.45	A 23 3.00	Dec. 23, 1844.	3	4.5121			
I 1 2.45	A 23 3.00	Dec. 26, 1844.	5	4.5020			
I 1 2.45	A 23 3.00	Jan. 15, 1845.	5	4.5082			
Î 1 2·45	A 23 3-00	May 9, 1845.	3	4.4970			
Mean							

^{*} Philosophical Transactions, 1846, p. 246.

[‡] Ibid. p. 168 (note).

[§] Ibid. 1844, p. 111.

[†] Ibid. 1843, p. 168.

[|] Ibid. p. 112.

Collecting in one view the different mean results, we have

Ross, in 1840-41, 15 in. magnets		•			•	•			•		4.573
KAY, in 1841, 15 in. magnets .		•					•		•	•	4.553
KAY, in 1842, 15 in. magnets .						•	•			•	4.513
KAY, in 1843, 12 in. magnets .				•				•	٠		4.520
Kay, in 1843, 9.18 and 7.50 in. ma	agr	nets	3	•		•	•		•		4.501
Kay, in 1844-45, magnets of vario	us	len	gth	s,	9.1	8 t	o 2	2.45	in		4.499

These results exhibit (with one exception) a progressive decrease, but between those of 1840-41, and subsequent years, there is a very great difference. The inclination has decreased from -70° 40'·7, observed in 1840-41*, to -70° 37'·6, which is the mean of the results obtained twice in each week at the Hobarton Observatory in the first nine months of 1845. Assuming the total force at Hobarton as constant, the horizontal component should have been increased rather than diminished by the small secular change which appears to have taken place in the Inclination. discrepancy between the earlier and later results of the absolute determinations cannot therefore be a consequence of secular change in the Inclination; nor is it probable that the total force should have undergone a decrease of such magnitude. Presuming the results of 1840-41, with the 15-inch magnets, to have been affected with error from some cause as yet unexplained, (possibly from an erroneous value having been taken for the moment of inertia of the magnet,) the subsequent results exhibit only such differences as cannot be regarded as excessive. They have all to undergo recalculation, as Lieut. Kay does not consider the elements of reduction as vet finally determined; and they will all, in common with all the other determinations of the absolute horizontal force given in these Contributions, have to receive a small correction for the difference of the magnetic moment of the deflecting bar, caused by the earth's inducing action in the different positions in which the bar is placed in the experiments of deflection and vibration. If, therefore, we assume provisionally the mean of the four last results, or 4.508, as the best approximation to which we have yet arrived for the horizontal component at Hobarton, and $-70^{\circ} 39'$ as the corresponding Inclination, we have the total force in the arbitrary scale 1.797; and we may hence conclude, that influenced by the earlier determinations (those of 1840-41), the provisional value of the total force at Hobarton, employed in the Vth and VIth Numbers of the Contributions (1.82), was taken too high, and that all the values of the force dependent on Hobarton will require a correction to be applied, in amount about -0.02, before they are combined in the general map of the southern hemisphere. For Lieut. Smith's and Lieut. Dayman's observations, Lieut. CLERK has taken a base value of 1.80 at Hobarton.

A subsequent number of these Contributions will contain the Magnetic Observations of the Erebus and Terror in the summer of 1843-1844, between the meridians

^{*} Philosophical Transactions, 1843, p. 165.

of Cape Horn and of the Cape of Good Hope, which will complete the survey of the high latitudes of the southern hemisphere.

I propose then to combine in one general view the several portions of the southern survey which have been successively communicated; and I shall reserve until that occasion, as more convenient than the present, such general remarks as suggest themselves in reference to the magnetic lines determined in the present Number.

"Report on the Magnetic Observations made in Her Majesty's hired bark Pagoda, from January to June 1845, by Lieut. Henry Clerk of the Royal Artillery.

"1. Calculation of Corrections for the Ship's Local Attraction.

"To obtain the corrections for the observations of the Declination, the deviations of the compass were observed on each of the sixteen principal points at the Cape of Good Hope, King George's Sound, the Mauritius, and again at the Cape on the return of the Expedition. The following are the observations:—

J.	Ship's head.	Cape of G	ood Hope.	King George's Sound.	Mauritius.
1	`	January.	June.		
	N. N.N.W. N.W. W.N.W. W.S.W. S.W. S.S.E. E.E. E.N.E. N.E.	0 12+ 0 57+ 0 08- 0 00 0 13- 0 28- 1 28- 1 06- *1 48+ 0 42+ 1 12+ 1 27+ 0 57+ 0 27+ 0 12+ 0 32+	0 20+ Not observed. 0 50+ 0 50- 0 15- 0 30- 1 20- 1 25- 0 18- Not observed. 1 50+ 1 40+ 1 45+ 1 50+ 1 35+ 1 13+	0 15+ 0 00 0 20+ 1 40- 1 40- 1 50- 1 00- 0 15- 0 50+ 0 55+ 2 20+ 3 10+ 2 40+ 3 30+ 2 35+	0 20+ 0 30+ 0 20- 0 30- 0 50- 1 10- 1 10- 0 50- 0 20+ 1 00+ 1 20+ 0 55+ 1 20+ 0 50+ 1 20+ 1 20+

The + sign denotes a deviation of the north end towards the west.

"The values of θ (the Inclination) being as follows, viz.—

Cape of Good Hope . . . $\theta = -5\mathring{3}$ 44 King George's Sound . . $\theta = -65$ 04 Mauritius $\theta = -53$ 56

"From these observations we can obtain the values of a and b by the formulæ in No. V. of the Contributions to Terrestrial Magnetism \uparrow , which give the following values, viz.—

^{*} This observation is evidently erroneous.

⁺ Philosophical Transactions, 1843, Part II. p. 148.

Cape of Good Hope . . .
$$a=.0148$$
 . . . $b=.9848$
King George's Sound . . . $a=.0199$. . . $b=1.0040$
Mauritius $a=.0158$. . . $b=.9907$
Mean . . $a=.0168$. . . $b=.9932$

"The values of a and b can also be obtained by observations of the horizontal intensity on the N., S., E. and W. points alone.

"If the card of the azimuth compass be deflected by another magnet (the small deflectors belonging to the dipping-needle for instance), and if v_n , v_s , v_w , and v_e be the angles of deflection observed on the N., S., W. and E. points respectively, then

$$a \tan \theta = \frac{\csc v_n - \csc v_s}{\csc v_n + \csc v_s}; \quad b = \frac{\csc v_w + \csc v_e}{2 \sqrt{\csc v_w \cdot \csc v_e}}.$$

"The deflections were obtained in this manner at the Cape of Good Hope, and at King George's Sound on the N. and S. points, viz.—

Cape of Good Hope.	King George's Sound.
At N. the deflection $=16^{\circ} 20$	At N. the deflection $\cdot = 15^{\circ} 23^{\circ}$
At S = 15 35	At S = $14 06$
Hence $a = \frac{1}{0168}$	And $a = 0198$

Agreeing very closely with the values determined above.

"After an inspection of the observations at the several stations, Mr. Archibald Smith has kindly furnished the following Memorandum.

- "'The formulæ for the correction of observations of magnetic declination, made on board ship, given in the Vth and VIth numbers of the Contributions, are deduced on the supposition that the soft iron of the ship is symmetrically distributed on each side of the fore and aft vertical section passing through the compass. The deviations observed in the Pagoda by Lieut. Clerk, seem to show that the soft iron was not so distributed in that vessel, and to require for their correction formulæ in which no supposition is made as to the distribution of the iron of the vessel, except that there is no iron very near the compass.
- "'Using the notation of the memorandums in Nos. V. and VI. of the Contributions, let φ represent the total magnetic force of the earth at the place of observation, θ the inclination, ζ the azimuth of the ship's head, reckoning from (magnetic) north to west, and let φ' , θ' , ζ' represent the values of the same quantities, shown by an instrument placed at a fixed position in the vessel, and affected by the attraction of the iron in the vessel.
- "'The first three equations in the memorandum in Contribution No. VI. may be transformed into the following, viz.—

$$\varphi \cos \theta \cos \zeta = \varphi' \cos \theta' \{A' \cos \zeta' + B' \sin \zeta'\} + \varphi' \sin \theta' C' + P'. \qquad (1.)$$

$$\varphi \cos \theta \sin \zeta = \varphi' \cos \theta' \{ D' \cos \zeta' + E' \sin \zeta' \} + \varphi' \sin \theta' F' + Q'. \qquad (2.)$$

$$\varphi \sin \theta = \varphi' \cos \theta' \{G' \cos \zeta' + H' \sin \zeta'\} + \varphi' \sin \theta' K' + R'. \qquad (3.)$$

"'The coefficients A'B'...R' might, if required, be expressed in terms of the corresponding coefficients of Contribution No. VI. It is here however only important to observe that A'B'C'D'E'F'G'H'K' depend only on the amount and distribution of the soft iron. P'Q'R' depend partly on the amount and distribution of the soft iron, and partly on the amount and distribution of the permanently magnetic iron, and become zero when there is no permanently magnetic iron. If the soft iron is symmetrically distributed on each side of the fore and aft vertical section passing through the compass, B'D'F'H' are equal to zero.

"The above equations are deduced, it must be remembered, on the hypothesis that the soft iron of the vessel receives its full charge of induced magnetism instantly on the vessel assuming a new position, and that the rest of the iron in the vessel is in a permanently magnetic state. On this hypothesis, and supposing that no iron is very near the compass, the equations are accurate, and the coefficients A' B', &c. are constant, and independent of the latitudes. The hypothesis is however evidently not strictly true. The magnetic state of the hard, if not of the soft iron of the vessel, changes with a change of position and with time. In consequence of this, different values of the coefficients are derived from observations made at different places, and at the same place at different times.

"'Careful observations, made in a variety of circumstances and localities, and particularly, (for a reason which will appear in a subsequent part of this Memorandum,) observations made near the line of no dip, when the affected dip is zero, may hereafter throw light on the nature of the change which takes place in the magnetic state of a vessel, and furnish the means of determining the change which the coefficients undergo. In the present Memorandum they are supposed to be constant.

"'From equations (1.) and (2.) the following may be deduced:

$$\sin (\zeta - \zeta') = \frac{\varphi' \cos \theta'}{\varphi \cos \theta} \left\{ \frac{D' - B'}{2} - \frac{A' - E'}{2} \sin 2\zeta' + \frac{B' + D'}{2} \cos 2\zeta' \right\} \\
- \frac{\varphi' \sin \theta' C' + P'}{\varphi \cos \theta} \sin \zeta' + \frac{\varphi' \sin \theta' F' + Q'}{\varphi \cos \theta} \cos \zeta'$$
(4.)

"'This equation is rigorously accurate, on the assumptions which have been made. If $\varphi' \cos \theta'$ and $\varphi' \sin \theta'$ were known in terms of φ , θ and ζ' , and the coefficients determined by observation, this equation would furnish accurate corrections for observations of Declination. The expression is very much simplified if we may assume $\theta'=\theta$, and $\varphi'=\varphi$. This assumption may I believe in general be safely made, except in high magnetic latitudes. Making this assumption, we have the following approximate formula,

$$\sin(\zeta - \zeta') = \frac{D' - B'}{2} - \left\{ C' \tan \theta + \frac{P'}{\varphi \cos \theta} \right\} \sin \zeta' + \left\{ F' \tan \theta + \frac{Q'}{\varphi \cos \theta} \right\} \cos \zeta'$$

$$- \frac{A' - E'}{2} \sin 2 \zeta' + \frac{B' + D'}{2} \cos 2 \zeta'$$
(5.)

"This equation may conveniently be put under the form $\sin \delta = A + B \sin \zeta' + C \cos \zeta' + D \sin 2\zeta' + E \cos 2\zeta'$ (6.)

 $\delta = \zeta - \zeta'$ is the deviation of the compass; B corresponds to the coefficient a tan θ of the former memorandum; D to the coefficient 1-b. A, B, C, D, E are coefficients, which are to be determined by observations of deviation made with the ship's head on different azimuths. A, D and E, it will be seen, are independent of the dip, and, to the extent to which the hypothesis above mentioned is correct, will have the same values in different latitudes. B and C depend on the dip, and also on the proportion of the soft to the permanently magnetic iron. This ratio cannot be determined from observations made in one place. If P', Q', C', F' remain constant, they can severally be determined from values of B and C deduced in two different latitudes, and the values of B and C in any other latitude may be deduced from the equations

$$\mathbf{B} = -\left\{ \mathbf{C}' \tan \theta + \frac{\mathbf{P}'}{\varphi \cos \theta} \right\} \dots (7.) \qquad \mathbf{C} = \mathbf{F}' \tan \theta + \frac{\mathbf{Q}'}{\varphi \cos \theta} \dots (8.)$$

the accurate values of B and C being

$$\mathbf{B} = -\frac{\varphi' \sin \theta' \mathbf{C}' + \mathbf{P}'}{\varphi \cos \theta'}, \qquad \mathbf{C} = \frac{\varphi' \sin \theta' \mathbf{F}' + \mathbf{Q}'}{\varphi \cos \theta}.$$

If the affected dip is zero, we have

$$R = -\frac{P'}{\phi}, \qquad C = \frac{Q'}{\phi}.$$

So that from observations on the line of no dip, or more accurately when the affected dip is zero, the effect of the permanent magnetism may be obtained.

"'If we distinguish the points of the compass, reckoning from north to west, by the numbers from 1 to 32, north being 0 or 32, and north by west being 1; and if we designate by δ_0 , δ_1 , &c. the westerly deviation when the ship's head is north, or north by west, &c., so that δ_8 represents the deviation at W., δ_{16} at S., δ_{24} at E., it is evident from the equations that we have at once the following simple expressions for the values of the coefficients:—

$$A = \frac{1}{4} \left\{ \sin \delta_0 + \sin \delta_8 + \sin \delta_{16} + \sin \delta_{24} \right\}. \qquad (9.)$$

$$C = \frac{1}{2} \left\{ \sin \delta_0 - \sin \delta_{16} \right\}. \qquad (11.)$$

$$D = \frac{1}{4} \left\{ \sin \delta_4 - \sin \delta_{12} + \sin \delta_{20} - \sin \delta_{28} \right\}. \quad . \quad . \quad . \quad (12.)$$

$$E = \frac{1}{4} \left\{ \sin \delta_0 - \sin \delta_8 + \sin \delta_{16} - \sin \delta_{24} \right\}. \quad . \quad . \quad . \quad . \quad (13.)$$

- "' More accurate values of the coefficients may be obtained by combining observations of deviation, made with the ship's head on the several points, in the following manner:—
- "'1. Suppose the deviation to have been observed on all the thirty-two points. Let MDCCCXLVI. 2 z

 $\zeta'_1, \zeta'_2, \ldots, \zeta'_{32}$ be the observed azimuths, which of course are 11° 15′, 22° 30′, &c. Then we have

$$\sin \delta_{0} = A + C + E$$

$$\sin \delta_{1} = A + B \sin \zeta'_{1} + C \cos \zeta'_{1} + D \sin 2\zeta'_{1} + E \cos 2\zeta'_{1}$$

$$\sin \delta_{2} = A + B \sin \zeta'_{2} + C \cos \zeta'_{2} + D \sin 2\zeta'_{2} + E \cos 2\zeta'_{2}$$

$$&c. &c.$$

$$\sin \delta_{31} = A + B \sin \zeta'_{31} + C \cos \zeta'_{31} + D \sin 2\zeta'_{31} + E \cos 2\zeta'_{31}$$
(14.)

Combining these equations by the method of least squares, we obtain by virtue of a well-known property of circular functions,

$$A = \frac{1}{32} \sum \sin \delta$$

$$B = \frac{1}{16} \sum \sin \delta \sin \zeta'$$

$$C = \frac{1}{16} \sum \sin \delta \cos \zeta'$$

$$D = \frac{1}{16} \sum \sin \delta \sin 2\zeta'$$

$$E = \frac{1}{16} \sum \sin \delta \cos 2\zeta'$$
(15.)

where

$$\Sigma \sin \delta = \sin \delta_0 + \sin \delta_1 \dots + \sin \delta_{31},$$

$$\Sigma \sin \delta \sin \zeta' = \sin \delta_0 \sin \zeta'_0 + \sin \delta_1 \sin \zeta'_1 + \&c. + \sin \delta_{31} \sin \zeta'_{31}$$
&c. &c. &c.

"'If we represent $\sin \delta_0$, $\sin \delta_1$, &c. by s_0 , s_1 , &c., and remember that all the values of $\sin \zeta'$, $\cos \zeta'$, $\sin 2\zeta'$, $\cos 2\zeta'$ which occur in these formulæ can be represented by the quantities s_1 , s_2 , s_3 , s_4 , s_5 , s_6 , s_7 , we shall find

$$\mathbf{C} = \frac{1}{16} \{s_0 - s_{16}\},$$

$$+ \cdot 0613 (\log = \overline{2} \cdot 78745) \{s_1 + s_{31} - s_{15} - s_{17}\},$$

$$+ \cdot 0577 (\log = \overline{2} \cdot 76149) \{s_2 + s_{30} - s_{14} - s_{18}\},$$

$$+ \cdot 0520 (\log = \overline{2} \cdot 71572) \{s_3 + s_{29} - s_{13} - s_{19}\},$$

$$+ \cdot 0442 (\log = \overline{2} \cdot 64536) \{s_4 + s_{28} - s_{12} - s_{20}\},$$

$$+ \cdot 0347 (\log = \overline{2} \cdot 54062) \{s_5 + s_{27} - s_{11} - s_{21}\},$$

$$+ \cdot 0239 (\log = \overline{2} \cdot 37872) \{s_6 + s_{26} - s_{10} - s_{22}\},$$

$$+ \cdot 0122 (1c^{--} = \overline{2} \cdot 08611) \{s_7 + s_{25} - s_9 - s_{23}\}. \qquad (18.)$$

$$\mathbf{D} = \cdot 0577 (\log = \overline{2} \cdot 76149) \{s_1 - s_{31} - s_{15} + s_{17} + s_7 - s_{25} - s_9 + s_{23}\},$$

$$+ \cdot 0442 (\log = \overline{2} \cdot 64536) \{s_2 - s_{30} - s_{14} + s_{18} + s_6 - s_{26} - s_{10} + s_{22}\},$$

$$+ \cdot 0229 (\log = \overline{2} \cdot 37872) \{s_3 - s_{29} - s_{13} + s_{19} + s_5 - s_{27} - s_{11} + s_{21}\},$$

$$+ \frac{1}{16} \{s_4 - s_{28} - s_{12} + s_{20}\}. \qquad (19.)$$

$$\mathbf{E} = \frac{1}{16} \{s_0 + s_{16} - s_8 - s_{24}\},$$

$$+ \cdot 0239 (\log = \overline{2} \cdot 37872) \{s_1 + s_{31} + s_{15} + s_{17} - s_7 - s_{25} - s_9 - s_{23}\},$$

$$+ \cdot 0442 (\log = \overline{2} \cdot 64536) \{s_2 + s_{30} + s_{14} + s_{18} - s_6 - s_{26} - s_{10} - s_{22}\},$$

$$+ \cdot 0442 (\log = \overline{2} \cdot 64536) \{s_2 + s_{30} + s_{14} + s_{18} - s_6 - s_{26} - s_{10} - s_{22}\},$$

$$+ \cdot 0442 (\log = \overline{2} \cdot 64536) \{s_2 + s_{30} + s_{14} + s_{18} - s_6 - s_{26} - s_{10} - s_{22}\},$$

$$+ \cdot 0442 (\log = \overline{2} \cdot 64536) \{s_2 + s_{30} + s_{14} + s_{18} - s_6 - s_{26} - s_{10} - s_{22}\},$$

$$+ \cdot 0577 (\log = \overline{2} \cdot 76149) \{s_3 + s_{29} + s_{13} + s_{19} - s_5 - s_{27} - s_{11} - s_{21}. \qquad (20.)$$

2. Using the deviations observed on the sixteen principal points only, we have

$$A = \frac{1}{16} \{s_0 + s_2 + s_4 \dots + s_{30}\}. \dots (21.)$$

$$B = 0.0478 (\log = \overline{2} \cdot 67975) \{s_2 - s_{30} + s_{14} - s_{18}\},$$

$$+ 0.0884 (\log = \overline{2} \cdot 94639) \{s_4 - s_{28} + s_{12} - s_{20}\},$$

$$+ 1155 (\log = \overline{1} \cdot 06252) \{s_6 - s_{26} + s_{10} - s_{22}\},$$

$$+ \frac{1}{8} \{s_8 - s_{24}\}. \dots (22.)$$

$$C = \frac{1}{8}(s_0 - s_{16}),$$

$$+ \cdot 1155 (\log = \overline{1} \cdot 06252) \{s_2 + s_{30} - s_{14} - s_{18}\},$$

$$+ \cdot 0884 (\log = \overline{2} \cdot 94639) \{s_4 + s_{28} - s_{12} - s_{20}\},$$

$$+ \cdot 0478 (\log = \overline{2} \cdot 67975) \{s_6 + s_{26} - s_{10} - s_{22}\}. \qquad (23.)$$

$$\mathbf{D} = 0884 (\log = \overline{2} \cdot 94639) \{ s_2 - s_{30} - s_{14} + s_{18} + s_6 - s_{26} - s_{10} + s_{22} \},$$

$$+ \frac{1}{8} \{ s_4 - s_{28} - s_{12} + s_{20} \}. \qquad (24.)$$

$$\mathbf{E} = \frac{1}{8} \{ s_0 + s_{16} - s_8 - s_{24} \},$$

$$+ \cdot 0884 \ (\log = \overline{2} \cdot 94639) \{ s_2 + s_{30} + s_{14} + s_{18} - s_6 - s_{10} - s_{22} - s_{26} \}. \tag{25.}$$

"'3. Using the deviations observed on the eight principal points only, we have

"'Having found A, B, C, D, E by any of the above methods, a table of the deviations on all the points may then be computed. The computation will be facilitated by using the following Table:—

"'Let B_1 , B_2 B_7 , C_1 , C_2 C_7 represent the values of B and C multiplied by $\sin 11^{\circ} 15'$, $\sin 22^{\circ} 30'$, and let D_2 , D_4 , D_6 , E_2 , E_4 , E_6 represent the values of D and E multiplied by $\sin 22^{\circ} 30'$, $\sin 45^{\circ}$, and $\sin 67' 30^{\circ}$, we have then

$$\begin{split} & \sin \delta_0 = A + C + E \\ & \sin \delta_{16} = A - C + E \\ & \sin \delta_1 = A + B_1 + C_7 + D_2 + E_6 \\ & \sin \delta_{31} = A - B_1 + C_7 - D_2 + E_6 \\ & \sin \delta_{15} = A + B_1 - C_7 - D_2 + E_6 \\ & \sin \delta_{15} = A + B_1 - C_7 + D_2 + E_6 \\ & \sin \delta_{15} = A - B_1 - C_7 + D_2 + E_6 \\ & \sin \delta_2 = A + B_2 + C_6 + D_4 + E_4 \\ & \sin \delta_3 = A - B_2 + C_6 - D_4 + E_4 \\ & \sin \delta_{30} = A - B_2 + C_6 - D_4 + E_4 \\ & \sin \delta_{14} = A + B_2 - C_6 - D_4 + E_4 \\ & \sin \delta_{18} = A - B_2 - C_6 + D_4 + E_4 \\ & \sin \delta_3 = A + B_3 + C_5 + D_6 + E_2 \\ & \sin \delta_{29} = A - B_3 + C_5 - D_6 + E_2 \\ & \sin \delta_{19} = A - B_3 - C_5 + D_6 + E_2 \\ & \sin \delta_{19} = A - B_3 - C_5 + D_6 + E_2 \\ & \sin \delta_{29} = A - B_4 + C_4 - D \\ & \sin \delta_{29} = A - B_4 - C_4 - D \\ & \sin \delta_{20} = A - B_4 - C_4 + D \end{split}$$

$$\begin{split} &\sin\delta_5 = A + B_5 + C_3 + D_6 - E_2 \\ &\sin\delta_{27} = A - B_5 + C_3 - D_6 - E_2 \\ &\sin\delta_{11} = A + B_5 - C_3 - D_6 - E_2 \\ &\sin\delta_{21} = A - B_5 - C_3 + D_6 - E_2 \\ &\sin\delta_6 = A + B_6 + C_2 + D_4 - E_4 \\ &\sin\delta_{26} = A - B_6 + C_2 - D_4 - E_4 \\ &\sin\delta_{10} = A + B_6 - C_2 - D_4 - E_4 \\ &\sin\delta_{22} = A - B_6 - C_2 + D_4 - E_4 \\ &\sin\delta_{22} = A - B_7 + C_1 + D_2 - E_6 \\ &\sin\delta_{23} = A - B_7 + C_1 - D_2 - E_6 \\ &\sin\delta_{23} = A - B_7 - C_1 + D_2 - E_6 \\ &\sin\delta_{23} = A - B_7 - C_1 + D_2 - E_6 \\ &\sin\delta_8 = A + B - E \\ &\sin\delta_{24} = A - B - E. \end{split}$$

- "'If the deviations are under 7° or 8°, the angles of deviation may be used in the formulæ instead of the sines of the angles without producing a sensible error in the result.
- "'It may be observed that $\varphi'\cos\theta'$ and $\varphi'\sin\theta'$ would be themselves properly expressed in a series containing sines and cosines of ζ' and $2\zeta'$, and this would introduce into the expression for $\sin\delta$ terms of the form

F sin
$$3\zeta' + G \cos 3\zeta' + H \sin 4\zeta' + K \cos 4\zeta'$$
.

"'The omission of these terms from the formula we have used does not affect the values we have found for A, B, C, D, E; and the values of the additional coefficients may be determined from the following expressions, in which we make use of the observations on the sixteen principal points only:—

$$F = \frac{1155}{\log = 1.06252} \{s_2 - s_{30} + s_{14} - s_{18}\},$$

$$+ \frac{0884}{\log = 2.94639} \{s_4 - s_{28} + s_{12} - s_{20}\},$$

$$- \frac{0478}{\log = 2.67975} \{s_6 - s_{26} + s_{10} - s_{22}\},$$

$$- \frac{1}{8} (s_8 - s_{24}). \qquad (31.)$$

$$G = \frac{1}{8} (s_0 - s_{16})$$

$$+ \frac{0478}{\log = 2.67975} \{s_2 + s_{30} - s_{14} - s_{18}\},$$

$$- \frac{0884}{\log = 2.94639} \{s_4 + s_{28} - s_{12} - s_{20}\},$$

$$- \frac{1155}{\log = 1.06252} \{s_6 + s_{26} - s_{10} - s_{22}\}. \qquad (32.)$$

$$H = \frac{1}{16} \{s_2 - s_{30} - s_{14} + s_{18} - s_6 + s_{26} + s_{10} - s_{22}\}. \qquad (33.)$$

$$K = \frac{1}{16} \{s_0 + s_{16} + s_8 + s_{24} - s_4 - s_{28} - s_{12} - s_{20}\}. \qquad (34.)$$

- "'If the deviations are so small that the angles may be used instead of their sines, then the differences between the observed deviations and the deviations calculated with the first five terms may be used instead of s_2 , s_4 , &c. in finding F and G or H and K. There is however no advantage gained thereby, as the quantities within the brackets in F and G have already been found in calculating B and C.
- "'As an example of the use of these formulæ, we may take the deviations observed on board Her Majesty's ship Erebus at Gillingham, in Sept. 1839*.
 - "'From the deviations observed on the sixteen principal points, I find

$$\delta = 17' + 235' \cdot \sin \zeta' - 13' \cos \zeta' + 21' \cdot \sin 2\zeta' - 1' \cdot 23 \cos 2\zeta'$$
.

"'From the deviations on the eight principal points, I find

$$\delta = 16' + 233' \cdot 5 \sin \zeta' - 14' \cdot \cos \zeta' + 21 \sin 2\zeta' - 0' \cdot 75 \cos 2\zeta'$$

"'Applying the correction derived from the first formula, the residuary differences on the sixteen principal points, beginning with north, are respectively—

$$-3', 0, +6', +14', -6', -18', +12', +7', +1', -11', -12', -9', +5', +7', +6', 0.$$

"'These differences evidently nearly follow the law of $\sin 3\zeta'$; they give

$$F=5'.5$$
; $G=-7'.$

" 'After applying the correction $5' \cdot 5 \sin 3\zeta' - 7' \cos 3\zeta'$, the residuary difference is +4' -2', -3', +9', 0', -9', +13', -1', -6', -9', -3', -4', -1', -2', +5', +8'.

"'The differences, it will be seen, are smaller, and do not distinctly follow any regular law. If we calculate H and K we shall find

$$H=2'$$
; $K=1'$.

But these corrections are so much within the errors of observation, that there could be no advantage in using them.

"'The expression for sin & may be put under the following form, viz.—

$$\sin \delta = A + \sqrt{B^2 + C^2} \sin (\zeta' + \alpha) + D \sin 2\zeta' + E \cos 2\zeta', \dots (35.)$$

in which α is the angle whose tangent is $\frac{C}{B}$, and is nearly the easterly azimuth of the line of no deviation.

"It seems probable that in ordinary cases A, α , D and E will not change materially with a change of latitude, while $\sqrt{B^2+C^2}$ will vary nearly as the tangent of the dip. The last-mentioned term is also the most important, from its magnitude and its dependence on the changes which the permanent magnetism undergoes. It may therefore be useful to have the means of obtaining this quantity separately. This may be done from observations of the horizontal force, made in the position of the standard compass, with the ship's head on any two opposite (affected) courses, from the formula

$$\sqrt{B^2 + C^2} = \frac{\sqrt{H_1^2 + H_2^2 + 2H_1H_2\cos(\text{diff. of true azimuth})}}{H_1 + H_2}, \dots (36.)$$

^{*} Contributions, No. V., p. 150.

in which H_1 H_2 represent the observed horizontal force in the two positions of the ship's head.

"' If the difference of the true azimuths of the ship's head is 180°, the expression

becomes
$$\sqrt{B^2+C^2} = \pm \frac{H_1-H_2}{H_1+H_2}, \quad (37.)$$

which is the same expression as that for the value of $\alpha \tan \theta$ in the Memorandum in No. V. of these Contributions.

- "'The value of the horizontal force may be determined by vibrating a horizontal needle, or by deflecting the compass needle in the manner described by Lieut. CLERK in page 347. The difference of azimuths may be determined by the bearings of a distant object, or astronomically.
- "'This method seems to be adapted to the case of a ship lying at moorings in a tideway. The observations may be made before and after the change of tide, and the rudder adjusted so that the difference of the compass bearings of the ship's head may be exactly 180°.
- "'This formula is more accurate the more nearly the dip approaches to 90°; and the method seems therefore particularly applicable in high magnetic latitudes.
- "'If the true magnetic azimuth of the ship's head on the two positions is determined, the values of B and C may be obtained by the formula

$$B = -\frac{H_2 \cos \zeta_1 + H_1 \cos \zeta_2}{H_1 + H_2},$$

$$C = \frac{H_2 \sin \zeta_1 + H_1 \sin \zeta_2}{H_1 + H_2}.$$

" 'A. S.'

" 'Lincoln's Inn, March 3, 1846."

"The constants for correcting the declination observations were (in consequence of this Memorandum) calculated by the equations 21, 22, 23, 24 and 25, taking the mean of the two series at the Cape of Good Hope.

"The following are the deduced values of the constants:-

Station.	θ.	ø.	A.	В.	C.	D.	E.
Cape of Good Hope Mauritius King George's Sound	-53 56	1.158		01550	+.00514	+.00448	00333 +-00335 +-00082
Means	-57 35	1.291	+.00844	02086	+.00638	+.00401	+.00028

"From the three values of B, and C, values of C' and P', F' and Q' were obtained by the equations

B=-
$$\left(C'\tan\theta+\frac{P}{\varphi\cos\theta}\right)$$
; and C=F' tan $\theta+\frac{Q}{\varphi\cos\theta}$;

for we have

Cape . .
$$-\cdot 01412 = C' \times 1\cdot 363 + P' \times 1\cdot 669$$
; also $+\cdot 00742 = -1\cdot 363F' - 1\cdot 669Q'$
Mauritius . $-\cdot 01550 = C' \times 1\cdot 373 + P' \times 1\cdot 467$; also $+\cdot 00514 = -1\cdot 373F' - 1\cdot 467Q'$
King George's Sound . $-\cdot 03295 = C' \times 2\cdot 151 + P' \times 1\cdot 393$; also $+\cdot 00658 = -2\cdot 151F' - 1\cdot 393Q'$.

Hence by elimination we obtain

$$C' = -.0209$$
; $F' = -.0006$; $P' = +.0088$; $Q' = -.0034$.

"From the values of C', P', F' and Q', a table of the values of B and C in different dips and intensities was formed, and from them with the mean values of A, D and E, a table for correcting the observations of Declination was calculated by equ. 35. The corrections thus obtained appear to give very closely the true corrections, at all events much within the limits of observation errors. The following is a comparison between the observed and calculated deviations at King George's Sound, θ being $=-65^{\circ}$ 04', and $\varphi=1.70$.

Ship's head.	δ by calcula- tion.	δ by observa- tion.	Difference.	Ship's head.	δ by calcula- tion.	δ by observa- tion.	Difference.
N. N.N.W. N.W. W.N.W. W. S.W. S.W.	+0° 52° +0° 17° -0° 21° -0° 58° -1° 16° -0° 54° -0° 24°	+0° 15′ 0 00 +0 20 -1 40 -1 50 -1 00 -0 24	-0 37 -0 17 +0 41 -0 42 -0 15 -0 34 -0 06 +0 09	S. S.S.E. S.E. E.S.E. E. N.E. N.E. N.N.E.	+0 03 +0 47 +1 25 +2 02 +2 25 +2 17 +1 52 +1 22	+0° 50° +0° 55° +2° 20° +3° 10° +2° 40° +3° 10° +3° 30° +2° 35°	+0 47 +0 08 +0 55 +1 08 +0 15 +0 53 +1 38 +1 13

+ Sign denotes a deviation towards the west.

"It appears from this comparison, that the calculated corrections are smaller in amount than the observed. As the ship had just returned from a high magnetic latitude, it is probable that the observed corrections belonged to a greater dip than the one at the station, and therefore that the corrections would be more nearly represented by taking them out from the Table for a larger Inclination and Intensity. The great differences on the E.S.E., N.E. and N.N.E. points are caused most probably by errors of observation.

"The correctness of equation (6.) will be more easily perceived by the accordance of observations made at sea, in a high dip, making due allowance for the difficulty of observing in bad weather.

"2. Calculation of Corrections for the Inclination Observations.

"To obtain these corrections four constants are necessary, viz. a, b, c, d; a and b are obtained from the deviations of a compass (placed on the same spot as the dipping-

needle) on the sixteen principal points.	The following are the observations at King
George's Sound, the Mauritius, and the	Cape of Good Hope.

Ship's head.	King George's Sound.	Mauritius.	Cape of Good Hope.	Ship's head.	King George's Sound.	Mauritius.	Cape of Good Hope.
N. N.N.W. N.W. W.N.W. W. S.W. S.W. S.S.W.	-0 45 -1 15 -2 05 -3 20 -3 35 -3 45 -1 55 *3 00	-0 05 -1 25 -1 45 -2 25 -3 05 -3 05 -1 35 -1 05	-0 25 Not observed0 05 -0 35 -0 50 -1 15 -1 45 -0 35	S. S.S.E. S.E. E.S.E. E. N.E. N.E.	Not observed. +2 40 +3 25 +3 25 +3 25 +2 35 +2 45 +2 20	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-0 50 Not observed. +1 55 +2 35 +2 40 +1 10 +0 45 +0 05

[&]quot;Allowing for the errors of observation, it appears from these observations that the iron is symmetrically distributed in reference to the compass placed on the same spot where the observations of inclination and intensity were made, and therefore that we may use the equations in Contributions V. and VI.

"From these equations the values of a and b are found,—

At King George's Sound . . .
$$a=0296$$
; $b=9867$; Mauritius $a=0272$; $b=9910$; Cape of Good Hope $a=0192$; $b=9766$.

"The values of a and b can be found independently of the compass, from the observations of dip and intensity themselves, A' being supposed =1, by means of the formulæ

"Values of ϕ' and θ' were obtained from observations on the sixteen principal points of the compass made at King George's Sound, Mauritius, and the Cape of Good Hope. They are as follows:—

Values of θ' .

	Obs	erved Inclinati	on.		Obs	erved Inclinati	on.
Ship's head.	King George's Sound.	Mauritius.	Cape of Good Hope.	Ship's head.	King George's Sound.	Mauritius.	Cape of Good Hope.
N. N.N.W. N.W. W.N.W. W. S.W. S.W.	-66 15 -66 33 -66 19 -66 07 -65 44 -65 42 -65 31 -64 48	-54 38 -54 44 -54 47 -55 02 -55 21 -54 39 -54 29 -54 07	$\begin{array}{cccc} -5\mathring{4} & 0\mathring{1} \\ -5\mathring{4} & 35 \\ -5\mathring{4} & 56 \\ -5\mathring{4} & 47 \\ -5\mathring{4} & 46 \\ -5\mathring{4} & 31 \\ -5\mathring{3} & 45 \\ -5\mathring{3} & 09 \\ \end{array}$	S. S.S.E. S.E. E.S.E. E. E.N.E. N.E.	$\begin{array}{c} -6\overset{4}{4} \ 5\overset{2}{2} \\ -65 \ 00 \\ -65 \ 29 \\ -65 \ 5\overset{2}{2} \\ -66 \ 23 \\ -66 \ 07 \\ -66 \ 31 \end{array}$	-53 46 -53 41 -54 20 -54 25 -54 50 -54 55 -54 47 -54 27	-53 28 -53 50 -53 51 -54 24 -54 46 -54 53 -54 37 -54 25

^{*} This observation is not taken into account, being obviously erroneous. 3 a

Values	of	φ'	
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	Оъ	served Intens	ity.		Observed Intensity.				
Ship's head.	King George's Sound.	Mauritius.	Cape of Good Hope.	Ship's head.	King George's Sound.	Mauritius.	Cape of Good Hope.		
N. N.N.W. N.W. W.N.W. W. S.W. S.S.W.	1·737 1·736 1·734 1·752 1·758 1·775 1·790	1·150 1·152 1·151 1·158 1·166 1·198 1·191 1·200	1.024 1.020 1.025 1.025 1.028 1.036 1.049	S. S.S.E. S.E. E.S.E. E. N.E. N.E.	1·799 1·797 1·790 1·773 1·753 1·757 1·736	1·206 1·204 1·182 1·189 1·169 1·166 1·159	1.066 1.055 1.045 1.032 1.029 1.024 1.023		

"The observed values of θ and φ are approximately—

King George's Sound . .
$$\theta = -65^{\circ} 11^{\circ}$$
; $\varphi = 1.733$
Mauritius $\theta = -54 14$; $\varphi = 1.158$
Cape of Good Hope . . . $\theta = -53 37$; $\varphi = 1.027$.

"Substituting these values in equations (1.) and (2.), we have

King George's Sound . .
$$a=.0242$$
; $b=.9905$; Mauritius $a=.0234$; $b=1.0105$; Cape of Good Hope . . . $a=.0186$; $b=.9916$.

"Including these values with those obtained from the compass observations, we get the mean values for a and b,

$$a = .0237$$
; $b = .9912$.

"The constants c and d are calculated from the formula

$$c\cos\zeta+d\tan\theta=b\sin\zeta\csc\zeta'\tan\theta'$$

for the observations between N.N.W. and S.S.W., and N.N.E. and S.S.E.; and for the other points, viz. N. and S., by the formula

$$c\cos\zeta+d\tan\theta=(\cos\zeta+a\tan\theta)\sec\zeta'\tan\theta'.$$

"The values of ζ and θ ' were given by the observations at the several stations. The values of c and d are as follows:—

King George's Sound . .
$$c=.010$$
; $d=1.054$; Mauritius $c=.014$; $d=1.011$; Cape of Good Hope . . . $c=.003$; $d=1.033$.

The values of c and d were also obtained from the observations of dip and intensity, independently of a and b, by the formula

$$c\cos\theta\cos\zeta-d\sin\theta=\frac{\phi'}{\phi}\sin\theta'$$

A being supposed equal to unity; which gives the following values:—

King George's Sound . . c=.028; d=1.023; Mauritius c=.024; d=1.017; Cape of Good Hope . . . c=.021; d=1.020.

"The mean of these six values makes

$$c=0.017$$
; $d=1.026$.

"From these values of a, b, c and d, a table of corrections was found by means of equations (12.) and (13.) (Contribution V.), employing calculated values of ζ .

"In order to test the accuracy of the table, we may compare observed and calculated values of the dip at King George's Sound. It will be seen that on the northerly points the correction is rather too large, on the easterly and westerly too small, and nearly correct on the S., S.S.W. and S.S.E. points. The differences however are within the limits of observation errors.

Ship's head.	Observed Incli- nation.	Tabular correction.	Corrected Inclination.
N. N.N.w. and N.N.E. N.W. and N.E. W.N.W. and E.N.E. W. and E. S.W. and S.E. S.W. and S.E. S.S.W. and S.S.E.	$\begin{array}{c} -6\mathring{6} \ 1 \acute{5} \\ -66 \ 3 2 \\ -66 \ 18 \\ -66 \ 07 \\ -66 \ 03 \\ -65 \ 47 \\ -65 \ 30 \\ -64 \ 54 \\ -64 \ 52 \\ \end{array}$	+1 23 +1 23 +1 31 +1 09 +0 46 +0 23 +0 02 -0 16 -0 18	$ \begin{array}{c} -6\mathring{4} & 5\mathring{2} \\ -65 & 09 \\ -64 & 47 \\ -64 & 58 \\ -65 & 17 \\ -65 & 24 \\ -65 & 28 \\ -65 & 10 \\ -65 & 10 \end{array} $

The mean inclination observed on shore with the same needle being -65° 11'.

"3. Calculation of Corrections for Intensity Observations.

"The constant A is calculated from the above observations by means of the formula

$$\frac{\Phi_{\cdot}^{f}}{A'\Phi}\sin\theta'=c\cos\theta\cos\zeta+d\sin\theta.$$

"The values of θ , φ' and ζ , are all given by the observations on the sixteen points of the compass; those of φ and θ by the observations on shore. The following are the resulting values for A', viz.—

King George's Sound . . . A'=0.998Mauritius A'=0.992Cape of Good Hope . . . A'=0.992Mean . . A'=0.994

"This value being so near unity, A is assumed =1.0, with which and the values of c and d already determined, a table of corrections was formed by means of the equation

$$\frac{\phi'}{\phi} = A'c(\frac{d}{c}\tan\theta + \cos\zeta)\cos\theta \csc\theta' *,$$

 θ' and ζ being obtained from the tables for correcting the dips and declinations.

* Philosophical Transactions, 1843, Part II. p. 162.

"II. Determination of Index Corrections.

"1. Declination Observations.

"The compass used was one of the Admiralty compasses (B. 20). It was supplied with two cards, one considerably heavier than the other to be used in bad weather; but as it was found that in all weathers the heavy card was the steadiest and gave the best results, it was accordingly generally used. The index corrections of both cards were determined at the Magnetic Observatory, Cape of Good Hope. The following are the means of several observations with each card; the mean monthly declination by the observatory declinometer being $+29^{\circ}$ 07'.

Card A (the light card) gave
$$.+2\mathring{8} \stackrel{\circ}{20}$$
; correction $+4\mathring{7}$.
Card J (the heavy card) gave $.+28 \stackrel{\circ}{15}$; correction $+52$.

"These corrections have been applied to all the observations, according to the card employed.

"2. Inclination Observations.

"Two of Mr. Fox's instruments were kept in constant use, one observed in the forenoon and the other in the afternoon. In order to distinguish them, we may call the one observed in the morning No. 1, the other was marked C. 9. In No. 1, needle 1 was mounted and used throughout, the spare needle 2 being used as a deflector. The index correction for 1 was determined at the Magnetic Observatory at the Cape, both before and after the Expedition, by comparing the inclination with the face of the instrument west (that being the way the observations were taken on board) with the mean monthly inclination shown by the observatory needles. The following are the observations with the deflectors at 40° from the apparent dip:—

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November 10, 1844, needle 1, face west -5\overset{\circ}{3} 3\overset{\circ}{9}; correction +\overset{\circ}{8} November 10, 1844, needle 1, face east -53 59; correction +28 November 21, 1844, needle 1, face west -53 38; correction +7 November 21, 1844, needle 1, face east -53 58; correction +27 The mean monthly inclination being -53^{\circ} 31'.
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"After the 13th of January it was found more convenient to adjust the deflectors at the apparent dip, and make the same observations serve both for dip and intensity. The index corrections to be applied in this case are given by the following observations:—

70.4		Observed	Inclination.—I	Face West.	•	True Inclina-	Index correc-
Date.	Direct.	Def. N.	Def. S. Def. N and S. Mean.		Mean.	tion.	tion.
1844. December 1 December 5 1845.	$-5\overset{\circ}{3} \overset{\circ}{52} \\ -53 \overset{\circ}{49}$	$-5\overset{\circ}{3}\overset{\circ}{21}$ $-5\overset{\circ}{3}\overset{\circ}{20}$	$-5\overset{\circ}{3} \overset{\prime}{44} \\ -53 & 43$	$-5\overset{\circ}{3} \overset{\circ}{39} \\ -53 \overset{\circ}{38}$	$-5\overset{\circ}{3} \overset{\circ}{3}\overset{\circ}{9} \\ -53 \overset{\circ}{3} 8$	$\left.\begin{array}{cccccccccccccccccccccccccccccccccccc$	+ 07
June 30	$ \begin{array}{rrr} -54 & 12 \\ -54 & 08 \end{array} $	-53 13 $-53 15$	$-53 ext{ } 46 \\ -53 ext{ } 46$	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$ \begin{array}{rrr} -53 & 45 \\ -53 & 43 \end{array} $	$\left53 \ 25 \right.$	+19
Mean	-54 01	-53 17	-53 45	$-53 \ 43$	$-53 \ 41$	-53 28	+13

"Magnets N and S are the small magnets belonging to the apparatus used conjointly; deflector N and deflector S are the respective poles of the spare needle. +13' has been applied in all cases except when only magnets N and S have been used, in which case +24' has been used, that being the mean correction for direct and magnets N and S.

"For the index corrections for needle A of C. 9, we have only an observation in Simon's Bay, Cape of Good Hope, before starting. Needle A was used from the Cape to King George's Sound, and was observed on shore at King George's Sound on the 7th of April. On the 10th it was found, from the discordance of the observations, that its axle had been damaged since the observations on the 7th, it was therefore taken out and needle B mounted in its place. The instrument had a third needle C which was used as a deflector. The small magnets were also used, both conjointly and separately. The observation in Simon's Bay gives,—

For C. 9, needle A
$$-53^{\circ} 24'$$
 Corrected inclination, needle 1 . . . $-53^{\circ} 50'$ Index correction $-26'$.

This correction has been applied to all observations made with needle A of C. 9. For the correction of needle B, we have a comparison at the Cape of Good Hope after the return of the Expedition, and also at Woolwich, in January 1846. All observations with this instrument were taken with the face east.

"The following	g are the	observations	at the	Cape:—
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Date.			Observed	Inclination.—l	Face East.			True	Index correc-	
Batter	Direct.	Def. N.	Def. S.	Mag. N and S.	Mag. N.	Mag. S.	Mean.	Inclination.	tion.	
1845. June 30. July 2.		$-5\overset{\circ}{4} \ 1\overset{\circ}{5} \\ -54 \ 11$	$-5\overset{\circ}{2} 4\overset{\prime}{7} \\ -52 55$	$-5\mathring{4} 06'$ $-54 15$	$-5\overset{\circ}{3} \overset{\circ}{29} \\ -53 \overset{\circ}{49}$	$-53^{\circ} 23^{\circ} -53^{\circ} 41^{\circ}$	$-5\overset{\circ}{3} \overset{40}{45}$	$-5\overset{\circ}{3}\ 2\overset{\prime}{5} \\ -53\ 25$	$+15 \\ +20$	
Mean	-53 48	-54 13	-52 51	-54 10	-53 39	-53 32	-53 43	-53 25	+18	

"And at Woolwich:-

Date.					True	Index			
Date.	Direct.	Def. N.	Def. S.	Mag. N and S.	Mag. N.	Mag. S.	Mean.	Inclination.	correc- tion.
1846. Jan. 13. 15.		$+68 02 \\ +68 21$	$+68 37 \\ +68 52$	$+68^{\circ} 24^{\circ} +68^{\circ} 45^{\circ}$	$+68 \ 32 \ +68 \ 35$	$+68 \ 30 \ +68 \ 34$	$+68 \ 31 \ +68 \ 41$	$\left.\right\} + 68^{\circ} 58^{\circ}$	+22
Mean	+6857	+68 12	+68 44	+68 35	+68 33	+68 32	+68 36	+68 58	+22

[&]quot;The index correction obtained at the Cape has been used for all the observations taken with this needle.

- "3. Elements of Calculation of the Intensity Observations.
- "Fox No. 1.—For the observations with this instrument, the Cape of Good Hope has been taken as a base station, the intensity having been observed there both before and after the Expedition, so that any change in the magnetism of the deflectors or needles can be detected.
- "The intensity at Woolwich being assumed =1.372, it is necessary to get the corresponding intensity at the Cape. This can be got independent of the dippingneedles, by means of the absolute horizontal intensity and inclination observed at each station.
- "The value of the horizontal intensity at the Cape is given as follows by observations made at the observatory in February, March, April and May 1845:—
- "Observations of the Absolute Horizontal Intensity, at the Magnetic Observatory, Cape of Good Hope, 1845.

Bar. A. 21. Suspended . . . length 3.00 inch . . .
$$\left(1 + \frac{H}{F}\right) = 1.00084$$
.

Bar. V. Deflecting . . . length 3.67 inch . . . $q = .00008 . . . \log \pi^2 . k = 1.57254$.

Date.	Angles of	Deflection.	time of		Bifilar readings at 60 during		Results.			
er	Dist. 1.2 ft.	Dist. 1·3 ft.	vibration.	Deflection.	Vibration.	Deflection.	Vibration.	m.	x.	
1845. Feb. 10, 11, 12. Mar. 10, 11, 12. Apr. 13, 14, 15. May 14, 15, 16.	6 01·1 5 57·5	4 47.5 4 44.0 4 41.2 4 39.2	s 4·4970 4·5310 4·5570 4·5650	7 ¹ ·4 71·4 62·9 60·7	7 [°] 1·7 71·9 62·6 59·9	Scale dir. 185·9 186·0 176·9 177·2	185·8 177·4	0·4118 0·4064 0·4019 0·4001	4·480 4·478	4.482

[&]quot;The value of k is obtained by means of two cylindrical weights in the usual manner; the value employed is the mean of several determinations. Bifilar magnetometer k=000218, q=000218. Increase of reading denotes increase of force.

Whence
$$X=4.482$$
, θ being $=-53^{\circ} 25'.5$.

"The corresponding values at Woolwich are

$$X=*3.7284$$
, θ being = $+68^{\circ}$ 57'.9.

- "From these values of X and θ , we obtain the relative value of the intensity at the Cape (that at Woolwich being 1.372), I=0.993.
- "The relative intensity given by the needles of No. 1, from observations made at Woolwich and the Cape and given in the sequel, are as follows:—

Needle 1.
$$\{ \begin{array}{ll} \text{Weight 1 gr. I=0.996} \\ \text{Weight 2 grs. I=1.017} \\ \end{array} \} 1.006. \quad \text{Needle 2.} \{ \begin{array}{ll} \text{Weight 1 gr. I=0.994} \\ \text{Weight 2 grs. I=1.006} \\ \end{array} \} 1.000.$$

^{*} Contributions, No. VII.; Philosophical Transactions, 1846, p. 246.

"The value of I at the Cape has therefore been assumed provisionally as unity; subject to future correction should any appear to be required.

"The spare needle 2 was always used as a deflector; the two small magnets were used conjointly only with this apparatus.

"Tables of equivalent weights were made at the Cape both before and after the Expedition, according to the method given in the instructions for the use of Mr. Fox's instrument. The following Table contains the mean of the two series.

De	ef. N.	De	ef. S.	Mag. 1	Mag. N and S.		f. N. inued.)	Def. S. (Continued.)		Mag. N. and S. (Continued.)	
v'.	w'.	v'.	w'.								
21 22 23	gr. 1.816 1.835 1.850	22 23 24	gr. 1·950 1·964 1·972	41 42 43	grs. 3·608 3·522 3·438	31 32 33	gr. 1·843 1·828 1·814	32 33 34	gr. 1.935 1.918 1.903	51 52 53	grs. 2·786 2·717 2·654
24 25 26 27 28	1.861 1.867 1.868 1.867 1.866	25 26 27 28 29	1.977 1.983 1.980 1.977 1.968	44 45 46 47 48	3·350 3·262 3·179 3·093 3·013	34 35 36 37 38	1.801 1.788 1.770 1.756 1.744	35 36 37 38 39	1.891 1.868 1.852 1.833 1.812	54 55 56 57 58	2.595 2.535 2.480 2.428 2.377
29 30	1.861 1.858	30 31	1.960 1.946	49 50	2.933 2.853	39 40	1.726 1.707	40 41	1.793 1.775	59 60	2.330

"With these values of w', and the following values of v and w, the values of I' have been calculated by the formula

 $I' = I \frac{\sin v \cdot w'}{\sin v' \cdot w}$ when deflectors are used, and

 $I'=I\frac{\sin v}{\sin v'}$ when weights are used.

Values of v at the Cape of Good Hope.

	Date.	Def. N. $w = 1.721$.	Def. S. $w = 1.782$.	Mag. N and S. $w=2.337$.	Weight 1 grain.	Weight 2 grains.	Weight $2\frac{1}{2}$ grains.
	1844. Dec. 1. 5.	39 06 39 01	40 38 40 37	59 23 59 22	21 36 21 34	46 54 46 33	65 22 65 20
	1845. June 30. July 2.		40 39 40 39	5 8 16 58 21	21 38 22 06	46 32 46 21	65 30 65 30
1	Mean	39 15	40 38	58 51	21 42	46 35	65 25

"From this Table it is evident that, with the exception of magnets N and S, the needles preserved their magnetism throughout the voyage. Magnets N and S lost magnetism to the amount of 033. The mean of the four observations have been taken; the early intensities by this method will therefore be rather too small, the latter ones rather too great.

"The formulæ for calculation are as follows:-

"Fox C. 9.—The values of the intensity at the Cape by the observations before and after the Expedition, by Fox, No. 1, are:—

Before
$$I=0.999$$
 After $I=1.001$ diff. 002 .

"These values agreeing so closely, we may assume that the intensity at King George's Sound with this apparatus will be very near the truth, and that King George's Sound may therefore be taken as a base station for needle A of C. 9, which was not observed at the Cape before our departure. The intensities were observed with needle A mounted, from the Cape to King George's Sound, when the needle got unfortunately damaged, and it was necessary to replace it with needle B: one day's observations had however been made before the accident, and these observations serve for calculating the intensities taken on the voyage, assuming the intensity at King George's Sound to be that given by the other apparatus, viz. 1.688.

"The same deflectors and weights were used throughout; the spare needle C as a deflector, the two small magnets both conjointly and separately.

"Tables of equivalent weights for these deflectors, with needle A mounted, were obtained in the same way as in the case of the other apparatus. They are as follows:

De	f. N.	De	f. S.	Mag. N	and S.	Ma	g. N.	Ma	g. S.
v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.
5ů	grs.	5	grs.	7ů	grs. 2.625	5ů	grs.	5 0	grs.
	2.175		2.206	70	2.675	49	1.578	49	1.975
49	2.200	49	2 247	69		49 48	2.028	48	2.025
48	2.225	48	2.288	$\frac{68}{67}$	2.725	47	2.078	47	2.075
47	2.263	47	2.323	66	2·775 2·825	46	2.130	46	2.125
46	2.300	46	2.357	65	2.875	45	2.235	45	2.175
45	2.338	45	2.388		2.925	44	1 1 1	44	2.240
44	2.375	44	2.419	$\begin{array}{c} 64 \\ 63 \end{array}$	2.982	43	2·288 2·341	43	2·304 2·368
43	2.413	43	2.460		3.038	42	2.394	42	1
42	2.450	42	2.500	62	3.038	41		41	2.433
41	2.488	41	2.538	61			2.447		2.498
40	2.525	40	2.575	60	3.150	40	2.500	40	2.563
. 39	2.565	39	2615	59	3.222	39	2.570	39	2.623
38	2.605	38	2.655	58	3.294	38	2.640	38	2.683
37	2.645	37	2.695	57	3.365	37	2.710	37 20	2.743
36	2.685	36	2.735	56	3.436	36	2.780	36	2.803
35	2.725	35	2.775	55	3.507	35	2.850	35	2.863
34	2.755	34	2.806	54	3.595	34	2.900	34	2.937
33	2.785	33	2.837	53	3.683	33	2.950	33	3.011
32	2.815	32	2.869	52	3.770	32	3.000	32	3.085
31	2.845	31	2.901	51	3.857	31	3.050	31	3.158
30	2.875	30	2.932	50	3.944	30	3.100	30	3.232
29	2.900	29	2.954	49	4.047		1		
28	2.925	28	2.975	48	4.150		1 1		

"The angles of deflection observed at King George's S	Sound are as follows:—
---	------------------------

Def. N. $w = 2.779$	Def. S. $w = 2.821$.	Mag. N and S. $w = 3.909$.	Mag. N. $w = 2.875$.	Mag. S. 2.895.	Weight 1 grain.	Weight 1½ grain.	Weight 2 grains.	Weight $2\frac{1}{2}$ grains.	Weight 3 grains.
33° 11	33 32	50° 24	34 30	34 34	10° 44	1 ₇ 16	22° 55	28 18	35° 10′

"Employing the values of v and w (I being = 1.688), we get formulæ for calculating the intensities, viz.—

```
Def. N . . . . I' = :3325 \csc v' \cdot w'.

Def. S . . . . I' = :3306 \csc v' \cdot w'.

Mag. N and S I' = :3327 \csc v' \cdot w'.

Mag. N . . . I' = :3326 \csc v' \cdot w'.

Mag. S . . . . I' = :3308 \csc v' \cdot w'.
```

Weight 1 grain . I'=:3144 cosec v'.

Weight $1\frac{1}{2}$ grain. I'=:5010 cosec v'.

Weight 2 grains . I'=:6573 cosec v'.

Weight $2\frac{1}{2}$ grains . I'=:8003 cosec v'.

Weight 3 grains . I'=:9722 cosec v'.

Comparing observations made at sea near the Cape with those given by the other needle, the deflectors of this apparatus do not appear to have lost magnetism.

"From King George's Sound to the Cape, needle B was mounted, the same deflectors and weights being used as with needle A. The Cape of Good Hope has been taken as the base station in this case, the intensity having been observed there on the return of the Expedition.

"The table of equivalent weights is given below.

De	ef. N.	$\mathbf{D}\epsilon$	f. S.	Mag. N	V and S.	Ma	g. N.	Ma	ıg. S.
v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.
2 9	1.794	$3\mathbf{\mathring{5}}$	2.104	5 0	2.763	3î	1.891	3 6	2.174
30	1.782	36	2.076	51	2.701	32	1.862	37	2.122
31	1.765	37	2.046	52	2.638	33	1.833	38	2.069
32	1.748	38	2.015	53	2.576	34	1.804	39 .	2.012
33	1.734	39	1.986	$\bf 54$	2.513	35	1.773	40	1.954
34	1.719	40	1.956	55	2.457	36	1.741	41	1.903
35	1.697	41	1.927	56	2.401	37	1.705	42	1.851
36	1.675	42	1.898	57	2.345	38	1.669	43	1.801
37	1.657	43	1.865	58	2.288	39	1.635	44	1.751
38	1.638	44	1.832	59	2.247	40	1.600	45	1.707
. 39	1.619	45	1.799	60	2.203	41	1.563	46	1.663
40	1.600	46	1.766	61	2.167	42	1.525	47	1.626
41	1.582	47	1.740	62	2.110	43	1.494	48	1.588
42	1.563	48	1.713	63	2.071	44	1.463		
43	1.541	49	1.684	64	2.032	45	1.443		
44	1.519	50	1.654	65	1.996		1 1		
45	1.491			66	1.960				
				67	1.927				1

"The following are the angles of deflection on three separate days at the Magnetic Observatory, Cape of Good Hope:—

Def. N. $w = 1.500$.	Def. S. $w = 1.659$.	Mag. N and S. $w = 1.953$.	Mag. N. w=1.480.	Mag. S. $w = 1.615$.	Weight 1 grain.	Weight 1½ grain.	Weight 2 grains.
4 ³ 3 ² 45 00	49 48 49 59	66 02 66 20	43 21 43 45	4 [°] 7 13 47 23	28° 00	44 1ó	69° 31′
44 33	49 42	66 16	43 15	47 20	28 26	44 16	69 15
44 42	49 50	66 13	43 27	47 19	28 13	44 13	69 23

"Assuming the intensity at the Cape as unity, we get the following formulæ for calculation:—

Def. N	•		٠.,	•.	$I'=4692 \csc v' \cdot w'$.
Def. S	•	•		•.	$l'=4606 \csc v' \cdot w'$.
Mag. N and S .		•			$I'=4686\csc v' \cdot w'$.
Mag. N					$I'=4634 \csc v' \cdot w'$.
Mag. S	•			•	$I'=4552 \csc v' \cdot w'$.
Weight 1 grain.		•		•	$I'=4728\csc v'$.
Weight 1½ grain		•.			$I' = 6974 \csc v'$.
					$I' = .9361 \csc v'$.

"The value of the intensity at King George's Sound by this needle is-

By weights 1 688. By deflectors . . . 1 672.

"The intensity by the other apparatus No. 1 is 1.688.

"At the Mauritius the intensity is-

By weights 1.156. By deflectors 1.155.

And by the other instrument 1.156.

"It is therefore evident that needle B preserved its magnetism from King George's Sound to the Cape. Comparing the results with the deflectors with those of the other instrument, the deflectors do not appear to have lost magnetism; the difference at King George's Sound of '01 arises probably from error of observation. As the results given by weights are the most accurate when the observations are made on land, they have been exclusively used in such cases; at sea both weights and deflectors have been used.

"Besides the correction for the effect of the ship's iron, a second correction for the effect of temperature on the needle and deflectors is necessary. The observations have all been reduced to a common temperature of 60° by means of the formulæ

$$c=\mathbf{I}'$$
. $q(t'-t)$,

t being taken as 60° and q being the coefficient for 1° of Fahr. Values of q for each needle and deflector employed, were obtained at the Magnetic Observatory, Cape of Good Hope, in the usual manner. The following is an abstract of the observations:—

Needle or deflector.	Approximate distance.	Total deflec- tion in scale divisions.	Mean alternation of temperature.	No. of alternations.	Corresponding mean differ- ence of deflection.	billar correc-	Values of q .
$\begin{array}{c} {\rm No.\ 1.} \begin{cases} {\rm A.\ 1.} \\ {\rm A.\ 2.} \\ {\rm Def.\ N} \\ {\rm Def.\ S} \end{cases} \\ {\rm C.\ 9.} \begin{cases} {\rm A.} \\ {\rm B.} \\ {\rm C.} \\ {\rm Def.\ N} \\ {\rm Def.\ S} \end{cases} \end{array}$	ft. in. 3 0 3 0 1 0 1 5 1 5 1 5 1 0 1 0	497.5 805.2 873.3 880.5 1019.0 1059.5 1065.9 1004.8 1021.7	38 35 38 76 40 43 40 02 34 68 43 35 43 46 45 85 47 38	5 5 5 5 3 4 5 5 5	1·36 3·88 4·33 2·82 4·21 3·18 3·67 7·08 6·45	+·000046 +·000004 ·000019 ·000054 -·000070 -·000004 +·000008 +·000004	**************************************

"From the values of q tables of corrections were formed; observing that when weights are used an increase of temperature gives an additive correction, and the contrary when the deflectors are used. As the values of q are small, and the greatest difference of temperature amounts only to 30° , the corrections are seldom of any importance; they have however always been applied.

"Besides the observations made on board the Pagoda, others have been laid down on the maps, in order to assist in drawing the magnetic lines. A series of observations made by Lieut. Smith, R.N., between the Cape and Van Diemen Island, and another by Lieut. Dayman, R.N., between Van Diemen Island and the Cape (with the same instrument), have been laid down on the map of the Inclination. The same needles and deflectors were used in both cases. Lieut. Smith's observations are all taken with the face of the instrument east; those of Lieut. Dayman's with it both east and west. The following observations, made at the Ross Bank Observatory, Van Diemen Island, will serve to obtain the index corrections; the inclination by the observatory needles being -70° 40'.

Observer.	Direct.	Def. N.	Def. S.	Def. N and S.	Mean.	Index correction.	Face of instrument.
Lieut. SMITH. Lieut. DAYMAN. Lieut. SMITH. Lieut. DAYMAN.	-7054	-69 54	-7042	-71 36 } }	1	+48 -27	East West

"These corrections have been applied to all the observations made by Lieut. Smith *.

"As no observations were made for local attraction, we can only obtain approximate corrections, by comparing observations made on or near the same spot with the ship's head on different points of the compass. In the series made by Lieut. Smith we have the following observations:—

T	August 14.	August 18.	September 10. September 13.	September 13.	
S.I	E. by E. ½ E68 06	E. by s -67 3	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	02 09	

- "From these comparisons it would appear that the correction is very small, especially on the easterly points which were those generally observed upon; the observations have therefore been entered without any correction for the effect of the ship's iron
- "With regard to those of Lieut. DAYMAN, there are two cases where observations have been taken on different days, but in nearly the same position, and with the
- * When observations have been made with the face both east and west, the correction becomes +10'; when weights as well as deflectors are used for the inclination, the correction face east and west becomes -13'; this has been applied to the observations made by Lieut. Dayman.

ship's head on different points of the compass, and also some in very nearly the same geographical position as the Pagoda. Comparing these, it appears that the effect of the iron is nearly the same in both ships; the observations have consequently been corrected from the Table that was used for those taken on board the Pagoda. The following comparisons will show how near these corrections approach the truth.

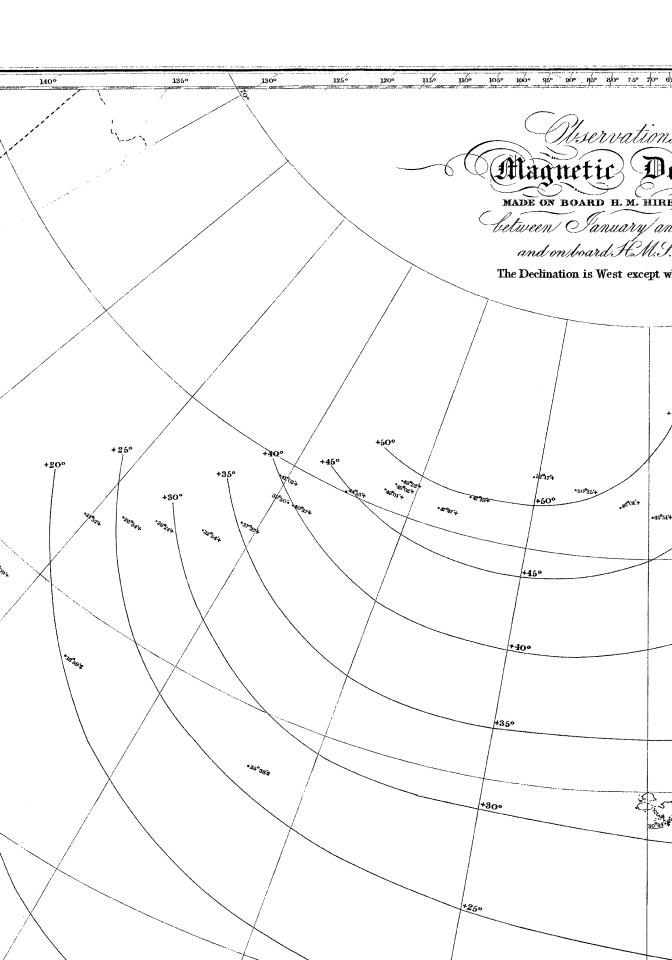
Lat.	Long.	Inclination.	Ship's head.	Tabular corrections.	Corrected Inclination.		Remarks.
-35 22 -35 06 -34 58 -34 16 -24 00 -23 59 -34 36 -34 31 -34 48 -35 07 -36 58 -36 06 -36 24	117 55 112 59 113 01 99 33 99 15 25 23	$ \begin{array}{r} -66 & 47 \\ -55 & 32 \\ -57 & 01 \\ -56 & 09 \end{array} $	N.W. W.N.W. S.W. $\frac{1}{2}$ W. N. by W. $\frac{1}{2}$ W.	+1 31 +1 12 +0 18 +1 19	-65 14 -65 16 -64 44 -54 20 -54 07 -56 43 -57 06 -55 08 -67 03 -67 19 -66 27	Lieut. Dayman. Lieut. Clerk. Lieut. Dayman. Lieut. Clerk. Lieut. Dayman. Lieut. Dayman. Lieut. Dayman. Lieut. Dayman. Lieut. Dayman. Lieut. Dayman.	Difference + 0

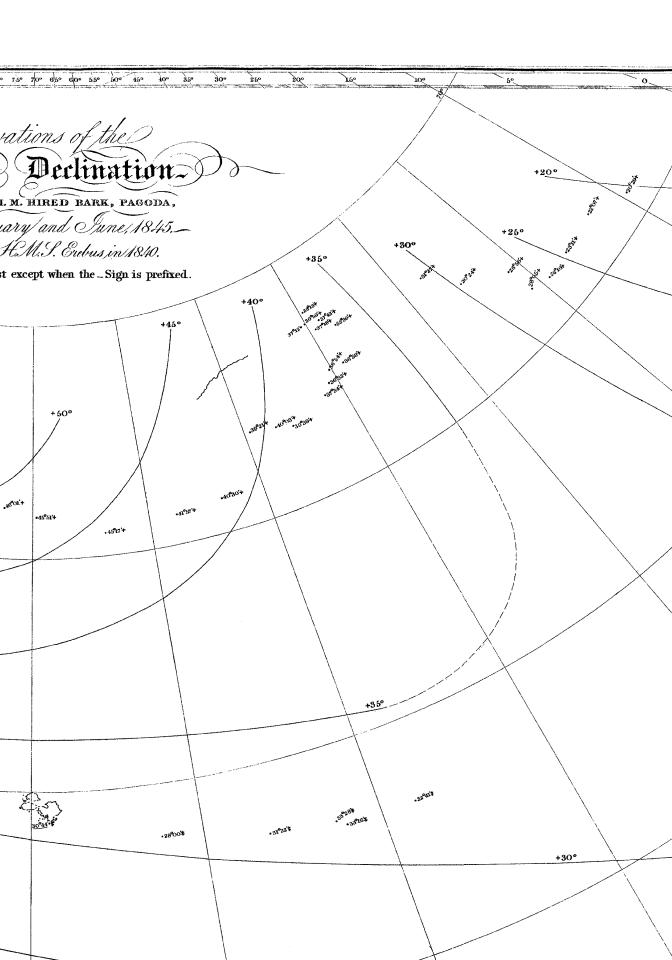
"The observations thus corrected have been entered in the chart. The lines on the chart are drawn by estimation, so as to conform as nearly as possible with the observations: some part of the lines laid down by Lieut.-Colonel Sabine (in No. V. of the Contributions) from Sir James C. Ross's observations have been dotted in, to show the agreement of the two series.

"In the Chart of 'Magnetic Declinations,' a series of observations made on board the 'Erebus' by Sir James C. Ross, between the Cape of Good Hope and Hobarton, have been laid down. These observations have been corrected for index error and local attraction, in the same way as the other observations during the Antarctic Expedition, the same constants being used.

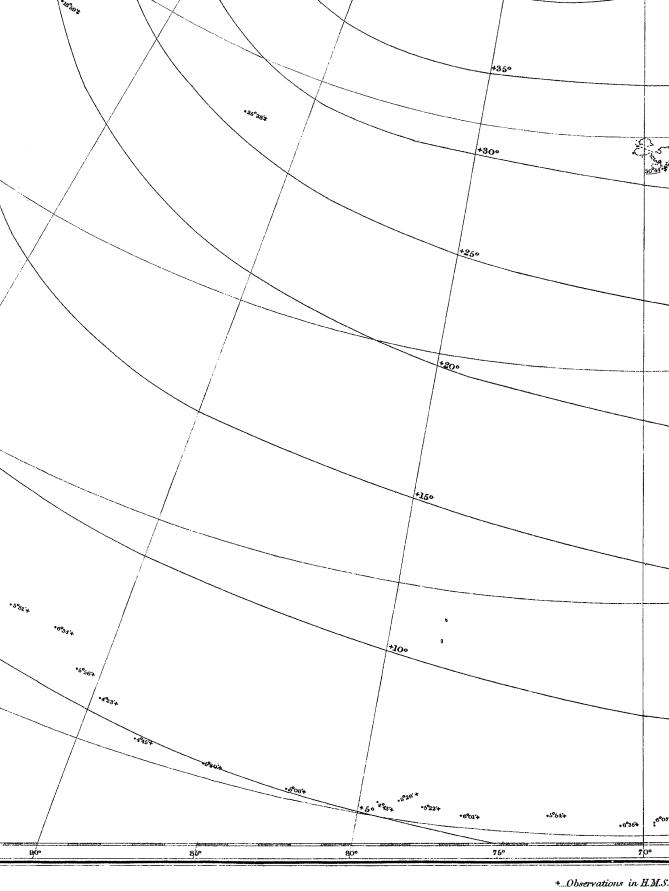
"In the chart of intensities, Sir James C. Ross's observations between the Cape of Good Hope and Hobarton have also been entered. These observations are contained in Lieut.-Colonel Sabine's Contributions, No. III. and V. The Cape of Good Hope is the base station in this case; but the intensity there has been taken as 0.981; it is therefore necessary to reduce them to an intensity at the Cape = 1.0, in order that they may compare with the intensities taken on board the Pagoda; this is done by multiplying each of them by $\frac{.981}{1.000} = 1.02$ nearly. The observations thus corrected are given in a table at the end of the 'Pagoda' observations, together with those of variation and inclination by Sir J. Ross, and the inclinations and intensities by Lieuts. Smith and Dayman.

"In calculating the intensities observed by Lieut. Smith, Hobarton has been taken as the base station, and the results by weights only used. The same has been done

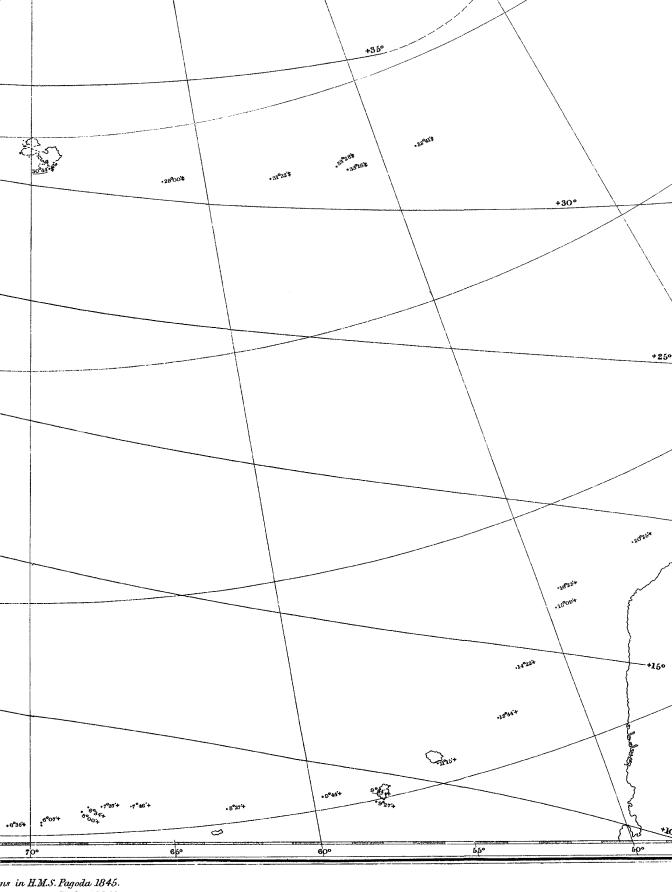




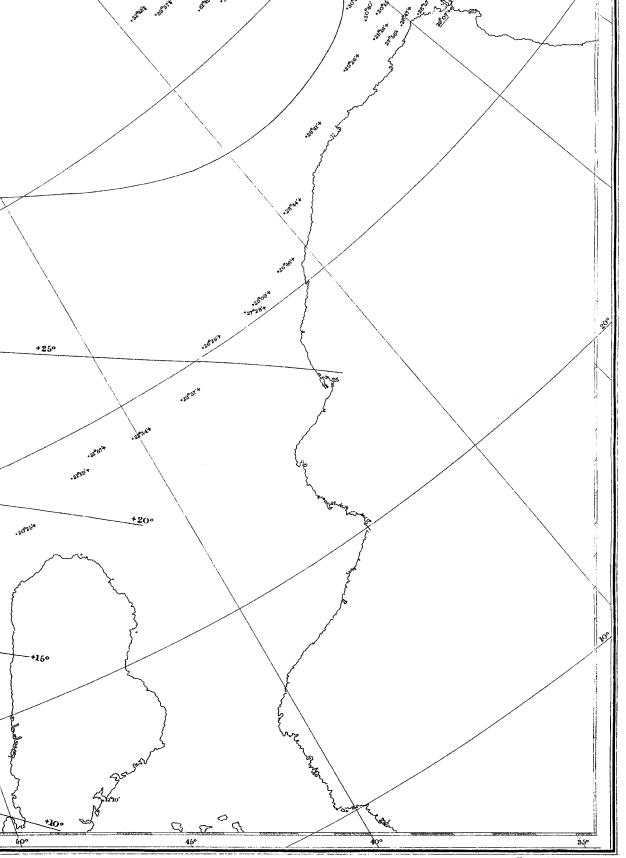




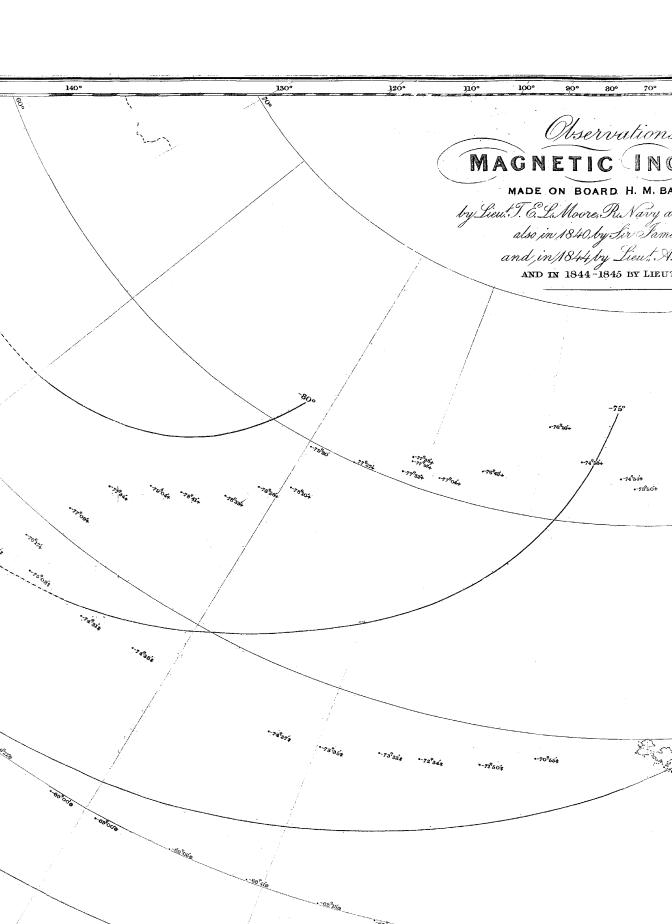
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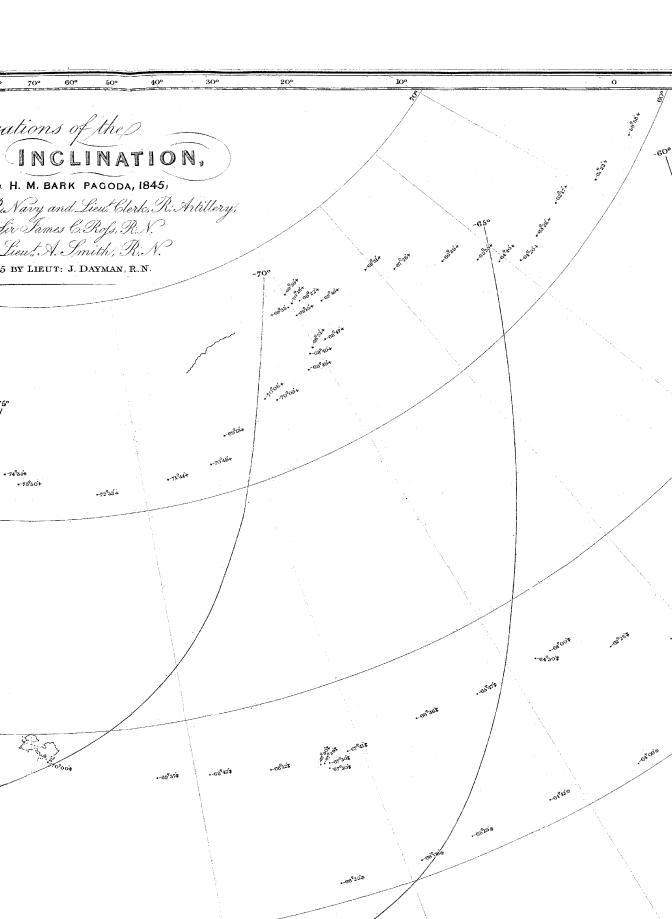


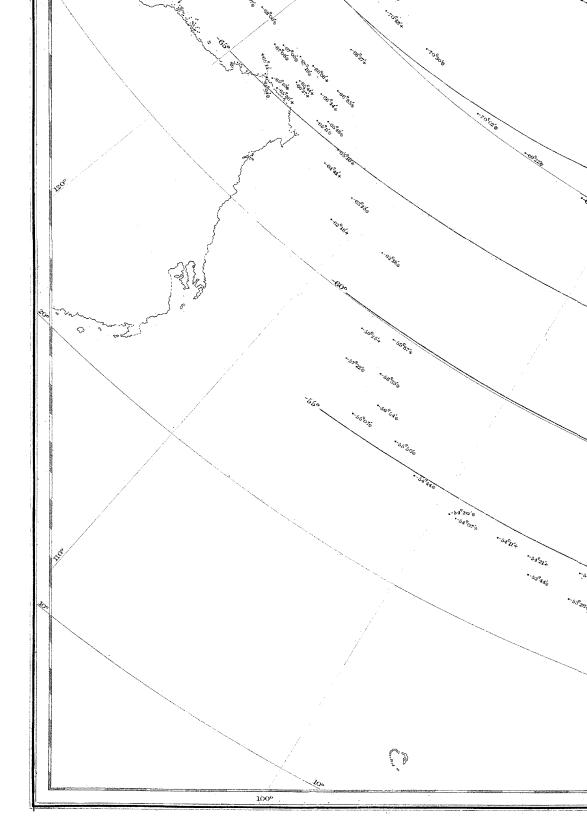
ns in H.M.S. Pagoda 1845.Erebus 1840.

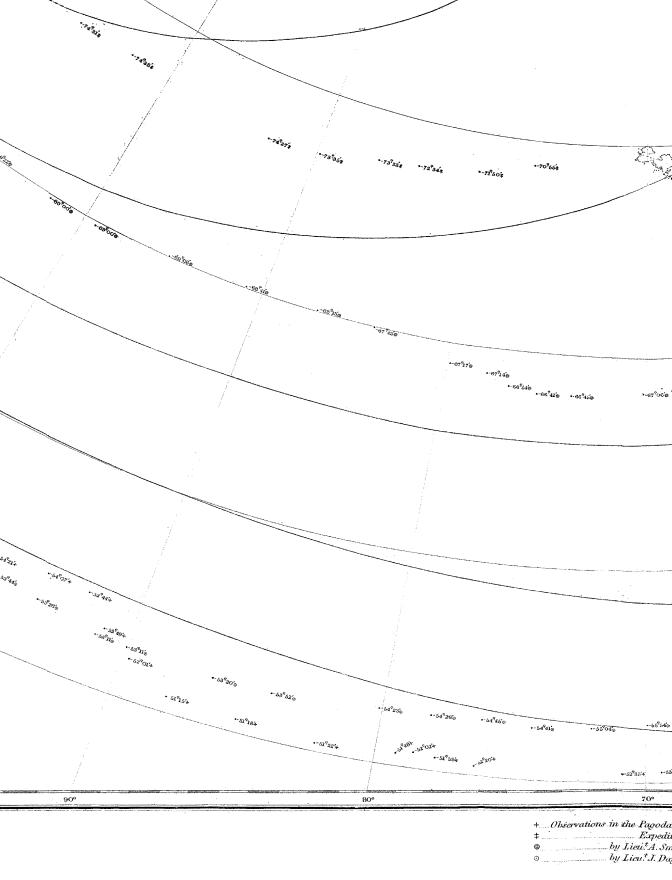


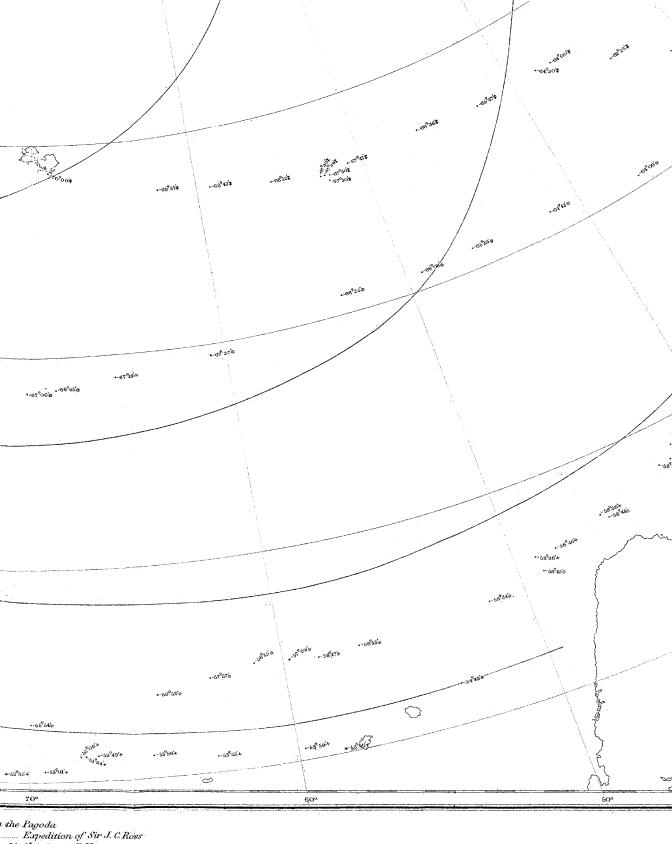
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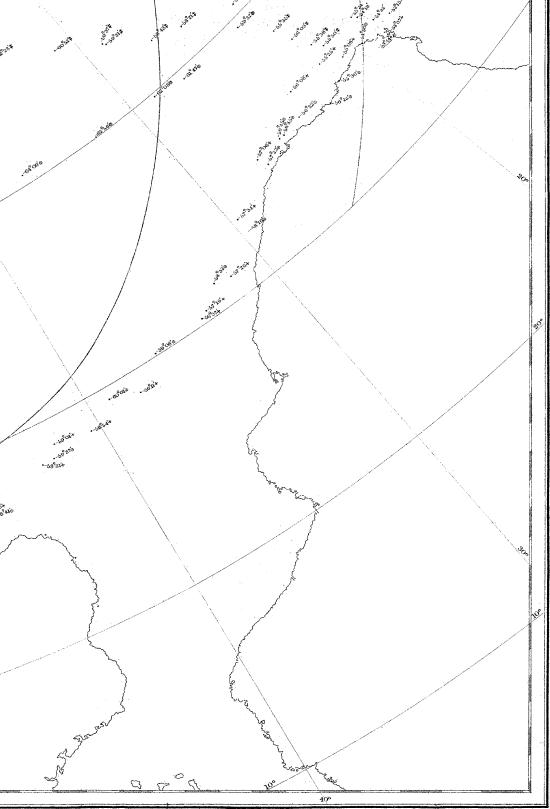




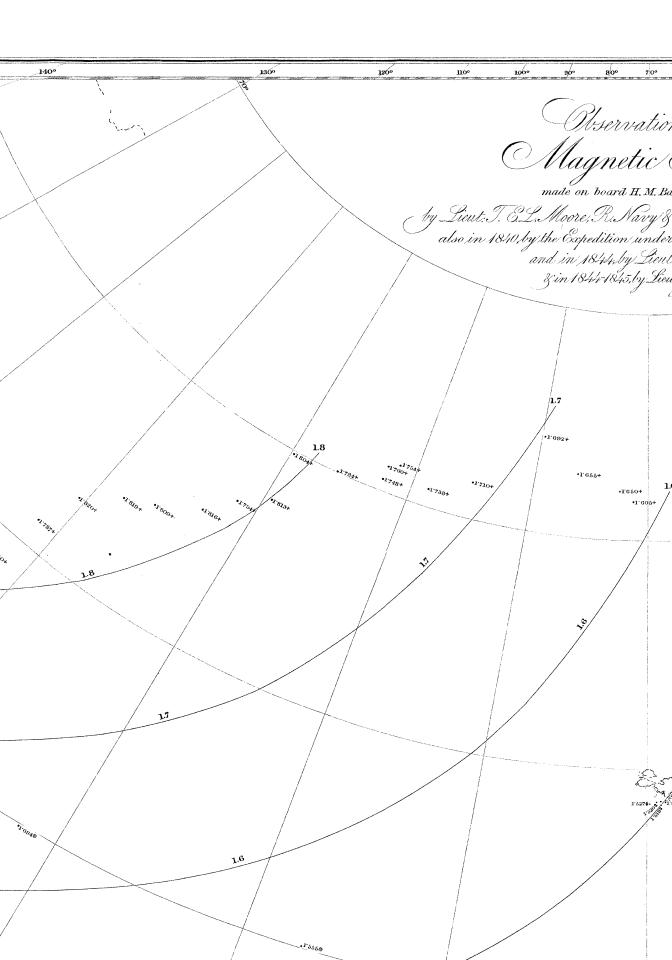


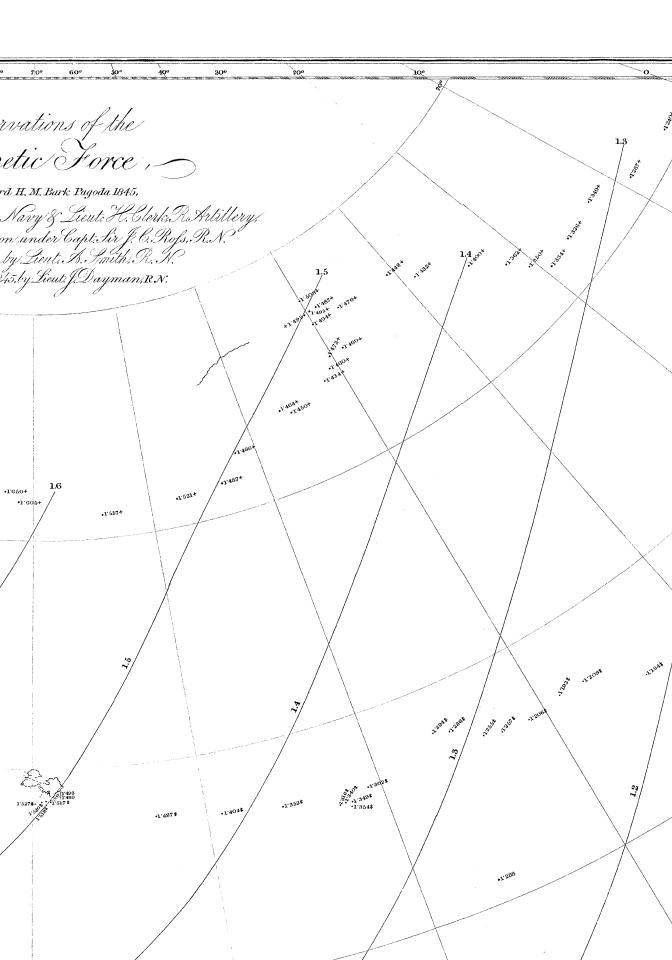


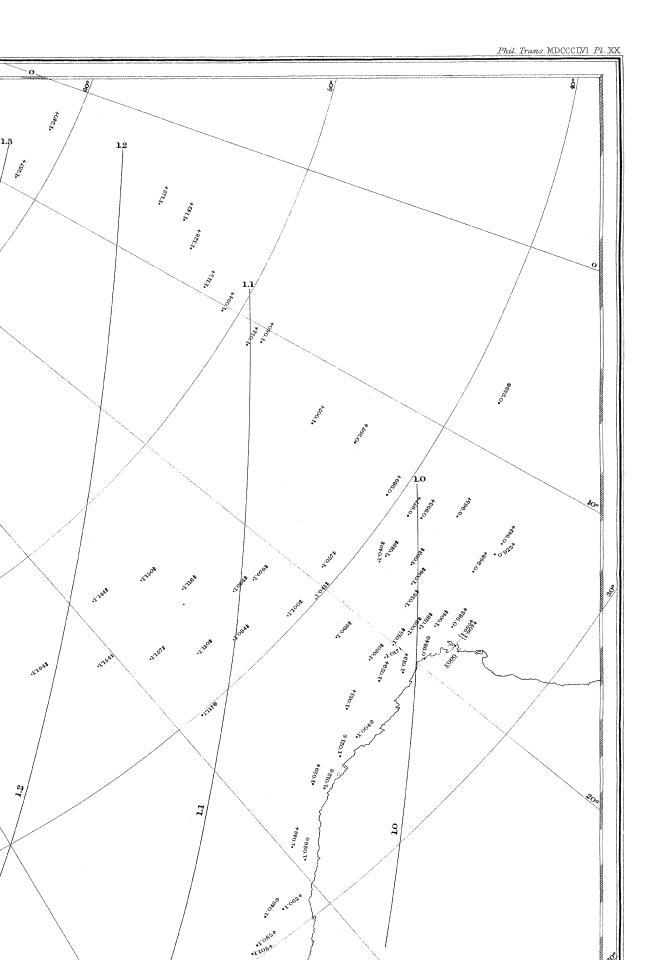
r the Pagoda ——Expedition of Sir J. C. Ross y Lieu[‡] A. Smith R.N. y Lieu[‡] J. Dayman R.N.

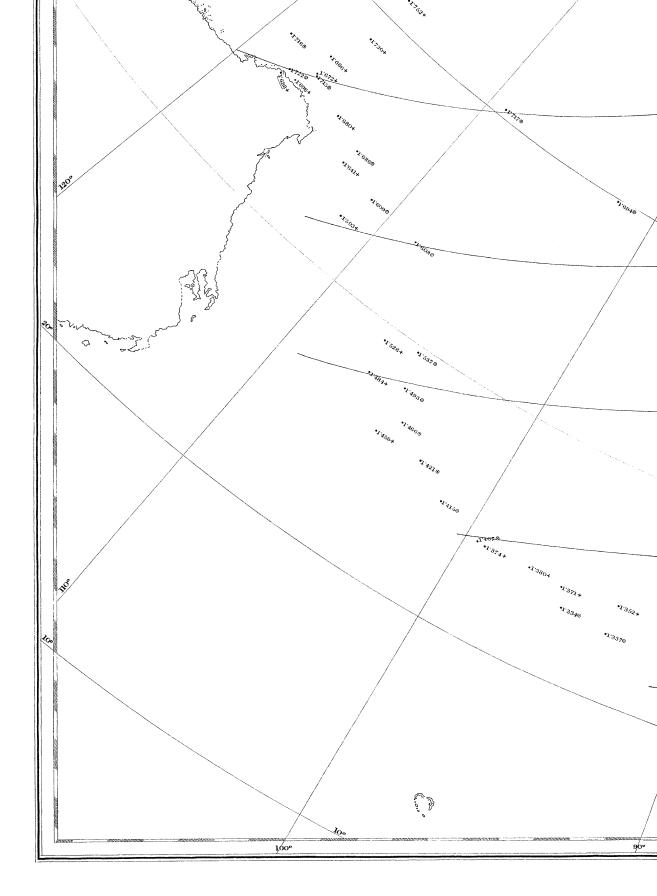


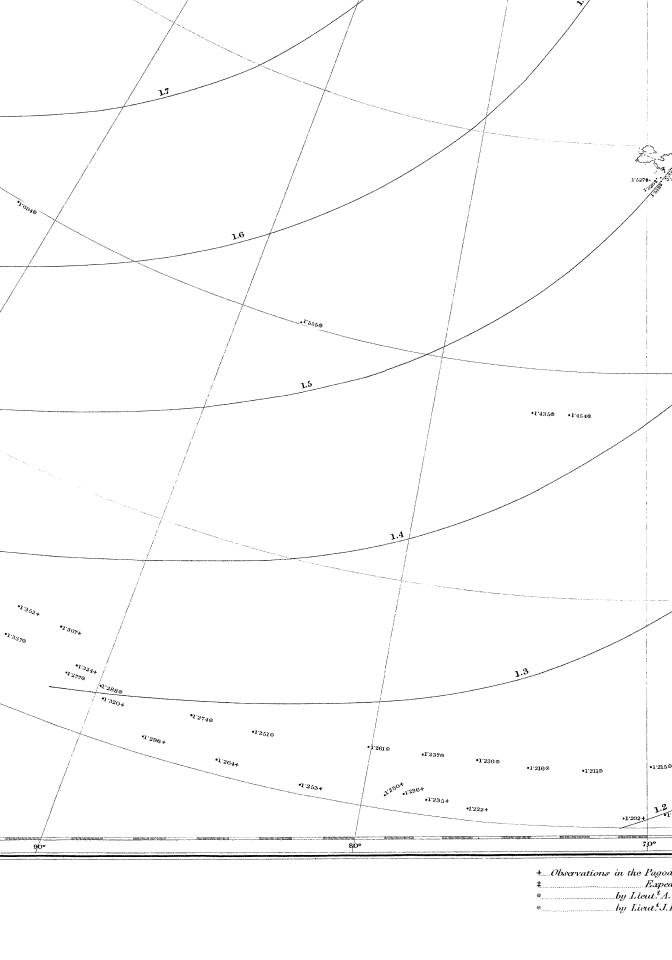
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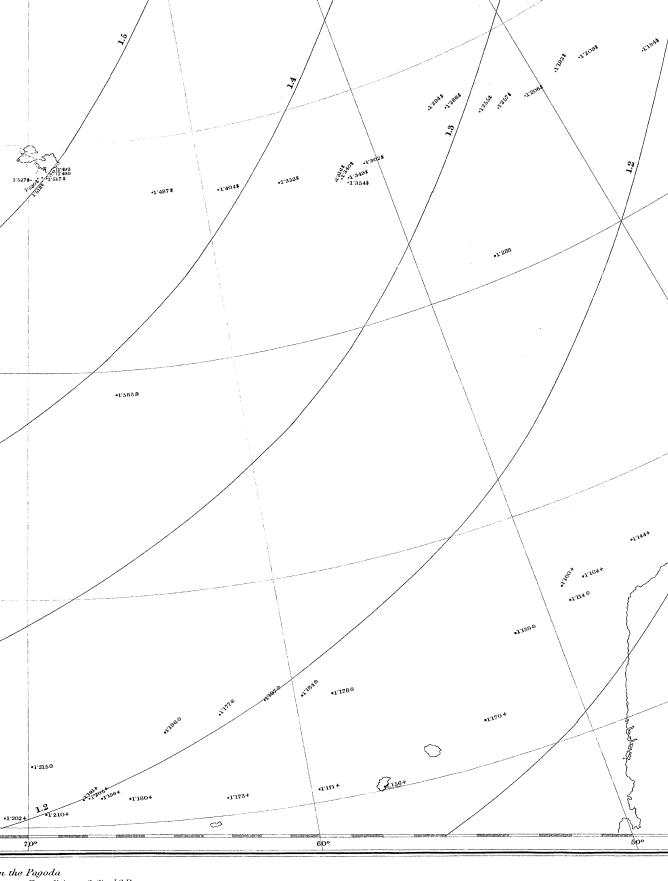




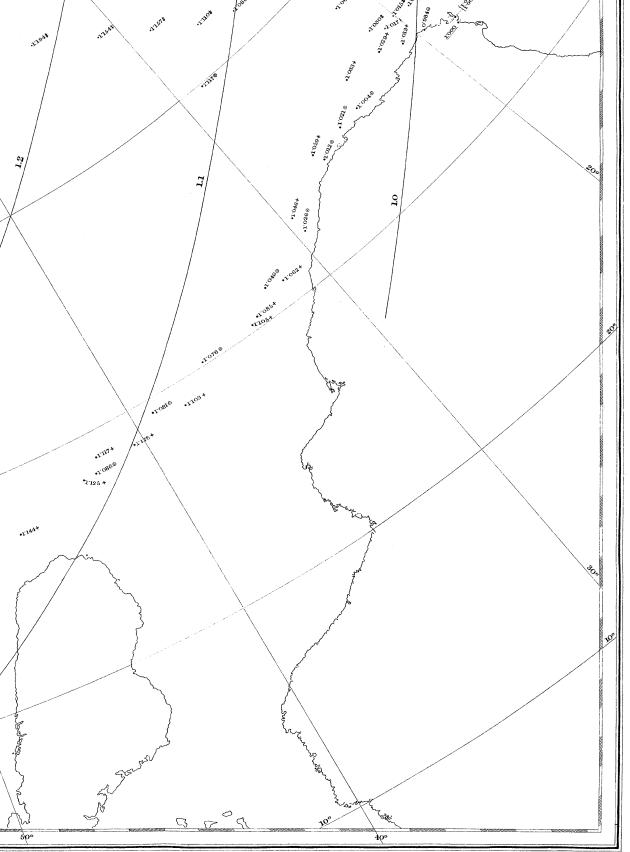








in the Pagoda ____Expedition of Sir J.C.Ross by Lieut.[‡]A.Smith R.N. by Lieut.[‡]J.Dayman R.N.



Engraved by J. & C. Walker.

with the series by Lieut. DAYMAN, the weights of two grains and three grains having been observed daily; the following observations with weights made at the observatory, Hobarton, give the formulæ for calculation:—

(II.) Lieut. Smith's.
$$\begin{cases}
2 \text{ grains } v = 10 & 33'; & I = 1.80; I' = .3296 \text{ cosec } v'. \\
3 \text{ grains } v = 16 & 05; & I = 1.80: I' = .4987 \text{ cosec } v'.
\end{cases}$$
(II.) Lieut. Dayman's.
$$\begin{cases}
1 \text{ grain } v = 5 & 19 \\
2 \text{ grains } v = 10 & 35 \\
3 \text{ grains } v = 16 & 20 \\
4 \text{ grains } v = 21 & 50 \\
5 \text{ grains } v = 27 & 41 \\
6 \text{ grains } v = 34 & 08
\end{cases}$$
From these we obtain the following values of v for 2 and 3 grains; viz.—

for 2 grains $v = 10 & 43'$.

for 3 grains $v = 16 & 11$.

Hence for 2 grains $I' = .3347$ cosec v' .

for 3 grains $I' = .5017$ cosec v' .

"In correcting these observations the same plan has been pursued as with the dip observations. As Lieut. Smith's observations required no correction in the latter case, so none has been applied to the intensities; and Lieut. Dayman's have been corrected from the same table as was used for the 'Pagoda' observations. No corrections have been applied for the effect of temperature; but they are probably so small as not to affect the results."

Observations of the Declination made on board Her Majesty's hired Bark "Pagoda," from the 10th of January to the 23rd of June 1845.

The Observers are distinguished as follows:—M. Lieut. Moore; B. Mr. Bodie, Master; Cl. Lieut. Clerk; Cm. Mr. Comber, Mate; T. Mr. Tufnell, and Bn. Mr. Burdon, Midshipmen. West Declination characterized by the sign +.

		Ì				-	Correct	tions.		
Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Ship's attraction.	Index.	Corrected Declination.	Remarks.
1845. Jan. 10 A.M.	$-3\overset{\circ}{4}\ 4\overset{\prime}{2} \\ -34\ 42 \\ -34\ 42$		М. М. М.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	W. W. W. ¹ / ₂ S.	$iggraphi -53 \ 15$	$+16 \\ +16 \\ +15$	+47	$\begin{vmatrix} +30 & 07 \\ +30 & 15 \\ +29 & 52 \end{vmatrix}$ $+29 & 51$	Card A.
11 ам.	$ \begin{array}{rrr} -34 & 42 \\ -35 & 26 \\ -35 & 26 \end{array} $	17 36	CL. CL. M. CL.	+28 06 $+27 31$ $+27 51$ $+27 43$	w. w.s.w. w.s.w. w.s.w.		$+16 \\ +11 \\ +11 \\ +11$	+47 +47 +47	$\begin{vmatrix} +29 & 09 \\ +28 & 29 \\ +28 & 49 \\ +28 & 41 \end{vmatrix} + 28 & 39$	Index correction +47' by observa- tions made at the observatory, Cape of Good Hope.
12 а.м.			M. B. B. B.	$ \begin{array}{r} +27 & 41 \\ +25 & 45 \\ +26 & 23 \\ +27 & 06 \end{array} $	s.w.byw. 1 w. w. by n. w. by n. w. by n.		$+10 \\ +03 \\ +03 \\ +03$	+47 + 47 + 47	$egin{pmatrix} +28 & 38 \ +26 & 35 \ +27 & 13 \ +27 & 56 \ \end{pmatrix} +27 & 15$	
13 A.M. 15 P.M.	$ \begin{array}{r} -35 & 10 \\ -35 & 10 \\ -38 & 43 \end{array} $	13 25 14 25	В. В. В. М.	$ \begin{array}{r} +24 & 37 \\ +25 & 04 \\ +24 & 38 \\ +24 & 22 \end{array} $	s.w. by w. s.w. by w. s.w. by w. s.s.w. $\frac{1}{2}$ w.		$ \begin{array}{r} +07 \\ +07 \\ +07 \\ \hline 00 \end{array} $	+47 +47 +47 +47	$ \begin{vmatrix} +25 & 31 \\ +25 & 58 \\ +25 & 32 \\ +25 & 09 \\ +25 & 09 \end{vmatrix} +25 & 09$. *
16 а.м. 16 р.м.	$ \begin{array}{rrr} -39 & 01 \\ -39 & 12 \\ -39 & 20 \end{array} $	14 45	М. См. М. М. В.	+27 13 +25 44 +27 48 +28 25	s.w. by w. $\frac{1}{2}$ w. s.w. by s. s.w. by s. s.w. by s.		+18 +06 +06 +06 +06	+47 +47 +47	$\begin{vmatrix} +28 & 18 \\ +26 & 37 \\ +28 & 41 \\ +29 & 18 \end{vmatrix}$	
	$\begin{array}{rrrr} -39 & 22 \\ -39 & 22 \\ -39 & 22 \\ -39 & 22 \\ -39 & 22 \\ -39 & 22 \end{array}$	14 25 14 25 14 25 14 25	B. B. B. B. B.	$\begin{vmatrix} +27 & 10 \\ +28 & 28 \\ +27 & 01 \\ +27 & 49 \\ +27 & 28 \\ +28 & 28 \end{vmatrix}$	s.w. by s. s.w. by s. s.w. by s. s.w. by s. s.w. by s.	>-54 13	$ \begin{array}{r} +06 \\ +06 \\ +06 \\ +06 \\ +06 \\ +06 \\ +06 \end{array} $	+ 47 + 47 + 47 + 47	$egin{array}{c ccccccccccccccccccccccccccccccccccc$	
17 а.м.	$ \begin{array}{rrr} -39 & 22 \\ -40 & 08 \\ -40 & 08 \\ -40 & 09 \end{array} $	14 25 14 32 14 32	См. В. В. М. Сг.	+26 26 +26 17 +25 18 +25 33 +26 56	s.w. by s. s.w. by w. s.w. by w. s.w. by w.		$+06 \\ +16 \\ +16 \\ +16 \\ +16 \\ +16$	+ 47 + 47 + 47 + 47	+27 19 +27 20 +26 21 +26 36 +27 59	
	-40 16 -40 18 -40 15	14 36 14 35 14 37 14 37	Т. Т. См. См.	+27 34 $+26 54$ $+27 04$ $+27 12$	s.w. by w. s.w. by w. s.w. by w. s.w. by w.	├ —55 05	$+16 \\ +16 \\ +16 \\ +16$	+47 +47 +47 +47	$egin{array}{c ccccccccccccccccccccccccccccccccccc$	
19 а.м.	$-44 45 \\ -44 45$	14 38 14 32 13 19 13 19	См. Т. М. Сь. М.	$\begin{array}{r} +26 & 00 \\ +26 & 00 \\ +27 & 57 \\ +25 & 09 \\ +23 & 05 \end{array}$	s.w. by w. s.w. by w. s.w. by w. s.s.w. $\frac{1}{2}$ w. s.s.w. $\frac{1}{2}$ w.		$+16 \\ +16 \\ +16 \\ +04 \\ +04$	+47 +47 +47 +47	+27 03 +27 03 +29 00 +26 00 +23 56 +26 34	Ship very unsteady;
20 л.м.	-46 24 $-46 24$	13 19 13 34 13 34 13 34	См. В. В.	$ \begin{array}{r} +27 & 40 \\ +27 & 00 \\ +24 & 51 \\ +24 & 31 \\ +25 & 02 \end{array} $	s.s.w. s.s.w. s.w. by w. s.w. by w. s.w. by w.		$+02 \\ +19$	+47 +47 +47	+28 29 +27 49 +25 57 +25 37 +26 08 +25 54	heavy sea.
22 а.м.	-48 27 -48 27 -48 27 -48 27	10 51 10 51	В. В. М. Ст.	$ \begin{array}{r} +23 & 08 \\ +22 & 41 \\ +24 & 40 \\ +24 & 54 \end{array} $	s.w. by s. s.w. by s. s.w. by s. s.w. by s.		+12 +12 +12 +12	+47 + 47 + 47	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	

			<u>;</u>				Correc	tions.		
Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Ship's attraction.	Index.	Corrected Declination.	Remarks.
1845. Jan. 23 а.м.	-50 30 $-50 31$	1	М. См.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	s.w. $\frac{1}{2}$ s. s.w. by s.	<u> </u>	+° 16 + 16	$+47 \\ +47$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
23 г.м.	-50 50	10 17	CL. M. CL. M.	$\begin{vmatrix} +24 & 27 \\ +23 & 18 \\ +21 & 09 \\ +23 & 14 \end{vmatrix}$	s.w. $\frac{1}{2}$ s. s.w.byw. $\frac{1}{2}$ w. s.w. by w.	-57 11	$\begin{vmatrix} + & 16 \\ + & 16 \\ + & 16 \end{vmatrix}$	+47 +47 +47	$\begin{vmatrix} +25 & 30 \\ +24 & 21 \\ +22 & 12 \end{vmatrix} + 23 & 55$	
24 A.M.	-5058 -5058	10 10 10 09	Сь. Т. В.	$\begin{vmatrix} +22 & 26 \\ +22 & 15 \\ +23 & 11 \end{vmatrix}$	s.w. s.w. s.w. s.w. by w.]]	$\begin{vmatrix} + & 16 \\ + & 16 \\ + & 16 \\ + & 25 \end{vmatrix}$	+47 +47	$egin{array}{c cccc} +24 & 17 \\ +23 & 29 \\ +23 & 18 \\ +24 & 23 \\ \hline \end{array}$	
24 p.m.	$ \begin{array}{rrr} -51 & 45 \\ -51 & 45 \\ -51 & 47 \\ -51 & 47 \end{array} $	9 34	М. Сь. См. См.	+22 00	s.w. by w. s.w. by w. s.w.byw.½w. s.w.byw.½w.	$\begin{vmatrix} -57 & 39 \\ 1 & 39 \end{vmatrix}$	+ 25 + 25 + 29 + 29	+47 + 47	$\begin{pmatrix} +21 & 18 \\ +22 & 10 \\ +23 & 16 \\ +25 & 06 \end{pmatrix}$	
	$ \begin{array}{r rrr} -51 & 47 \\ -51 & 47 \\ -51 & 45 \end{array} $	9 34 9 40 9 34	См. Вм. В.	$\begin{vmatrix} +24 & 04 \\ +22 & 50 \\ +23 & 11 \end{vmatrix}$	$\begin{array}{c} s.w.byw.\frac{1}{2}w.\\ s.w.byw.\frac{1}{2}w.\\ s.w.byw. \end{array}$		+ 29 + 29 + 25	$\begin{vmatrix} +47 \\ +47 \\ +47 \end{vmatrix}$	$egin{array}{cccc} +25 & 20 \\ +24 & 06 \\ +24 & 23 \\ \end{array}$	
		9 34 9 32	M. CL. CL. B.	$\begin{vmatrix} +20 & 06 \\ +20 & 58 \\ +22 & 46 \\ +21 & 49 \end{vmatrix}$	s.w. by w. s.w. by w. s.w. by w. s.w. by w.	$\left \begin{array}{c} -57 & 39 \end{array} \right $	1+ 26	5 + 47 $5 + 47$	$\begin{pmatrix} 1 + 21 & 18 \\ + 22 & 10 \\ + 23 & 58 \\ + 23 & 01 \end{pmatrix} + 23 \ 46$	Card A.
	$ \begin{array}{c cccc} -51 & 50 \\ -51 & 50 \\ -51 & 50 \end{array} $	9 32 9 31 9 31	B. CL. M. CL.	$\begin{vmatrix} +22 & 53 \\ +22 & 18 \\ +22 & 49 \end{vmatrix}$	s.w. byw. $\frac{1}{2}$ w. s.w. byw. $\frac{1}{2}$ w. s.w. byw. $\frac{1}{2}$ w.		+ 25 + 25 + 25	9 + 47 9 + 47 9 + 47	7 + 24 09 7 + 23 34 7 + 24 05	
25 A.M.	$ \begin{array}{r rrr} -51 & 50 \\ -51 & 50 \\ -52 & 45 \\ -53 & 00 \end{array} $	9 31 7 53 7 53	Т. М. См.	$\begin{vmatrix} +22 & 36 \\ +22 & 21 \\ +22 & 50 \end{vmatrix}$	s.w. by w. ½ w. s.w. by w. ½ w. s.w. by w. ½ w. s w. by w.	.IJ	+ 2: + 2: + 2: + 2:	$\begin{vmatrix} 9 + 4 \\ 9 + 4 \end{vmatrix}$	7 + 24 24 $7 + 23 52$ $7 + 23 37$ $7 + 24 02$ $+ 23 49$	3 Caral A
26 а.м	$ \begin{array}{r} -53 & 00 \\ -53 & 00 \\ -53 & 52 \\ -53 & 52 \end{array} $	7 53	См. См. М. В.	1 '	s.w. by w. s.w. by w. w. ½ N. w. ½ N.		+ 20 + 20 + 30 + 30	$5 + 47 \\ 6 + 59$	$7 + 23 ext{ } 18 $ $7 + 24 ext{ } 06$ $2 + 21 ext{ } 17$ $2 + 21 ext{ } 46$	Card A.
	-53 52 -53 52 -53 52	6 16 6 16 6 16	CL.	$\begin{array}{c} +20 & 56 \\ +20 & 24 \\ +20 & 36 \end{array}$	w. by s. w. by s. w. by s.		+ 3 + 3 + 3	3 + 59 $3 + 59$ $3 + 59$	$\begin{vmatrix} 2 + 22 & 21 \\ 2 + 21 & 49 \\ 2 + 22 & 01 \end{vmatrix}$	
26 р.м	$ \begin{array}{r rrr} -53 & 58 \\ -53 & 58 \\ -53 & 58 \\ \hline -53 & 58 \\ \end{array} $	6 16	См.	$+20 36 \\ +21 08$	w. by s. w. by s. E. $\frac{1}{2}$ s. E. $\frac{1}{2}$ s.	-57 00	1+ 9	$\begin{vmatrix} 3 + 59 \\ 2 + 59 \end{vmatrix}$	$\begin{vmatrix} 2 & +22 & 53 \\ 2 & +22 & 01 \\ 2 & +20 & 38 \\ 2 & +21 & 08 \end{vmatrix} + 21 3$	4 Card J. Compass steady. Index correction +52' by observa- tions made at the
0.5	$ \begin{bmatrix} -53 & 58 \\ -53 & 58 \\ -53 & 58 \end{bmatrix} $	6 06 6 06 6 06	CL. CL. M.	$\begin{vmatrix} +20 & 54 \\ +20 & 53 \\ +22 & 03 \end{vmatrix}$	N.E. N. E. ½ S.		$\begin{bmatrix} -1 & 1 \\ - & 5 \\ -1 & 2 \end{bmatrix}$	7 + 59 + 59 + 59 + 59	$egin{array}{c ccc} 2 + 20 & 29 \ 2 + 20 & 54 \ 2 + 21 & 33 \ \end{array}$	Magnetic Observatory, Cape of Good Hope.
4	-55 13 -55 30 -55 48 -58 53	5 54 5 5 50	M. M.	1 .	s.w. by s. $\frac{1}{2}$ s s.s.w. $\frac{1}{2}$ w. s.w. by s. s.w. $\frac{1}{2}$ s.		$\begin{vmatrix} + & 1 \\ + & 1 \end{vmatrix}$	$\begin{vmatrix} 0 \\ +5 \\ 2 \\ +5 \end{vmatrix}$	2 + 21 00 $2 + 22 16 $ $2 + 22 52 $ $2 + 20 52 $ $2 + 17 18$	3 Card unsteady.
29 р. м	-5853 -5913	3 4 00	M.	$ +15 \ 36$	s.w. by s. s.w. $\frac{1}{2}$ s.	-59 0	$\begin{vmatrix} + & 1 \\ + & 1 \end{vmatrix}$	$\begin{vmatrix} 9 + 5 \\ 9 + 5 \end{vmatrix}$	$\begin{vmatrix} 2 & +14 & 56 \\ 2 & +16 & 47 \end{vmatrix} + 17 = 3$	O Card unsteady.
31 A.M	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	8 18 8 9 05	В. См	$+20 \ 32$	s.w. $\frac{1}{2}$ s. E. $\frac{1}{2}$ s. s.e. by s. s.e. by s.		$\begin{bmatrix} -1 & 4 \\ - & 4 \end{bmatrix}$	$\begin{vmatrix} 7 + 5 \\ 8 + 5 \end{vmatrix}$	2 + 20 59 2 + 21 40 2 + 20 36 2 + 19 31	
31 P.M	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	8 9 05 5 9 30	CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.e. by s. s.e. s.e. s.s.e. ½ E.	$\left \right _{-61}$ 3	$\begin{bmatrix} - & 4 \\ -1 & 0 \\ -1 & 0 \end{bmatrix}$	$\begin{vmatrix} 8 + 5 \\ 1 + 5 \\ 1 + 5 \end{vmatrix}$	$\begin{vmatrix} 2 & +19 & 47 \\ 2 & +20 & 22 \\ 2 & +20 & 59 \end{vmatrix} + 20 \ 2$	9 Unsteady,
	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	0 10 07 0 10 07 0 10 07 0 10 07	CL	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E.		- 3 - 3	$\begin{vmatrix} 1 + 5 \\ 1 + 5 \end{vmatrix}$	2 + 21 37 $2 + 20 49 $ $2 + 19 44 $ $2 + 19 42$	

			ដ		:		Correct	ions.		
Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Ship's attrac- tion.	Index.	Corrected Declination	. Remarks.
1845. Feb. 1 A.M. 1 P.M.		12 45 12 55 12 55	См. В. Сь.	$\begin{array}{r} +22 & 21 \\ +20 & 12 \end{array}$	s.e. by s. s.e. by s. s.e. by s.		- 48 - 48 -1 04	$+52 \\ +52 \\ +52$	+20 00	7 Very unsteady.
2 A.M. 2 P.M.	$\begin{array}{rrrr} -61 & 54 \\ -61 & 54 \\ -61 & 55 \\ -61 & 54 \\ -61 & 54 \end{array}$	16 34 16 38 16 40 16 42 16 57	B. M. M. T. CL. B.	+22 55 +25 19 +26 34 +23 04 +21 28 +21 36	E.N.E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. by E. S.E. $\frac{1}{2}$ E.	-63 28	-1 10 -1 10 -1 10 -1 18 -1 10	$+52 \\ +52 \\ +52 \\ +52 \\ +52 \\ +52$	$ \begin{vmatrix} +21 & 47 \\ +25 & 01 \\ +26 & 16 \\ +22 & 46 \\ +21 & 02 \\ +21 & 18 \\ +19 & 54 \end{vmatrix} $	l Unsteady.
3 А.М.	$ \begin{bmatrix} -61 & 54 \\ -61 & 54 \\ -61 & 49 \\ -61 & 50 \\ -61 & 50 \\ -61 & 50 \\ -61 & 50 \\ -61 & 50 \\ -61 & 50 $	16 57 19 15 19 15 19 15 19 06 19 12 19 13	Bn. T. Bn. Cm. B. M. M. M.	+20 12 +27 44 +27 56 +25 32 +27 32 +27 19 +27 41 +27 43 +27 15	S.E. \(\frac{1}{2}\) E. S.E. \(\frac{1}{2}\) E. E.S.E. S.E. by E. \(\frac{1}{2}\) E. S.E. by E. \(\frac{1}{2}\) E. E.S.E. E.S.E. E.S.E. E.S.E. E. by S.	\right\}-64 20	-1 10 -1 44 -1 36 -1 36 -1 44 -1 44	+52 $+52$ $+52$ $+52$ $+52$ $+52$ $+52$	+27 26 +27 04 +24 48 +26 48 +26 27	4 A less delicate point was used for the suspension of the
3 р.м.	$\begin{bmatrix} -61 & 50 \\ -61 & 50 \end{bmatrix}$	19 13 19 13 19 13 19 14 19 14 19 14	CL. BN. M. CL. CL.	$ \begin{array}{r} +27 & 13 \\ +27 & 56 \\ +27 & 59 \\ +27 & 32 \\ +26 & 52 \\ +24 & 05 \\ +23 & 31 \\ +23 & 24 \end{array} $	E.S.E. E.S.E. N.E. by N. N.W. ½ W. W. by N. W. by S.		$ \begin{vmatrix} -1 & 44 \\ -1 & 44 \\ -1 & 34 \\ + & 21 \\ +1 & 00 \end{vmatrix} $	+52 $+52$ $+52$ $+52$ $+52$ $+52$ $+52$	$\begin{array}{c} +25 & 04 \\ +27 & 04 \\ +27 & 07 \\ +26 & 40 \\ \end{array}$ $\begin{array}{c} +26 & 10 \\ +25 & 18 \\ +25 & 23 \\ +25 & 26 \\ \end{array}$	compass-card, which made it much steadier.
	$ \begin{array}{r rrr} -61 & 50 \\ -61 & 50 \\ -61 & 50 \\ -61 & 50 \\ -61 & 50 \\ -61 & 50 \\ -61 & 50 \end{array} $	19 14 19 14 19 14 19 14 19 14 19 14 19 14	CL. B. CL. CL. M. M.	+23 31 +24 37 +25 37 +24 52 +24 00 +24 06 +23 51	w.s.w. n.w. by w. n.w. n.w. w. by n. w. w.	-64 20	+1 07 + 29 + 12 + 12 +1 00 +1 13 +1 13	+52 $+52$ $+52$ $+52$ $+52$ $+52$ $+52$	$egin{array}{c cccc} +25 & 30 \\ +25 & 58 \\ +26 & 41 \\ +25 & 56 \\ +25 & 52 \\ +26 & 11 \\ +25 & 56 \\ \hline \end{array} > +26 \ 1$	6 Card steady. Being a calm the decli- nations were ob- served on different points of the com-
.4 а.м.	$\begin{array}{c cccc} -61 & 50 \\ -61 & 50 \\ -61 & 50 \\ -61 & 50 \\ -61 & 50 \\ -61 & 50 \\ -62 & 00 \\ -62 & 00 \end{array}$	19 14 19 14 19 14 19 14 19 14 20 55	M. M. M. M.	+25 46 +23 53 +28 55 +25 55 +24 45* +27 03 +25 36 +26 09	W.S.W. S.W. S.S.E. S. $\frac{1}{2}$ E. In the boat. S. by E. S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E.		+ 48 - 35 - 11 - 19 - 11	+52 $+52$ $+52$ $+52$ $+52$ $+52$	+27 45 +25 33 +29 12 +26 36 +25 37 +27 36 +26 17 +26 50	pass to obtain the effect of the ship's iron. The compass was afterwards placed in a copper-fastened boat and the declination observed at a distance from the ship.
4 P.M.	$\begin{array}{cccc} -62 & 00 \\ -62 & 05 \\ -62 & 07 \\ -62 & 10 \\ -62 & 10 \\ -62 & 10 \\ -62 & 10 \end{array}$	20 37 20 58 21 04 21 03 21 03 21 03	M. M. CL. CL.	$\begin{array}{c} +26 & 59 \\ +26 & 59 \\ +29 & 02 \\ +27 & 14 \\ +28 & 15 \\ +28 & 16 \\ +30 & 14 \\ +27 & 26 \\ \end{array}$	S. ½ E. S.S.E. ½ E. S.S.E. S.S.E. S.S.E. S.S.E. S.S.E. S.S.E.	>-64 40	_ 11 _ 44 _ 35 _ 35 _ 35 _ 35	+52 $+52$ $+52$ $+52$ $+52$ $+52$ $+52$	$\begin{vmatrix} +27 & 40 \\ +29 & 10 \end{vmatrix}$	5 Compass steady.
	$\begin{array}{r} -63 & 14 \\ -63 & 18 \\ -63 & 18 \\ -63 & 18 \\ -63 & 18 \\ -63 & 19 \end{array}$	21 10 21 10 21 10 21 10 21 10 21 10	M. M. CL. Bn. T.	$\begin{array}{c} +27 & 26 \\ +29 & 01 \\ +28 & 51 \\ +27 & 08 \\ +28 & 47 \\ +28 & 08 \\ +28 & 14 \\ \end{array}$	s. by E. s. by E. s. ½ E.		_ 19 _ 19 _ 11 _ 11 _ 11	$+52 \\ +52 \\ +52 \\ +52 \\ +52$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6 Steady.

^{*} This observation is not much to be depended on, as the compass was very unsteady and difficult to observe.

			Ŀ				Correc	tions.		
Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Ship's attraction.	Index.	Corrected Declination.	Remarks.
1845. Feb. 6 а.м.	-6406		В.	+28 41	S.S.E.	٦ ° ′	_° 42		+28 517 ° ′	
	-64 18 $-64 18$ $-64 20$	24 05	CL. CL. M.	$\begin{vmatrix} +28 & 29 \\ +29 & 44 \\ +29 & 57 \end{vmatrix}$	S.S.E. S.S.E. S.S.E.	N .	- 42	+52	$egin{array}{c c} +28 & 39 \\ +29 & 54 \\ +30 & 07 \\ \hline \end{array}$	
6 р.м.	-64 25 $-64 35$ $-64 38$	26 30	M. Cl. Cl.	$+28 \ 43$	s.s.e. $\frac{1}{2}$ e. s.e. by s. $\frac{1}{2}$ s. s.s.e.	}−66 39	-48 -50	$+52 \\ +52$	$\begin{vmatrix} +28 & 47 \\ +31 & 45 \\ +31 & 32 \end{vmatrix}$	Card steady.
7	-64 38 -64 25 -65 30	26 35 26 28	Bn. M.	$+3239 \\ +3106$	S.S.E. S.S.E. ½ E.		4248	$+52 \\ +52$	$\begin{bmatrix} +32 & 49 \\ +31 & 10 \end{bmatrix}$	
A.M.	-65 25 $-65 16$	27 45 27 45	B. Cl.	+32 02 +32 46 +30 41 +37 36	s.e. by s. s.s.e. s.s.e. ½ e.		-42 -52	$ +52 \\ +52$	$ \begin{array}{r} +31 & 51 \\ +32 & 56 \\ +30 & 41 \end{array} $	
7 г.м.	-65 16 $-66 02$	29 05	В.	+31 16 $+31 51 $ $+31 12$	S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E.	-67 28	- 52 - 18	$+52 \\ +52$		Compass steady.
	-66 02 $-66 02$	29 05 29 05	В.	+30 11 $+30 25$ $+31 08$	S. ½ E. S. ½ E. S. ½ E.		- 18 - 18	+52 + 52	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
9 р.м.	$ \begin{array}{rrr} -66 & 02 \\ -66 & 02 \\ -66 & 26 \end{array} $	29 05	B _N . C _L . C _L .	$+31 00 \\ +31 49 \\ +36 04$	S. ½ E. S. ½ E. S.E. by E.	<u>}</u>	- 18	+52	$+31 \ 34$ $+32 \ 23$ $+35 \ 48$:
10 а.м.	-66 26	37 25 37 25 38 32	B _N . M. B.	$+35 08 \\ +36 34 \\ +37 20$	s.e. by e. s.e. by e. s. by w. ½ w.	$-68 \ 49$	-1 08 + 32	$+52 \\ +52$	+3452 $+3539$ $+3618$ $+3844$	Steady.
10 p.m.	-67 03	38 32 38 32 38 32	B _N .	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.S.W. $\frac{1}{2}$ W. S.S.W. $\frac{1}{2}$ W.	-69 22	+ 52	+52	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Steady.
11 а.м.		38 32 39 41 39 41	CL.	+39 35	N. by w. E. E. by s.]	-246	$+52 \\ +52$	+3951 $+3812$ $+3833$	
	-67 34 $-67 34$	39 41 39 41 39 41	CL.	+39 26 +36 03 +37 37	E. by s. s.w. by s. s.	-69 38	$-2 & 30 \\ +1 & 00$	$+52 \\ +52$	$\begin{vmatrix} +37 & 48 \\ +37 & 55 \\ +38 & 31 \end{vmatrix}$	Card steady.
12 A.M.	$ \begin{array}{r} -67 & 34 \\ -67 & 38 \end{array} $	39 41 39 41 39 23	Сь.	+38 57 +37 49 +37 23	N.N.E. S. ½ E. N. by E.		$-1 & 40 \\ - & 15$	$+52 \\ +52$	$ \begin{array}{r} +38 & 09 \\ +38 & 26 \\ +36 & 50 \end{array} $	
	-66 38	39 23 39 20	CL. M.	+39 04 +35 56	S.S.E. S.S.E.	$-70 \ 16$	45 45	$ +47 \\ +47$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Card A. unsteady.
	-67 06 $-67 06$	40 03 40 03	Сь. Т.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.E. $\frac{1}{2}$ E. N.E. by E. N.E. by E.	$-69 \ 35$	-2 26 $-2 26$	$+52 \\ +52$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Card J. steady.
	$ \begin{array}{rrrr} -67 & 06 \\ -67 & 06 \\ -67 & 01 \end{array} $	40 03 40 30	B. B.	+3553	n.e. by e. n.e. by e. ½ e. n.n.e.	$\left. \begin{array}{c} \\ \\ \\ \\ \end{array} \right\} = 69 \ 15$	-2 32 $-1 35$	$+52 \\ +52$	$\begin{array}{c c} +36 & 29 \\ +36 & 45 \\ \hline +35 & 10 \\ +20 & 12 \\ \end{array}$	Very unsteady.
16 а.м.	$ \begin{array}{rrrr} -67 & 01 \\ -64 & 52 \\ -64 & 52 \\ 64 & 52 \end{array} $	38 35 38 35	M. CL.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.N.E. $\frac{1}{2}$ E. s. by E. N.N.E.		- 22 -137	+52 +52	$+36 \ 41$ $+40 \ 51$	Compass unsteady.
	$ \begin{array}{rrrr} -64 & 52 \\ -64 & 52 \\ -64 & 52 \end{array} $	38 37 38 37	T. Bn.	$+35 \ 44 \\ +36 \ 06 \\ +36 \ 31$	s.e. e.s.e. s.e. by e.	$\left.\right\}$ -68 47	-2 03 $-1 46$	$+52 \\ +52$	$+3455 \\ +3537$	compass unstrany.
17 р.м.	-6452 -6452	40 12	Bn. M.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.S.E. S.S.E. S.S.E.		- 44 - 44	$+52 \\ +52$	+37 087 $+35 36$ $+37 49$ $+36 54$	Steady.
	$ \begin{array}{r} -64 & 52 \\ -64 & 52 \\ -64 & 52 \end{array} $	40 12		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.s.e. s.e. by s. s.e. by s.		-106	+52	$ \begin{array}{c c} +38 & 28 \\ +37 & 40 \\ +34 & 40 \end{array} $, '

Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Corrections. Ship's sattraction.	Corrected Declination.	Remarks.
1845. Feb. 18 а.м.	$-6\overset{\circ}{4} \overset{\circ}{22} \\ -64 \overset{\circ}{22}$	40° 49° 40° 49°		$+38\ 35\ +34\ 41$	s. by E. $\frac{1}{2}$ E. N. by E. $\frac{1}{2}$ E.	$\left.\right\} - 68 $	-32 + 59	$\begin{pmatrix} 2 + 38 & 55 \\ 2 + 34 & 09 \end{pmatrix} + 36 & 32 \end{pmatrix}$	Very unsteady.
19 р.м.	$ \begin{array}{r rrrr} -63 & 58 \\ -63 & 58 \\ -63 & 56 \end{array} $	41 25 41 25	CL. Bn.	+38 43 +38 20	s.e. by e. ½ e. e.s.e.	$\left.\right\}_{-69}^{2}$	$\begin{vmatrix} -2 & 04 \\ -2 & 15 \\ +5 \end{vmatrix}$	$\begin{pmatrix} 2 + 37 & 31 \\ 2 + 36 & 57 \end{pmatrix} + 37 & 34$	Very unsteady.
20 а.м.	$\begin{bmatrix} -63 & 24 \\ -63 & 24 \end{bmatrix}$	44 47 45 32		$+40 08 \\ +41 03$	E. by s. s.e. by s. s.e. by e. ½ e.		$\begin{vmatrix} -2 & 30 \\ -1 & 08 \\ -2 & 04 \\ +59 \end{vmatrix}$	$\begin{bmatrix} +39 & 52 \\ +39 & 51 \end{bmatrix}$	
20 р.м.	-63 19	45 32 45 52	См. М.		s.e. by e. $\frac{1}{2}$ e. s.e. by e. $\frac{1}{2}$ e. s.e. by e.	}−70 09	$\begin{vmatrix} -2 & 04 & +5 \\ -1 & 54 & +5 \end{vmatrix}$	$\begin{vmatrix} +38 & 27 \\ 2 & +38 & 48 \end{vmatrix}$	Unsteady.
21 а.м.	-63 34	46 48 46 48	Cr.	$\begin{vmatrix} +39 & 46 \\ +39 & 00 \end{vmatrix}$	s.e. by s. E. by s. ½ s. s.s.e.			2 + 38 10 2 + 39 03	
21 р.м.	-63 41	47 03 47 24	М. В.	$\begin{vmatrix} +39 & 20 \\ +40 & 22 \\ +42 & 45 \end{vmatrix}$	S.S.E. S.E. $\frac{1}{2}$ S. S.E.	 	$\begin{vmatrix} -1 & 01 + 5 \\ -1 & 37 + 5 \end{vmatrix}$	2 + 42 00	Card steady.
22 p.m.		47 24 49 29		$+41 50 \\ +35 00$	S.E. S.E. S.S.W. ½ W.			2 + 41 05 2 + 36 43 $+ 30 91$	Very unsteady.
25 а.м.	-61 36 $-61 36$	52 56	М. В. Ст.	, -	s. by E. E. ½ N. E.		$ \begin{array}{r rrrr} & 24 + 5 \\ & 2 & 51 + 5 \\ & 2 & 57 + 5 \end{array} $	2 + 41 59 $2 + 39 04$ $2 + 39 35$	
25 р.м.	_61 30	53 43 55 13	Bn. M. Cl.	$+40 \ 31 \\ +43 \ 14$	s.e. by e. s.e. by s.	$-70 \ 48$	$\begin{bmatrix} -2 & 00 + 5 \\ -1 & 13 + 5 \end{bmatrix}$	$\begin{vmatrix} +39 & 23 \\ 2 & +42 & 53 \end{vmatrix}$	Card steady.
26 а.м.	-61 19	56 52 57 26	М. В. М.	$\begin{array}{r} +42 & 44 \\ +43 & 56 \end{array}$	S.E. $\frac{1}{2}$ E. S. S.E. $\frac{1}{2}$ E.		$ -1 \ 57 + 5$	2 + 43 39 2 + 42 51	
26 p.m.	-61 17	57 18 58 30	M. CL. CL.	$ \begin{array}{r} +42 & 00 \\ +42 & 11 \\ +43 & 29 \end{array} $	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E.	├ —71 44	$\begin{vmatrix} -1 & 57 + 5 \\ -1 & 46 + 5 \end{vmatrix}$	$\begin{vmatrix} 2 & +41 & 06 \\ 2 & +42 & 35 \end{vmatrix}$	Very unsteady.
27 A.M.	-61 02	62 55 62 55			S.E. $\frac{1}{2}$ E. E. S.E. $\frac{1}{2}$ S.	$\begin{bmatrix} \\ \\ \\ -72 & 53 \end{bmatrix}$	$\begin{vmatrix} -1 & 57 + 5 \\ -3 & 21 + 5 \\ -1 & 40 + 5 \end{vmatrix}$	2 + 43 39 2 + 45 14	Very unsteady.
27 p.m. 28 p.m.	_61 43	65 00 69 36	M. CL. M.	$\begin{vmatrix} +47 & 17 \\ +45 & 48 \\ +46 & 00 \end{vmatrix}$	S.E. ½ S. S.S.E. S.S.E.		$ -1 \ 40 + 5$	2 + 46 29 2 + 45 44	
March 1 A.M. 1 P.M.	$ \begin{array}{rrr} -62 & 10 \\ -62 & 10 \end{array} $	72 24 72 25	Сь. Т. М.	$\begin{vmatrix} +46 & 09 \\ +46 & 04 \\ +46 & 19 \end{vmatrix}$	S.S.E. S.S.E. S.S.E. ½ E.		$\begin{vmatrix} -1 & 02 + 5 \\ -1 & 02 + 5 \\ -1 & 19 + 5 \end{vmatrix}$	$2 + 45 54 \\ 2 + 45 52$	
	-62 10 $-62 10$	72 26 72 26 72 26	CL.	$\begin{vmatrix} +47 & 55 \\ +46 & 07 \\ +46 & 12 \end{vmatrix}$	s.E. by E. s.s.E. $\frac{1}{2}$ E. s.s.E. $\frac{1}{2}$ E.	 }−74 34	$\begin{vmatrix} -1 & 19 + 5 \\ -1 & 19 + 5 \end{vmatrix}$	2 + 45 45	Compass steady.
2 л.м.	-62 36 $-62 43$	76 05	В. М.	$\begin{vmatrix} +47 & 31 \\ +50 & 57 \\ +49 & 39 \end{vmatrix}$	s.E. by s. s. $\frac{1}{2}$ E. s. $\frac{1}{2}$ E.		$\begin{vmatrix} - & 10 + 5 \\ - & 10 + 5 \end{vmatrix}$	$egin{array}{cccc} 2 + 46 & 46 \ 2 + 51 & 39 \ 2 + 50 & 21 \ \end{array}$	
Permitted and Control of the Control	-6243	76 05 76 05	CL. CL. CM.	$\begin{vmatrix} +49 & 31 \\ +49 & 10 \\ +49 & 50 \end{vmatrix}$	s. by E. s. by E.		$\begin{vmatrix} + & 28 + 5 \\ - & 28 + 5 \end{vmatrix}$	$2 + 4955 \ 2 + 5010 \ 2 + 5014$	
2 г.м.	$\begin{bmatrix} -62 & 46 \\ -62 & 46 \end{bmatrix}$	76 50 76 50	CL.	$\begin{vmatrix} +49 & 52 \\ +48 & 18 \\ +48 & 37 \end{vmatrix}$	S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E. S. $\frac{3}{4}$ E.	-74 58	$\begin{bmatrix} - & 10 + 5 \\ - & 19 + 5 \end{bmatrix}$	$2 + 49 00 \ 2 + 49 10$	Card steady.
	_62 54	76 59 76 59 76 59		$ \begin{array}{r} +50 & 33 \\ +50 & 17 \\ +51 & 31 \end{array} $	s. s.		+ 08 + 5	$ \begin{array}{c cccc} 2 + 51 & 33 \\ 2 + 51 & 17 \\ 2 + 52 & 31 \end{array} $	

Date Lat Long E Declination observed. Ship's head. Inclination				#				Correc	tions.		
March 4 A.M.	Date.	Lat.	Long.	Observe		Ship's head.	Inclination.	attrac-	Index.	Corrected Declination.	Remarks.
5 A.M61 41 84 50 M. +50 48 Sec. \(\frac{1}{2} \) 84 50 M. +40 48 Sec. \(\frac{1}{2} \) 84 50 M. +46 36 Sec. \(\frac{1}{2} \) 84 50 Cc. +52 14 Sec. \(\frac{1}{2} \) 85 50 M. +46 36 Sec. \(\frac{1}{2} \) 85 59 M. +46 36 Sec. \(\frac{1}{2} \) 85 59 M. +46 24 Sec. \(\frac{1}{2} \) 85 59 M. +46 24 Sec. \(\frac{1}{2} \) 85 59 M. +46 24 Sec. \(\frac{1}{2} \) 85 59 M. +46 24 Sec. \(\frac{1}{2} \) 85 59 M. +46 24 Sec. \(\frac{1}{2} \) 85 57 A.M60 51 87 20 B. +49 16 E. \(\frac{1}{2} \) 90 00 M. +50 04 Sec. \(\frac{1}{2} \) 85 59 M. +46 16 E. \(\frac{1}{2} \) 90 00 M. +50 04 Sec. \(\frac{1}{2} \) 85 59 M. +46 36 Sec. \(\frac{1}{2} \) 85 59 M. +46 36 Sec. \(\frac{1}{2} \) 85 50 M. +46 36 Sec. \(\frac{1}{2} \) 85 50 M. +46 36 Sec. \(\frac{1}{2} \) 85 50 Sec. \(\frac{1}{2} \) 91 00 M. +50 04 Sec. \(\frac{1}{2} \) 85 50 Sec. \(\frac{1}{2} \) 91 00 M. +50 04 Sec. \(\frac{1}{2} \) 85 50 Sec. \(\frac{1}{2} \) 91 00 M. +50 04 Sec. \(\frac{1}{2} \) 85 Sec. \(\frac{1}{2} \) 85 Sec. \(\frac{1}{2} \) 91 30 M. +46 19 Sec. \(\frac{1}{2} \) 85 Sec. \(\frac{1}{2} \) 91 35 Sec. \(\frac{1}{2} \) 85 Sec. \(\frac{1}{2} \) 91 32 Bec. \(\frac{1}{2} \) 85 Sec. \(\frac{1}{2} \) 85 Sec. \(\frac{1}{2} \) 91 32 Bec. \(\frac{1}{2} \) 85 Sec. \(\frac{1}{2} \) 85 Sec. \(\frac{1}{2} \) 85 Sec. \(\frac{1}{2} \) 91 32 Bec. \(\frac{1}{2} \) 85 Sec. \(\frac{1}{2} \) 85 Sec. \(\frac{1}{2} \) 92 Bec. \(\frac{1}{2} \) 95 Sec. \(\frac{1}{2} \) 85 Sec. \(\frac{1}{2} \) 95 Sec. \(\frac{1}{2} \) 95 Sec.	1845.	aº ./				,	- 8 oó	9 00	(, , ,		/
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$\begin{bmatrix} -55 & 35 & 103 & 20 & \text{CL.} & +37 & 50 & \text{E. by s.} \end{bmatrix}$ $\begin{bmatrix} -4 & 40 & +32 & +34 & 02 \end{bmatrix}$	15 р.м.	_55 40	103 18	M.	+3537		} −78 33				Very unsteady.
	· .	55 35	103 20	CL.	+37 50	E. by s.	J	-4 40	+ 32	+ 04 0%)	

Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Correction Ship's		ected Declination.	Remarks.
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1845. Mar. 16 A.m. 16 p.m.	-54 42	2105 08	CL.		N.E. <u>1</u> E.) ° ′	$\begin{vmatrix} -3 & 47 \\ -3 & 56 \end{vmatrix} +$	52 + 2	9 12	
	-54 38	106 08 106 28		$+32 06 \\ +33 16$	N.E. ½ E. E.	-78 41		52 + 2	9 22 + 29 24	Very unsteady.
17 А.М.	$-54 36 \\ -54 05$	3 106 28 5 106 28 5 108 15	Bn. CL.	$\begin{vmatrix} +34 & 13 \\ +34 & 45 \\ +29 & 19 \end{vmatrix}$	E. E. by s.	$\left \begin{array}{c} \\ \\ \\ \end{array} \right = 79 \ 04$	$\begin{vmatrix} -4 & 46 + \\ -4 & 46 + \\ -4 & 52 + \end{vmatrix}$	$\begin{array}{c c} 52 + 3 \\ 52 + 2 \end{array}$	0 51 5 19 6 34	Very unsteady.
18 А.М.	$-53 \ 30$	510815 011013 411024	Bn.	$\begin{vmatrix} +32 & 02 \\ +25 & 18 \\ +22 & 05 \end{vmatrix}$	E. $\frac{1}{2}$ S. N.N.E. N.N.E. $\frac{1}{2}$ E.		$egin{bmatrix} -5 & 05 + \ -2 & 37 + \ -2 & 58 + \ \end{matrix}$	+2	23 33)	
STOCK STATE OF THE	-53 08	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	M.	$\begin{vmatrix} +26 & 50 \\ +26 & 25 \\ +23 & 34 \end{vmatrix}$	N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E.	$\left \begin{array}{c} -77 & 34 \end{array} \right $	$\begin{vmatrix} -4 & 01 \\ -3 & 47 \\ -4 & 01 \end{vmatrix}$	-52 + 2	$23 \ 30 \) + 21 \ 32$	Very unsteady.
18 p.m. 19 p.m. 20 A.m.	-53 03 $-52 38$	$ \begin{array}{ccccccccccccccccccccccccccccccccc$	T. CL.	+20 00	N. ½ W. N.N.E. N.E. by N.	-77 09		$\begin{array}{c c} 52 + 2 \\ 52 + 1 \end{array}$	$\begin{bmatrix} 0 & 04 \\ 6 & 43 \end{bmatrix} + 16 & 43 \end{bmatrix}$	Very unsteady.
20 A.M.	$\begin{vmatrix} -49 & 29 \\ -49 & 29 \end{vmatrix}$	211234 211234	Bn. Bn.	$\begin{array}{r} +21 & 06 \\ +20 & 05 \end{array}$	n. by E. ½ E. N.N.E.		$\begin{vmatrix} -2 & 04 \\ -2 & 19 \end{vmatrix} +$	-52 + 1 $-52 + 1$	9 54 8 38	
20 P.M	-49 00 $-49 00$	0 112 51	CL.	+1758 + 1830	N.E. $\frac{1}{2}$ N. N.E. $\frac{1}{2}$ N.	\\ \-76 17	-3 10 T	$\begin{array}{c c} -52 + 1 \\ -52 + 1 \end{array}$	$\begin{vmatrix} 5 & 40 \\ 6 & 12 \end{vmatrix} + 17 & 09$	Compass unsteady.
	-48 54 $-48 56$	911253 411255 611256	T. M.	$\begin{vmatrix} +21 & 50 \\ +17 & 12 \\ +17 & 24 \end{vmatrix}$	N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E.		$\begin{vmatrix} -3 & 35 & + \\ -3 & 35 & + \\ -3 & 35 & + \end{vmatrix}$	-52 + 1 $-52 + 1$	4 29 4 41	
	$-48 56 \\ -46 39 \\ -45 04$		M.	$\begin{vmatrix} +17 & 33 \\ +11 & 55 \\ +8 & 52 \end{vmatrix}$	N.E. $\frac{1}{2}$ E. N. $\frac{1}{2}$ W. N. $\frac{1}{2}$ W.	$\begin{bmatrix} 1 & -74 & 30 \\ 1 & -74 & 30 \end{bmatrix}$	15 +	-52 + 1 $-52 + 1$ $-52 + 1$	12 02 + 12 09	Steady.
25 а.м	-44 54 $-43 53$		M.	$\begin{vmatrix} +10 & 38 \\ + & 7 & 12 \\ + & 5 & 40 \end{vmatrix}$	N. N. by w. ½ w. N. by w.		$\begin{bmatrix} -1 & 03 \\ - & 30 \end{bmatrix}$	$ \begin{array}{c c} $	$\begin{bmatrix} 0 & 27 \end{bmatrix} + \begin{bmatrix} 9 & 45 \\ 7 & 34 \\ 5 & 50 \end{bmatrix}$	very unsteady.
Constitution of the Consti	$\begin{bmatrix} -43 & 59 \\ -43 & 49 \end{bmatrix}$	$ \begin{array}{c} 2 & 116 & 59 \\ 2 & 116 & 59 \\ \end{array} $	Bn. Cl.	+ 8 18 + 7 42	N. ½ W.	72 28	_ 54 +	- 52 + - 52 +	9 16	Card unsteady.
26 а.м	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$8 116 55 \\ 9 116 42$	CL.	+ 5 59 + 7 45 + 3 45	N. N. $\frac{1}{2}$ E. N. by W.		$\begin{vmatrix} -1 & 12 & + \\ - & 33 & + \end{vmatrix}$	- 52 + - 52 +	7 25 J 4 04	
26 p.m 27 a.m		4 116 42 2 116 42 0 116 15	M.	+ 3 10	N. by w. N. by w. N. by w.	$\left \right\} -70 \ 43$	- 33 + - 33 +	-52 +	$ \begin{array}{c c} 5 & 07 \\ 3 & 29 \\ 7 & 28 \end{array} $	Card unsteady.
27 г.м	$-38 \ 3$	0 116 15 2 116 17 8 116 19	/ M.	+ 7 48	N. by w. N. by E. N. by E.	-68 27	$\begin{vmatrix} - & 33 \\ -1 & 20 \\ -1 & 20 \end{vmatrix}$	- 52 +	1 20	Compass steady.
28 р.м	-37 0 $-36 4$	2 116 38 6 116 33 6 116 33	M. M.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N. by E. $\frac{1}{2}$ E N.N.E. N.N.E. $\frac{1}{2}$ E.	$-66 \ 38$	$\begin{vmatrix} -1 & 11 \\ -1 & 26 \\ -1 & 33 \end{vmatrix}$	$-52 + \\ -52 $	$ \begin{vmatrix} 3 & 51 \\ 5 & 11 \\ 4 & 32 \end{vmatrix} + 4 & 35$	Steady.
29 А.М	$-36 \ 1$ $-36 \ 1$	3 1 1 6 4 0 2 1 1 6 4 0 3 1 1 6 4 0	M. M.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	n. by E.	Ĭ	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	52 + 52 + 52	4 34) 5 41 4 14	
	$\begin{bmatrix} -36 & 1 \\ -36 & 1 \end{bmatrix}$	2 116 40 1 116 40	T. M.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N. by E.	-65 44	$\begin{vmatrix} -1 & 07 \\ - & 53 \end{vmatrix}$	+52 + +52 +	$\begin{array}{c c} 4 & 37 \\ 5 & 37 \end{array}$ + 4 59	Steady.
	-360	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E.		$\begin{vmatrix} -1 & 56 \\ -1 & 56 \\ -1 & 56 \end{vmatrix}$	-52 + 52 +	3 33 4 57 5 44	"
30 А.м	-35 0	911741 911741 411741	CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.E. \frac{1}{2} E. N. \frac{1}{9} E. S. \frac{1}{2} E.	_65 36	6 - 13 +	- 52 + - 52 +	$ \begin{array}{c c} 6 & 28 \\ 6 & 47 \\ 5 & 31 \end{array} $	O Compass steady.
30 р.м		4 117 41	l Bn.	+ 5 05	S. ½ E. S.		— 13 +		5 44	

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Date.	1340.	Long.	pse	observed.	omp s neada	Incimation.	Ship's attrac-	Index.	Corrected Decimation.	Remarks.
1			0				tion.	Inc	,	
1845.	000	118 04	n-	$+\mathring{7} \ 5\acute{9}$		$-6\mathring{5} 2\acute{0}$	1 =6	1.56	+6.55 + 6.55	
Mar. 31 A.M.					N.E. $\frac{1}{2}$ E.	-65 20 $-65 00$	1 00	+ 5%		Unsteady.
April 1 A.M.				+957	N.N.E.	-05 00	-1 22			Unsteady. Card J.
11 A.M. 14 A.M.			CL.	$ \begin{array}{c} +4 & 17 \\ +4 & 53 \end{array} $	Observed	on ahono			$\begin{vmatrix} +5 & 09 \\ +5 & 45 \\ \end{vmatrix}$ $+5 & 33$	Card J.
ITA.M.	King G Sound, A			+458	Observed	on shore.		+47		Card A.
21 л.м.				$+3 \ 48$	w. by s.	-65 11	+1 17			Card J. unsteady.
22 A.M.		1		+5 10	s.	-65 11			+5 59 +5 59	Unsteady.
23 а.м.		114 55		+3 05	N.W.	ה די			+4 18	
	-35 38	1	M.	+4 33	N.N.W. $\frac{1}{2}$ W.	-65 11			+5 16 > +5 41	Unsteady.
23 р.м.	1 .		M.	+629	N.W. $\frac{1}{2}$ N.)		+52	+7 30	
24 а.м.	-3424	113 17	M.	$+6 \ 31$	n.w. by n.	ń	- 04	+52	+7 19	
		113 15		+6 10	n.w. by n.	-64 44	- 04	+52	+6.58	Cond sunstands
	-34 17			+5 34	n.w. by n.	-07 44	- 04	+52	T 0 22	Card unsteady.
Noon.				+5 00	n.w. by n.	Ų	— 04	+52	$+5$ 48 \rightarrow	
25 A.M.		111 44	M.	+6.55	n.w. by n.		- 08	+52	+7 39	
	1	111 45	۱ ~	+604	n.w. by n.	-62 18	- 08	+52	+6 48	
	1	111 44		+5 20	N.W. $\frac{1}{2}$ N.	}		+52	$ +6 06\rangle +6 36$	Steady.
1		111 43		+5 05	N.W. $\frac{1}{2}$ N.		— 06	+ 5%	+5 51	
06		111 40		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	n.w. by n.	K	— US	+ 5%	$\begin{vmatrix} +6 & 37 \\ +6 & 39 \end{vmatrix}$	
26 а.м.		$109 15 \\ 109 15$	CL. Bn.	+6.25	n.w. by n.		10	+ 52	$\begin{vmatrix} +6 & 38 \\ +7 & 05 \end{vmatrix}$	
26 р.м.		109 13	M.	+5.58	N.W. by N.	 }−60 30	1 02	1 52	$\begin{vmatrix} +7 & 05 \\ +6 & 52 \end{vmatrix} + 7 & 20$	Unsteady.
20 F.M.		108 58		+752	N.W.	11	+ 02	± 52	+8 46	
27 л.м.		106 55		+604	N.W. $\frac{1}{2}$ W.	H	1. 10	+52	1 / AC 1	Q1 . 1 *
1		106 55	См.	+5 00	N.W.	-59 25	+ 02	+52	+5 54	Steady,
28 а.м.				+8 27	N.	$\left \frac{1}{2} - 57 \right 22$	_ 50	+52	+8 29 \ +6 22	Very unsteady.
28 р.м.		106 34		+4 26	n. by w.	J -0, 22	40	+52	T 4 38)	
29 а.м.	1 -	105 16	M.	+3.56	N.W.		— 07	+52	+4 41	
1	1	105 16		+5 52	N.W.	-55 07		+52	$\begin{vmatrix} +6 & 37 \\ +6 & 12 \end{vmatrix} + 5 & 30$	Very unsteady.
20		105 16	-	+5 28	N.W.	Ŋ	- 07		+6 13	
30 а.м.	$ \begin{array}{r} -24 & 10 \\ -24 & 05 \end{array} $		CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	W.N.W.	$\frac{1}{5}$ -54 30			$\begin{vmatrix} +5 & 10 \\ +5 & 54 \end{vmatrix} + 5 & 32$	Very unsteady.
Мау 1 л.м.	1		CL.	+3 02	W.N.W.	K			+4 32	
May 1 A.M.	-23 58		CL.	+3 00	w.		+ 38	± 52	1 4 90	
1	-23 58		M.	+4 25	w.	-54 07	+ 38	+52	$\begin{vmatrix} +4 & 30 \\ +5 & 55 \end{vmatrix} + 5 & 14$	Unsteady.
Noon.			M.	+4 30	w.				+6 00	
2 A.M.			M.	+757	N. by E. $\frac{1}{2}$ E.	ĸ	- 58	+52	+7 51	
	_24 01	1	М.	+750	N.N.E.	_54 11	-1 00	+52	+7 42 \ 17 08	Compass steady.
	_24 01			+6.26	N. by E. $\frac{1}{2}$ E.	\	– 58	+52	T 0 20]	
1	_24 01			+647	N.N.E.	Ų	-1 00	+52	+6 39	
3 А.М.			M.	+5 58	$W_{\bullet} \frac{1}{2} N_{\bullet}$]	+ 40	+52	$\begin{bmatrix} +7 & 30 \\ +6 & 20 \end{bmatrix}$	
	_23 55		M.	+458	$W. \frac{1}{2} N.$		+ 40	+52	+6 30	
	_23 55			$+3 \ 40$	W. $\frac{1}{2}$ N.	-54 21	+ 40	+ 5%	$\begin{vmatrix} +5 & 12 \\ +6 & 06 \end{vmatrix} + 6 & 10$	Steady.
3 р.м.	-24 00 $-24 00$			$+4 \ 41$	$W. \frac{1}{2} S.$		+ 93	+ 5%	$+5 \ 30$	
	-24 00 $-23 55$		Сь. См.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\mathbf{W}.\ \frac{1}{2}\ \mathbf{S}.$		+ 40	+ 52 + 50	+6 14	
4 A.M.			CL.	+5 09	w. ½ s. w.n.w.	\forall	+ 12	+52	+6 13	
TA.M.	-24 17		M.	+4 22	w.n.w.				+ 5 06 1	Card J. steady.
1	-24 17		M.	+351	w.n.w.	-54 07	+ 12	+47	$+\frac{3}{4} \frac{20}{50} > +5 31$	Card A. steady.
Noon.			M.	+4 30	w.n.w.		+ 12	+52	+5 34]	Card J. steady.
5 A.M.	24 05	92 11	CL.	+605	n.w. by n.	52 44	- 23	+52	$+6 \ 34 \ +6 \ 34$	Steady.
6 а.м.	22 54	90 50	M.	+4 38	N.W.	η	- 13	+52	+5 177	
	_22 54	90 50	B _N .	+457	N.W.		— 13	+52	+5 36	
	-22 54			+449	N.W.		— 13	+52	+5 28	
	_22 50	90 48		+5 04	N.W.		- 13	+52	+5 43	
6 р.м.	_22 39	90 35	iVI.	+5 59	n.w. by n.	-5249	— 23	+52	+6 28 > +5 56	Compass steady.
		<u> </u>			<u>!</u>			-		

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Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Ship's	, i	Corrected Declination.	Remarks.
			Ops	observed.	-		attrac- tion.	Index.		
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1845. Мау 6 р.м.	-2239	90 32	M.	+612	N.N.W.	>-52 49	- ° 34	+52	+6 30 > +5 56	Compass steady.
	-22 39	90 32	Bn.	+4 40	n.w. by n.		- 23	+52	+5 09	,,
C	-22 39		Cr.	+553	n.w. by n.				+6 22	
Sunset. 7 A.M.		90 32 89 42	CL. M.	$\begin{array}{r} +6 & 33 \\ +3 & 30 \end{array}$	N.N.W. N.W.	ر ا	- 34 - 18		$\begin{vmatrix} +6 & 51 \\ +4 & 04 \\ \end{vmatrix}$	
•	-21 53	89 42	CL.	+409	N.W.	-52 01	- 18	+52	$\begin{pmatrix} +4 & 04 \\ +4 & 43 \end{pmatrix} +4 & 23$	Unsteady.
8 л.м.		88 08	M.	+3 42	n.w. by w.		$-\frac{10}{10}$	+52	+4 24	
		88 05 88 05	M. Cl.	$+3 53 \\ +3 25$	n.w. by w. n.w. by w.	$> -51 \ 15$		$+52 \\ +52$	$\begin{vmatrix} +4 & 35 \\ +4 & 07 > +4 & 45 \end{vmatrix}$	Card steady.
	-20 45	88 05	B _N .	+4 11	n.w. by w.		- 10	+52	+4 53	
Noon.		87 56	M.	+430	$W_{\bullet} \frac{1}{2} N_{\bullet}$	J	+ 26	+ 52	$+5 \ 48$	
9 а.м.		85 39 85 39	M. Cl.	$\begin{array}{c c} +4 & 38 \\ +3 & 28 \end{array}$	W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N.	>-51 18	$+ 26 \\ + 26$	$+52 \\ +52$	$\begin{vmatrix} +5 & 56 \\ +4 & 46 \\ +5 & 20 \end{vmatrix}$	Steady.
Noon		85 19	M.	+4 00	$W \cdot \frac{1}{2} N \cdot$		+ 26	+52	+5 18	
10 A.M.	1	82 45	M.	+4 12	$W_{\bullet} \frac{1}{2} N_{\bullet}$)	+ 26	+52	+5 30	
		82 24 82 30	M. Bn.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c} W \cdot \frac{1}{2} & N \cdot \\ W \cdot \frac{1}{2} & N \cdot \end{array}$	-51 22	+ 26 + 26	$+52 \\ +52$	$\begin{array}{c c} +5 & 35 \\ +4 & 24 > +5 & 08 \end{array}$	Very unsteady.
		82 30	CL.	$+3 \ 26$	$\mathbf{W} \cdot \frac{1}{2} \mathbf{N} \cdot$	61 22	+ 26	+52	+4 44	roay unstoucy:
		82 30	T.	+4 08	$W_{\bullet} \frac{1}{2} N_{\bullet}$	ا لِ		+52	+5 26	
		79 36 79 34	M. M.	$\begin{array}{c c} +2 & 56 \\ +2 & 31 \end{array}$	W. $\frac{1}{4}$ N. W. $\frac{1}{4}$ N.		+ 24 + 24	$+52 \\ +52$	$\begin{array}{c c} +4 & 12 \\ +3 & 47 \end{array}$	
1	. 1	79 34	B _N .	+2 27	W. ¼ N. W. ¼ N.		+ 24	+52	$+3 \ 43$	
	-20 36	79 34	CL.	+3 12	w. 1 N.	├ —51 48	+ 24	+52	+4 28 > +4 43	Compass unsteady.
11 Р.М.	-20 36 $-20 36$	79 00 79 00	M. CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	W. $\frac{1}{4}$ N.			$+52 \\ +52$	$\begin{array}{c c} +6 & 04 \\ +5 & 50 \end{array}$	
		79 00	T.	$+3 \ 43$	W. $\frac{1}{4}$ N. W. $\frac{1}{4}$ N.]		+52	+459	
12 A.M.	-20 44	78 34	M.	+5 38	N.	1	_ 50	+52	+5 40	
		78 34 78 34	CL.	$\begin{array}{c c} +6 & 28 \\ +5 & 06 \end{array}$	N.			$+52 \\ +52$	$\begin{array}{c c} +6 & 30 \\ +5 & 20 \end{array}$	
		78 34	CL.	+6 32	N.N.W.			+52	$\begin{array}{c c} +5 & 20 \\ +6 & 46 \end{array}$	
	-20 44	78 34	M.	+5 27	N.W.		_ 22	+52	+5 57	
		78 34 78 34	CL. M.	$\begin{array}{c c} +5 & 12 \\ +3 & 23 \end{array}$	N.W.			+52	+5 42	
		78 34 78 34 78 34	CL.	$\begin{array}{c c} +5 & 25 \\ +5 & 36 \end{array}$	W.N.W.			$+52 \\ +52$	$\begin{array}{c c} +4 & 19 \\ +6 & 32 \end{array}$	
,	-20 44	78 34	М.	+2 23	w.		+ 20	+52	$+3 \ 35$	
		78 34	CL.	+4 09	w.	50.00	1	+52	+5 21	To obtain correc-
		78 34 78 34	M. CL.	$\begin{array}{c c} +2 & 58 \\ +4 & 22 \end{array}$	w.s.w.	-52 02		$+52 \\ +52$	$\begin{array}{c c} +4 & 05 \\ +5 & 29 \end{array}$	tions for the ship's
	-20 44	78 34	М.	+4 20	s.w.		+ 06	+52	+5 18	A calm, heavy swell, compass unsteady.
	-20 44 20 44		CL.	+4 26	s.w.		+ 06	+52	+5 24	
•		78 34 78 34	M. CL.	$\begin{array}{c c} +4 & 46 \\ +4 & 48 \end{array}$	s.s.w.		_ 01	$+52 \\ +52$	$\begin{array}{c c} +5 & 37 \\ +5 & 39 \end{array}$	
	-20 44	78 34	M.	+4 42	s.	1	- 08	+52	+5 26	
	-20 44	78 34	CL.	+4 29	s.		-08	+52	+5 13	
	-20 44 $-20 44$	78 34 78 34	M. CL.	$\begin{array}{c c} +5 & 41 \\ +6 & 00 \end{array}$	E.N.E.		-1 13 $-1 13$	$+52 \\ +52$	$\begin{array}{c c} +5 & 20 \\ +5 & 39 \end{array}$	
	-20:44	78 34	M.	+6 21	N.N.E.	j	- 57	+52	+6.16	
13 а.м.	-20 39	77 45	CL.	+4 11	w. ,)	+ 20	+52	+5 23	
-	-20 39 $-20 39$	77 45 77 45	T. M.	$\begin{array}{c c} +4 & 29 \\ +3 & 49 \end{array}$	w.	-51 59	+ 20 + 20	$+52 \\ +52$	$+5 \ 41 + 5 \ 22 + 5 \ 01$	Steady.
14 А.М.	-20 28	76 23	M.	$+4 \ 43$	$w. \frac{1}{2} N.$	7	+ 16	+52	+551	
	-20 28	76 23	B _N .	+4 25	$W \cdot \frac{1}{2} N \cdot$	-52 20	+ 16	+52	+5 33 > +6 01	Very unsteady.
15 а.м.	-20 28 $-20 45$	76 23 73 20	Сь. М.	$\begin{array}{c c} +5 & 31 \\ +4 & 46 \end{array}$	$W \cdot \frac{1}{2} N \cdot W \cdot \frac{1}{2} N \cdot$	-52[25]	+ 16 + 16	$+52 \\ +52$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Unsteady.
	-20 27	70 49	M.	+6 12	$\begin{array}{c} W \cdot \frac{1}{2} N \cdot \\ W \cdot \frac{1}{2} N \cdot \end{array}$	~ i	+ 16	+52	+7.20] $+6.35$	
<i>(</i> *)	—20 27	70 49	CL.	+4 43	$W_{\bullet} \stackrel{\overline{1}}{\underline{2}} N_{\bullet}$	$\int_{0}^{\infty} dz dz$	+ 16	+52	$+5 51$ $\}$ $+0 55$	Card unsteady.
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							Correct	ions.		
5 0.			Observer.	Declination	~		~	1		
Date.	Lat.	Long.	ser	observed.	Ship's head.	Inclination.	Ship's attrac-	Index.	Corrected Declination.	Remarks.
			O				tion.	nd		
1845.	0 /		~	9 .6			,		2 / 0 /	
Мау 17 л.м.			CL.	('	w.	$-53 \ 01$	+20	+52		Card unsteady.
		69 35	CL.	+ 4 45	W.	J 00 01	+20	+52	T 0 0/	Card unsteady.
18 а.м.		68 30	CL.	+ 6 28	$\mathbf{W} \cdot \frac{1}{4} \mathbf{S} \cdot$		+20	+52		
		68 22	M. M.	+624	w. by s.	50.00	+18	+52		G
P.M.		68 04 68 04	Bn.	$\begin{vmatrix} + & 7 & 35 \\ + & 8 & 59 \end{vmatrix}$	N.N.W.	$-53\ 06$	$-37 \\ -37$	+52 + 52		Compass steady.
Sunset.		68 00	M.	+ 7 45	N.N.W. N. by W. ½ W.		$-37 \\ -47$	+52 + 52		
19 л.м.	1	67 54	M.	+640	N.W.	\forall	-19	+52		
13 A.M.	1	67 54	CL.	+621	N.W. $\frac{1}{2}$ N.	-53 24	-23	+52		Card steady.
	$-21 11 \\ -21 11$,	т.	+511	N.W. $\frac{1}{2}$ N.	-35 24	-23	+52		Cura stoucy.
20 A.M.	-21 12		CL.	+ 6 24	w. by N.	ጘ <u>.</u>	+15	+52	l # 01 1	
		67 29	B _N .	+ 6 36	w. by N.	-5349	+15	+52		Steady.
21 а.м.		66 26	CL.	+ 6 53	w. by N.	ነ	+15	+52		
		66 26	Bn.	+ 6 34	w. by N.	-53 56	+15	+52		
ľ	-21 01	66 20	M.	+ 6 30	w. by N.]	+15	+52	+ 7 37	
22 A.M.	$-20 \ 41$	63 16	M.	+ 7 17	w. by N.	$\left.\right\} -53 \ 53$	+15	+52	$+824$ $_{\perp 897}$	
Sunset.	-20 38	62 44	М.	+ 7 23	w. by n.	3-33 33	+15	+52	T 8 30 J	
23 A.M.		59 42	CL.	+ 8 40	w. by N.)	+15	+52		
	$ -20 \ 30$		B _N .	+ 8 12	w. by N.	>-54~09			+919>+944	
	_20 30	1	M.	+ 9 00	w. by n.	J .	+15		+10 07)	
24 A.M.	, -	57 55	M.	+ 8 15	$W \cdot \frac{1}{2} N \cdot$	-53 56	+20	+52		Very unsteady.
27 A.M.			M.	+ 8 31	On shore.				$ +923\} + 944$	Port Louis, Mauri-
20	-2009		M.		J	3	Lac		T10 05 J	tius.
29 а.м.			CL.	+913	w.	54 00	+26		$\left \begin{array}{cc} +10 & 31 \\ +10 & 50 \end{array} \right\} + 11 & 15$	Card steady.
20 4 34		55 33	M.	+10 47	W. $\frac{1}{2}$ N.	ΙŹ	+20		T11 09 J	
30 A.M.		53 10	M.	+12 09	s.w.byw.½w.	1 1	+19		$\left { +13\ 20}\atop { +13\ 52} \right $	1
P.M.		52 58 52 58	B.	$\begin{vmatrix} +12 & 44 \\ +12 & 34 \end{vmatrix}$	s.w. by w. s.w. by w.	$-54 \ 45$	$\begin{vmatrix} +16 \\ +16 \end{vmatrix}$		$\begin{vmatrix} +13 & 52 \\ +13 & 42 \end{vmatrix} + 13 & 44$:
.		52 58	M.	+12 54	s.w. by w.	11	+16		$\begin{bmatrix} +13 & 42 \\ +14 & 02 \end{bmatrix}$	
31 р.м.	1 .		CL.		s.w.byw. $\frac{1}{2}$ w.	K	+19		$ +13 \ 28$	
02 11	$-23 \ 44$	1	CL.		s.w.byw. $\frac{1}{2}$ w.				+14 59>+14 22	Card unsteady.
	_23 44	1	M.	+13 28	s.w.byw. $\frac{1}{2}$ w.		+19		+14 39	1
June 1 A.M.	1 .	1	CL.		w.s.w.	15	1 27	+52	115 25	
	_25 47		M.	+13 24	w.s.w.	$ \} -57 19$	+27		$\begin{vmatrix} +13 & 33 \\ +14 & 43 \end{vmatrix} + 15 & 09$	Unsteady.
2 A.M.		49 20	M.	+15 38	N.W.	11	-01		+16 297	
1	_26 30	49 20	CL.	+15 25	N.W.	├ —58 36		+52	$+16\ 16 > +16\ 23$	
1	_26 30		T.	+15 32	N.W.	IJ	-01		+16 23J	**
4 A.M.			CL.		w. by s.	Ŋ	+48		$+21 \ 30$	
		46 09	Cr.	+1901	w. by s.		+48	+52	+20 41	
I .		46 14		+17 56	w. by s.	$-58 \ 38$				Very unsteady.
4 P.M.		45 59		+19 18	w. by s.		+48		+20 58	
Sunset		45 39	CL.	+17 38	w.	K	+51		+19 21]	
5 А.М.			CL.		w.		+31		$\begin{bmatrix} +21 & 03 \\ +20 & 27 \end{bmatrix}$	Card very unsteady.
1	_28 19		M.	+21 14	w.	$-58 \ 31$	+31			card very unsteady.
· C		43 00	CL.	+18 55	W.	K	+31		$\begin{bmatrix} +20 & 18 \ +21 & 02 \end{bmatrix}$	
0 A.M	-28 50			+19 58 +19 47	N.W. by W.		$ \begin{array}{c} +12 \\ +12 \end{array} $		1 00 51	
1	$\begin{bmatrix} -28 & 49 \\ -28 & 49 \end{bmatrix}$	$\begin{vmatrix} 42 & 10 \\ 42 & 11 \end{vmatrix}$	M. CL.		N.w. by w.	├ —59 01	+12 + 12		$\begin{vmatrix} +20 & 51 \\ +22 & 52 \end{vmatrix} + 21 & 57$	Very unsteady,
1		42 00	M.	$\begin{vmatrix} +21 & 48 \\ +22 & 00 \end{vmatrix}$	N.W. by W.	11	+12 + 12		$\begin{bmatrix} +22 & 32 \\ +23 & 04 \end{bmatrix}$	
7 4 34		40 32		$\begin{vmatrix} +22 & 00 \\ +21 & 48 \end{vmatrix}$	w. by w.	K	+22	+59	$\begin{bmatrix} +23 & 04 \end{bmatrix} \\ +23 & 02 \end{bmatrix}$	
I A.M		40 20	M.	+21 29	w. by n.	11	+22	+52	$\begin{bmatrix} +22 & 02 \\ +22 & 43 \end{bmatrix}$	
1		40 32			w. by N.	-5854			$\begin{vmatrix} +22 & 18 \\ +22 & 18 \\ +22 & 34 \end{vmatrix}$	Unsteady
7 р.м	_28 40			+21 17	w. by N.	1	+22		$+22 \ 31$	
1		39 52	CL.	+21 04	w. by N.		+22		+22 18	
]				1			1		

			ï.				Correction	ons.		
Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Ship's attraction.	Index.	Corrected Declination.	Remarks.
1845. June 8 A.M.	-28 53	37 58 37 55 37 56	M. M. CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	W. W. W. ½ S.	<u> </u>	+ 32 -	+52	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
8 p.m.	-28 56 -28 58	37 56 37 49 37 37	Т. М. М.	$\begin{vmatrix} +21 & 13 \\ +22 & 00 \\ +21 & 44 \\ +23 & 19 \end{vmatrix}$	$\begin{array}{c} W \cdot \frac{1}{2} S \cdot \\ W \cdot \frac{1}{2} S \cdot \\ W \cdot \\ W \cdot \frac{1}{2} S \cdot \end{array}$	-59 11	$\begin{vmatrix} + & 27 \\ + & 32 \end{vmatrix}$	$^{+52}_{+52}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
Sunset. 9 A.M. 11 A.M.	-30 20 $-30 16$		CL. M. CL. M.	$\begin{vmatrix} +22 & 48 \\ +25 & 36 \\ +24 & 38 \\ +26 & 28 \end{vmatrix}$	$\begin{array}{c} W. \frac{1}{2} S. \\ W. \frac{1}{2} S. \\ W. \frac{1}{2} S. \\ N.W. \text{ by } W. \end{array}$	$\left.\begin{array}{c} \\ \\ \\ \end{array}\right\} -57 59$	+ 30 + 30	$^{+}52$ $^{+}52$	T 20 00 j	Very unsteady.
11 A.M.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	33 41 33 41 33 41	M. M.	$\begin{vmatrix} +24 & 42 \\ +27 & 05 \\ +26 & 59 \end{vmatrix}$	W. ½ N. S.E. N.E.	-56 37	$\begin{vmatrix} + & 24 \\ - & 40 \\ -1 & 10 \end{vmatrix}$	$^{+52}_{+52}_{+52}$	T 20 41	Very unsteady.
12 A.M. 13 A.M.		33 41	Bn. Cl. M. M.	$\begin{vmatrix} +27 & 43 \\ +29 & 36 \\ +23 & 58 \\ +25 & 15 \end{vmatrix}$	s.e. s.e. $\frac{1}{2}$ e. w. by N. w. by s. $\frac{1}{2}$ s.	-57 19	$\begin{vmatrix} - & 46 \\ + & 19 \end{vmatrix}$	$^{+52}_{+52}$	$egin{bmatrix} +27 & 55 \ +29 & 42 \ +25 & 09 \ +26 & 32 \ \end{pmatrix}$	Very unsteady.
	$\begin{vmatrix} -31 & 05 \\ -31 & 06 \\ -31 & 16 \end{vmatrix}$	31 34 31 30 31 28	M. M. M. Bn.	$ \begin{array}{r} +25 & 22 \\ +25 & 13 \\ +25 & 25 \end{array} $	w. by s. $\frac{1}{2}$ s. w. by s. $\frac{1}{2}$ s. w. by s. $\frac{1}{2}$ s.		$egin{bmatrix} + & 25 \ + & 25 \ + & 25 \ \end{pmatrix}$	$^{+52}_{+52}_{+52}$	$\begin{vmatrix} +26 & 39 \\ +26 & 30 \\ +26 & 42 \end{vmatrix}$	
13 р.м.	-31 05		CL.	$\begin{vmatrix} +27 & 16 \\ +25 & 46 \\ +24 & 39 \\ +25 & 06 \end{vmatrix}$	w. by s. $\frac{1}{2}$ s. s.w.byw. $\frac{1}{2}$ w.s.w.byw. $\frac{1}{2}$ w.		$\begin{vmatrix} + & 25 \\ + & 21 \end{vmatrix}$	$^{+52}_{+52}$	$\begin{vmatrix} +28 & 34 \\ +27 & 03 \\ +25 & 52 \\ +26 & 19 \end{vmatrix}$	Card steady.
14 A.M.		29 51 3 29 45	M. CL. T.	$\begin{vmatrix} +25 & 26 \\ +28 & 06 \\ +27 & 02 \\ +27 & 19 \end{vmatrix}$	$\begin{array}{c c} s.w.byw.\frac{1}{2}w.\\ s.w.byw.\frac{1}{2}w.\\ w.\frac{1}{2}s.\\ w.\frac{1}{2}s. \end{array}$	$\left \begin{array}{c} \\ \\ \\ \end{array} \right = 57 34$	$egin{pmatrix} + & 21 \\ + & 22 \\ + & 30 \end{bmatrix}$	$+52 \\ +52$	$\begin{vmatrix} +26 & 39 \\ +29 & 20 \\ +28 & 24 \\ +28 & 41 \end{vmatrix}$	Card unsteady.
15 А.М	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	29 55 27 14 5 27 12	CL. M. T.	$\begin{vmatrix} +27 & 09 \\ +27 & 06 \\ +26 & 23 \end{vmatrix}$	$W. W. \frac{1}{2} S. W. \frac{1}{2} S.$		$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$+52 \\ +52 \\ +52$	$egin{pmatrix} +28 & 32 \ +28 & 28 \ +27 & 45 \ \end{pmatrix}$	
	-3440	$\begin{vmatrix} 27 & 10 \\ 27 & 00 \end{vmatrix}$	Bn. CL.	$\begin{vmatrix} +28 & 21 \\ +26 & 52 \end{vmatrix}$	$\begin{array}{c cccc} W \cdot \frac{1}{2} & N \cdot \\ W \cdot \frac{1}{2} & N \cdot \\ W \cdot \frac{1}{2} & N \cdot \\ W \cdot \frac{1}{2} & N \cdot \end{array}$	-57 06	$^{+}_{5}$ $^{26}_{+}$ 26	$+52 \\ +52$	$\begin{vmatrix} +27 & 26 \\ +29 & 16 \\ +29 & 39 \\ +28 & 10 \end{vmatrix} +28 & 41$	
15 Noon P.M	-345	26 46 25 58 25 58	M. CL.		N.w. by w. N.w. by w. N.w. by w.		+ 02 00 00	$+52 \\ +52 \\ +52$	$egin{pmatrix} +29 & 44 \\ +28 & 46 \\ +28 & 46 \end{bmatrix}$	
10 A.M	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$egin{pmatrix} 23 & 38 \\ 0 & 23 & 34 \\ 2 & 23 & 32 \end{bmatrix}$	B _N . C _L .	$\begin{vmatrix} +27 & 26 \\ +28 & 06 \\ +28 & 14 \end{vmatrix}$	$w.\frac{1}{2} s.$ $w.\frac{1}{2} s.$ $w. by n.$ $w. by n.$	-56 08	$\begin{vmatrix} + & 27 \\ 3 + & 17 \\ + & 17 \end{vmatrix}$	+52 + 52 + 52	$\begin{vmatrix} +28 & 30 \\ +28 & 45 \\ +29 & 15 \\ +29 & 23 \end{vmatrix}$	Card unsteady.
	-354	0 21 34	CL.	$ \begin{array}{r} +31 & 16 \\ +28 & 38 \\ +28 & 21 \\ +26 & 41 \end{array} $	N. $\frac{1}{2}$ E. N.W. $\frac{1}{2}$ W. W.N.W. W. by S.	$\begin{vmatrix} $	$\begin{bmatrix} - & 53 \\ - & 14 \\ + & 04 \end{bmatrix}$	$+52 \\ +52 \\ +52$	$egin{pmatrix} +31 & 15 \ +29 & 16 \ +29 & 17 \ +27 & 56 \ \end{pmatrix} +29 & 16 \ \end{array}$	1
19 А.м	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	8 20 24 8 20 24 5 19 35	M. CL.	$\begin{vmatrix} +27 & 29 \\ +27 & 43 \\ +29 & 00 \end{vmatrix}$	8.W. $\frac{3}{4}$ S. S.W. $\frac{3}{4}$ S. N.W.	$\left.\right\} -54 50$	$\begin{vmatrix} + & 19 \\ + & 19 \\ - & 19 \end{vmatrix}$	+52 + 52 + 52	$egin{pmatrix} +28 & 40 \\ +28 & 54 \\ +29 & 33 \end{pmatrix} +28 & 47 \\ +29 & 33 \end{pmatrix}$	7
		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		$\begin{vmatrix} +28 & 14 \\ +27 & 34 \end{vmatrix}$	N.W. $\frac{1}{2}$ W.				$\begin{array}{c c} +29 & 06 \\ +28 & 12 \end{array}$	7

Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Ship's attraction.	Index. su	Corrected Declination.	Remarks.
	-34 12 -34 12 Wanchor in Simon's Bay. As 56 Magnet servator of Good	-dO Hobe. Cape of Good Hobe.	M. M. M. M. M. CL. CL.	+28 52 +28 23 +28 23 +27 40 +27 28 +27 14 +27 40 +28 36 +29 30 +29 34 +29 47 +30 22 +29 56 +29 51 +29 26 +28 26 +28 11 +28 07	Correction	the Index as for Cards true Decli-	- 37 - 19 + 04 + 26 + 21 + 11 + 02 - 07 - 20 - 39 - 1 01 - 1 23 - 1 19 - 1 09	+52 $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$ $+52$	+29 21 +30 02 +29 47 +29 38 +29 51 +29 29 +29 34 +29 18 +29 18	To obtain the corrections for the ship's iron. Card J. error ~52'. Card A. error -47'.

Observations of the Inclination made on board Her Majesty's hired Bark "Pagoda," from the 10th of January to the 21st of July 1845, with Needle A (Fox C. 9). Face East.

Observer Lieut. T. E. L. MOORE, R.N. One hour after Noon.

						Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845. Jan. 10.	34 46	17 46	Direct. Needle N. Needle S. Mag. N. Mag. N.S. Mag. S.	$\begin{array}{rrrrr} -5\overset{\circ}{4} & 2\acute{6} \\ -54 & 44 \\ -53 & 27 \\ -54 & 22 \\ -53 & 53 \\ -53 & 54 \end{array}$	w. by n.	+63	, - 26	-53 34	Fresh breeze, a head swell.
11.	-35 29	15 09	Direct. Direct. Needle N. Needle S. Mag. N.S. Mag. N.	$\begin{array}{r rrrr} -54 & 32 \\ -52 & 27 \\ -52 & 38 \\ -51 & 42 \\ -52 & 55 \\ -52 & 15 \end{array}$	w. by N. N.W. by W.	Len	-26	-51 27	A little motion.
12.	-35 17	14 00	Mag. S. Direct. Needle N. Needle S. Mag. N.S. Mag. N. Mag. S.	-52 09 -51 45 -52 17 -51 20 -51 56 -51 29 -51 26	N.W. by W. W. \frac{1}{2} S.		-26	—51 16	A little motion.
13.	-35 24	13 23	Direct. Direct. Needle N. Needle S. Mag. N.S. Mag. N.	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{array}{c} \text{W.} \frac{1}{2} \text{ S.} \\ \text{S.W.} \frac{1}{2} \text{ S.} \end{array}$	+27	-26	-51 19	A little motion.
15.	-38 42	14 27	Mag. S. Direct. Needle N. Needle S. Mag. N.S. Mag. N. Mag. S.	$ \begin{array}{r} -53 & 47 \\ -52 & 36 \\ -53 & 38 \\ -53 & 19 \end{array} $	s.w. $\frac{1}{2}$ s. s. by w. $\frac{1}{2}$ w. s. by w. $\frac{1}{2}$ w.	+18	-26	-53 31	A head' swell, table unsteady.
16.	-39 10	14 38	Direct. Direct. Needle N. Needle S. Mag. N.S. Mag. N.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s. by w. ½ w. s. by w. ½ w. s.w.byw.½w. s.w.byw.½w. s.w.byw.½w. s.w.byw.½w.	$\left \begin{array}{c} \\ \\ \\ \\ \end{array} \right _{>+12}$	-26	54 12	Table very unsteady.
17.	- 40 41	14 16	Mag. S. Direct. Direct. Needle N. Needle S. Mag. N.S.	$\begin{array}{rrrrr} -53 & 58 \\ -53 & 36 \\ -55 & 17 \\ -55 & 27 \\ -54 & 47 \\ -55 & 22 \end{array}$	s.w.by w.½w. s.w.by w.½w. w.s.w. w.s.w. w.s.w.		-26	54 - 59	A heavy head swell, much motion.
21.	50 21	10 31	Direct. Needle N. Needle S. Mag. N.S. Mag. N. Mag. S.	-55 39 -55 32 -55 15 -55 49 -55 25 -55 31	s.w. s.w. s.w. s.w. s.w.	+24	-26	55 34	Moderate breezes, a little motion.

						Corrections.			
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclin	ation. Remarks.
1845. J an. 23.	$-\mathring{5}0$ 48	3 10 18	Direct. Needle N.	-5745	s.w.byw.½w. s.w.byw.½w.) ′	-	0 /	
			Mag. N.S. Mag. N. Mag. N. Mag. S.	$-57 ext{ } 45 \ -57 ext{ } 28$	s.w.byw. $\frac{1}{2}$ w. s.w.byw. $\frac{1}{2}$ w. s.w.byw. $\frac{1}{2}$ w. s.w.byw. $\frac{1}{2}$ w.	+34	-26	-57 19	A little motion.
24.	-51 4	9 36	Direct. Direct. Needle N.	$ \begin{array}{r rrr} -57 & 25 \\ -57 & 24 \end{array} $	s.w.byw. $\frac{1}{2}$ w. s.w. by w.	$\left. ight\} +30$	-26	-57 28	Moderate breeze,
24.	-51 50	9 30	Direct. Mag. N.S.	-5741	s.w. by w. s.w.byw.½w. s.w.byw.½w.	3		-57 42	table steady. A head swell, much
25.	-53 2	7 32	Direct. Direct. Needle N.	$ \begin{array}{r rrr} -57 & 44 \\ -57 & 26 \\ -57 & 51 \end{array} $	s.w.byw. $\frac{1}{2}$ w. s.w.byw. $\frac{1}{2}$ w. s.w.byw. $\frac{1}{2}$ w.			• =:·	motion 4½ P.M.
			Mag. N.S. Mag. N. Mag. N. Mag. S.	-57.24 -57.33	s.w.byw.½w. s.w.byw.½w. s.w.byw.½w. s.w.byw.½w.	>+28	-26	-57 24	Ship passing through streams of loose ice.
26.	-54 09	6 02	Direct. Direct. Needle N.	$ \begin{array}{r rrr} -57 & 24 \\ -57 & 56 \\ -57 & 49 \end{array} $	s.w.byw.½w. w. by n. w. by n.				
			Needle S. Mag. N.S. Mag. N. Mag. S.	$ \begin{array}{rrrr} -57 & 02 \\ -57 & 55 \\ -57 & 05 \\ -57 & 18 \end{array} $	w. by n. w. by n. w. by n. w. by n.	>+61	-26	-56 58	Table steady, small pieces of loose ice about the ship.
27.	-55 1	5 55	Direct. Direct. Needle N. Direct.	$ \begin{array}{r rrrr} -57 & 43 \\ -57 & 30 \\ -58 & 23 \\ -57 & 54 \end{array} $	w. by N. s.s.w. ½ w. s.s.w. ½ w. s.s.w. ½ w.	$\left. \begin{array}{c} \\ \\ \\ \end{array} \right. + 10$	—26	-58 12	Ship pitching heavily, fresh breezes.
31.	-61 1	9 07	Direct. Needle N. Needle S.	$ \begin{vmatrix} -61 & 13 \\ -61 & 41 \\ -60 & 41 \end{vmatrix} $	S.S.E. S.S.E. S.S.E.				
			Mag. N.S. Mag. N. Mag. S. Direct.	$ \begin{vmatrix} -61 & 04 \\ -60 & 58 \\ -61 & 26 \\ -61 & 23 \end{vmatrix} $		>+05	-26	-61 43	Table steady, heavy snow.
Feb. 1.	-62 0	12 52	Direct. Needle N. Needle S.	$ \begin{vmatrix} -62 & 56 \\ -62 & 41 \\ -62 & 36 \end{vmatrix} $	s.e. by s. s.e. by s.) 0	-26	-63 17	Much motion, table very unsteady,
2.	-61 5	6 16 36	Direct. Direct. Needle N. Needle S.	$ \begin{array}{r rrrr} -63 & 12 \\ -63 & 59 \\ -62 & 25 \\ -63 & 37 \end{array} $	s.e. by s. s.e. $\frac{1}{2}$ e. s.e. $\frac{1}{2}$ e. s.e. $\frac{1}{2}$ e.				heavy snow.
			Needle N.S. Mag. N. Mag. S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	+13	-26	-63 55	Heavy snow, a head sea, ship pitching violently, water clear from ice.
3.	-61 5	0 19 14	Direct. Direct. Direct.	$ \begin{vmatrix} -64 & 09 \\ -65 & 09 \\ -64 & 49 \end{vmatrix} $	w.s.w.	$egin{pmatrix} +25 \\ +92 \end{smallmatrix}$			
	Co. ^	0 20 40	Direct. Direct.	$ \begin{array}{r rrr} -65 & 00 \\ -64 & 59 \\ -64 & 44 \\ \hline 64 & 18 \\ \hline \end{array} $	w. w.s.w. s.w.	$\begin{vmatrix} +47 \\ +25 \\ +03 \end{vmatrix}$		-64 44	Calm.
4.	-63 0	0 20 40	Direct. Needle N. Needle S. Needle N.S.	$ \begin{array}{r rrrr} -64 & 13 \\ -64 & 12 \\ -63 & 39 \\ -64 & 06 \end{array} $	s.w.	\\\\>+03	-26	-64 25	Unsteady.
	•		Mag. N. Mag. S.	$\begin{bmatrix} -63 & 59 \\ -64 & 06 \end{bmatrix}$]			

						Correc	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.						,	,	0 /	
Feb. 5.	$-63\ 19$	21 48	Direct.	$-65^{\circ} 17^{\circ}$	S.S.E.	ר ו	.•		
			Needle N.	-64 39	S.S.E.				}
			Needle S.	-64 29	S.S.E.	,,	o.c	Gr of	
. ,			Needle N.S. Mag. N.		S.S.E. S.S.E.	\rangle -15	- 26	-65 35	Heavy swell from S.E., light breeze
			Mag. N.	$\begin{vmatrix} -64 & 46 \\ -64 & 52 \end{vmatrix}$	S.S.E. S.S.E.				table steady.
			Direct.	-65 25	S.S.E.				
6.	-64 25	24 18	Direct.	$-66 \frac{17}{17}$	S.S.E. 1/2 E.	ξ			
			Needle N.	-66 16	S.S.E. 1/2 E.				
			Needle S.	-65 28	S.S.E. 1/2 E.	>-14	-26	-66 41	Table steady.
			Needle N.S.		S.S.E. 1/2 E.				j
	C= 00	20.40	Direct.	-66 07	S.S.E. \(\frac{1}{2}\) E.	Į.			ļ
7.	-65 39	28 48	Direct. Needle N.		s. by E. ½ E.				
			Needle S.	-66 54	s. by E. $\frac{1}{2}$ E. s. by E. $\frac{1}{2}$ E.				-
			Needle N.S.	-67 05	s. by E. $\frac{1}{2}$ E.	\rangle -22	-26	-67 56	Table steady.
			Mag. N.	-67 02	s. by E. $\frac{1}{2}$ E.				
			Mag. S.	-67 10	s. by E. 1/2 E.				
8.	-66 27	30 45	Direct.	-68 28	s.E. by E.)			•
			Needle N.	-68 09	s.e. by e.				
			Needle S.	-6749	s.E. by E.	105	06	-68 31	Ì
			Needle N.S.	-6804	s.E. by E.	$\rangle + 05$	26	-08 31	Fresh breeze, table steady.
			Mag. N. Mag. S.	$ \begin{array}{r rrr} -68 & 08 \\ -68 & 06 \end{array} $	s.e. by e.				
			Direct.	-68 26	s.e. by e.				
9.	$-66 \ 36$	36 50	Direct.	-6911	s.e. by e.	3 1			
3.			Needle N.	-69 13	s.e. by e.				
			Needle S.	-68 40	s.e. by e.				(
			Needle N.S.		s.e. by e.	>+05	-26	-69 22	Light breeze, very steady.
			Mag. N.	-6859	s.e. by e.			et i	
			Mag. S. Direct.	-69 02 60 00	s.e. by e.				
10.	-67 10	38 51	Direct.	$\begin{vmatrix} -69 & 20 \\ -70 & 12 \end{vmatrix}$	s.e. by e.	\forall			
10.	-0, 10	00 01	Needle N.	$-70^{\circ} 12^{\circ} -70^{\circ} 53^{\circ}$	s. by w.				
	-		Needle S.	-70 02	s. by w.				
			Needle N.S.		s. by w.	-32	-26	-71 07	Steady.
			Mag. N.	-70 00	s. by w.	1			
			Mag. S.	-70 12	s. by w.				
	C# 90	40.00	Direct.	-70 05	s. by w.	ر ا			
11.	-67 39	40 28	Direct. Needle N.	$\begin{vmatrix} -70 & 33 \\ -70 & 26 \end{vmatrix}$	N.E.	\ \ +89	-26	-69 27	Strong breeze, sail-
12.	-67 18	40 22	Direct.	$-69 \ 36$	N.E. S. ½ E.	7			ing along a pack of ice, unsteady.
1 ~.	0, 10	10 22	Needle N.	$-69 \ 43$	S. $\frac{1}{2}$ E.				
			Needle S.	-68 58	S. $\frac{1}{2}$ E.				
	ļ		Needle N.S.	-6928	$S_{\bullet} = \frac{1}{2} E_{\bullet}$	> -32	-26	-70 20	Fresh breeze, table
- 1			Mag. N.	-69 18	S. $\frac{1}{2}$ E.				unsteady.
·			Mag. S.	-69 03	$s. \frac{1}{2} E.$				
13.	-66 55	40 1C	Direct.	-69 28	S. \(\frac{1}{2}\) E.	Ν, I			
19.	00 99	40 16	Direct. Needle N.	-70 12 $-70 28$	E.N.E. E.N.E.				
			Needle S.	-69 54	E.N.E.				
.			Needle N.S.	-7008	E.N.E.	_+67	-26	-69 30	A swell from the
			Mag. N.	-70 14	E.N.E.				eastward, table unsteady.
			Mag. S.	-70 06	E.N.E.				
1			Direct.	-70 13	E.N.E.	ا زا			

						Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Observed. Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.									
Feb. 14.	-66° 24	40 01	Direct.	-7038	N.E. by N.	h '	1	0, 1	
			Needle N.	-70 07	n.e. by n.	>+89	-26	-69 15	Very squally, with
			Needle S.	$-70\ 10$	n.e. by n.	100		0, 10	thick weather, table unsteady.
16.	-64 52	90 97	Direct.	-70 17	N.E. by N.	7		**	table unsteady.
	-04 6%	38 37	Direct. Needle N.	-68 03 $-68 13$	s. by E. s. by E.				
			Needle S.	-67 20	s. by E.		00	00.00	
			Needle N.S.		s. by E.	>-30	-26	-68 53	A heavy swell, un- steady.
			Mag. N.	-6752	s. by E.				1
	0		Mag. S.	-68 06	s. by E.	J			
17.	$-64 \ 43$	40 12	Direct.	-6958	N.	Π			
			Needle N. Needle S.	$-70 02 \\ -69 22$	N. N.				
			Needle N.S.		N.	+76	-26	-68 18	Calm, a heavy sea,
	-		Mag. N.	-68 25	N.] [' ' '	,,,,		not steady.
			Mag. S.	-68 30	N.				
			Direct.	-68 50	N.	J.			
19.	-64 05	41 09	Direct.	$-70 \ 13$	E. by s.	} +27	-26	-70 02	Observed the inner
മെ	-63 19	45 52	Needle N. Direct.	-6952	E. by s.	IJ		•	circle to have moved, table
20.	-05 19	45 5%	Needle N.		s.e. by e . ½ e. s.e. by e . ½ e.	1 1		_	very unsteady.
			Needle S.		s.e. by E. $\frac{1}{2}$ E.		-26	-70 14	A heavy swell.
		-	Needle N.S.	-69 54	s.E. by E. 1/2 E.] .			
	-63 22	45 58	Direct.	-6954	S.E.	Й		\rangle -70 15	
			Needle N.	-69 53	S.E.	-08	-26	-70 15	Strong breezes, with
			Needle S.	-69 06	S.E.			,,,,,,	a heavy sea run- ning.
91	-63 36	46 46	Needle N.S. Direct.	$\begin{bmatrix} -69 & 50 \\ -69 & 38 \end{bmatrix}$	S.E.	K			5
Α1.	-00 00	10 10	Needle N.	-69 39	S.E.		~ 0		
			Needle S.	-69 03	S.E.	\\ \rightarrow -08	-26	-70 05	Table unsteady, eight icebergs in
			Needle N.S.	$-69 \ 43$	S.E.	IJ			sight.
	-63 36	46 50	Direct.	-70 01	S.E.	ח		>-70 13	3
			Needle N.	-7002	S.E.]]			
			Needle S. Needle N.S.	$\begin{vmatrix} -69 & 34 \\ -69 & 32 \end{vmatrix}$	S.E.	-10	-26	-70 21	Much motion.
			Mag. N.	$-69 \ 37$	S.E.		. ~0	10 213	much motion.
		1	Mag. S.	-69 32	S.E.	11 .			
			Direct.	-70 00	S.E.			6.	
25.	-61 34	53 49	Direct.	-7044	S.E. ½ E.	Ď.			
			Needle N. Needle S.	-70 22	S.E. $\frac{1}{2}$ E.	11			
			Needle N.S.		S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{3}$ E.	_05	-26	-70 49	Iceblink to the
			Mag. N.	-7008	S.E. ½ E.	7-00	-	70 13	southward, fresh
			Mag. S.	-70 08	S.E. $\frac{1}{2}$ E.				breezes, table unsteady.
			Direct.	-7042	S.E. 1 E.			-	
26.	-61 19	57 33	Direct.	-71 03	S.E. ½ E.)			1
			Needle N.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.E. ½ E.	-07	-26	-71 26	No ice in sight,
			Needle S. Needle N.S.		S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.				unsteady.
	-61 22	57 41	Direct.	$-70 \ 40$ $-71 \ 01$	S.E. 2 E. S.E.	K			
			Needle N.	-71 22	S.E.	1			
			Needle S.	-70 30	S.E.	_13	-26	-71 27	Danah har
			Needle N.S.	$-70 \ 43$	S.E.	> 13	-20	11 21	Fresh breeze, table steady.
			Mag. N.	-70 29	S.E.				
		1	Mag. S.	$-70 \ 40$	S.E.	IJ			

						Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclinatio	n. Remarks.
1845. Feb. 27.	-61° 16′	64 20	Direct. Needle N.	$ \begin{array}{c cccc} -71 & 20 \\ -71 & 48 \\ \hline \end{array} $	S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E.	-26	, -26	-72 18	Very unsteady.
28.	-61 49	71 30	Needle S. Direct. Needle N. Needle S.	$ \begin{array}{rrrrr} -71 & 10 \\ -72 & 44 \\ -72 & 49 \\ -72 & 36 \end{array} $	S.S.E. ½ E. S.S.E. S.S.E. S.S.E.		-		
-		-	Needle N.S. Mag. N. Mag. S.		S.S.E. S.S.E. S.S.E.	>-33	-26	$\begin{vmatrix} -73 & 36 \\ -73 & 36 \end{vmatrix}$	Table steady.
	-61 49	71 30	Direct. Needle N. Needle S. Needle N.S.	$ \begin{array}{rrr} -72 & 45 \\ -73 & 01 \\ -72 & 12 \end{array} $	s.s.e. s.s.e. s.s.e. s.s.e.	$\left \right\rangle$ -36	-26	-73 40	Steady.
Mar. 1.	-62 10	72 25	Direct. Needle N. Needle S. Needle N.S. Mag. N.	$ \begin{array}{rrr} -73 & 37 \\ -73 & 54 \\ -73 & 25 \end{array} $	s.e. by s. s.e. by s. s.e. by s. s.e. by s.	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	-26	-74 33	Calm, table steady.
2.	-62 47	76 14	Mag. S. Direct. Needle N. Needle S. Needle N.S. Mag. N.	$ \begin{array}{rrrr} -73 & 45 \\ -73 & 41 \\ -74 & 12 \\ -73 & 39 \\ -73 & 45 \end{array} $	s.E. by s. s. by E. $\frac{1}{2}$ E. s. by E. $\frac{1}{2}$ E. s. by E. $\frac{1}{2}$ E. s. by E. $\frac{1}{2}$ E. s. by E. $\frac{1}{2}$ E.	-40	-26	-74 55	
	-62 49	76 16	Mag. S. Direct. Needle N. Needle S. Needle N.S.	-73 48 -74 11 -74 21 -73 43 -73 58	s. by E. \(\frac{1}{2}\) E. s. s. s. s. s. s.	$\left. ight\}$ -45	-26	-75 15 -75 (Steady breeze, table steady.
3.	-64 20	79 38	Direct. Direct. Needle N. Needle S. Needle N.S.	$-74 56 \\ -74 39$	s. by w. $\frac{1}{2}$ w.	$\left. \begin{array}{c} -40 \end{array} \right $	-26	—75 57	Squalls of snow, fresh breeze, un- steady.
5.	-61 42	85 07	Direct. Direct. Needle N. Needle S.	-74 56 -76 13 -76 40 -76 18	s. by w. $\frac{1}{2}$ w. s.e. $\frac{1}{2}$ e. s.e. $\frac{1}{2}$ e. s.e. $\frac{1}{2}$ e.	} }-17	-26	-76 58	Table very unsteady
6.	-60 48	88 33	Needle N.S. Direct. Direct. Needle N. Needle S.	-75 59 -76 06 -76 21 -76 41 -76 06	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. S.F. S.F.				aurora visible.
	C1 00	01.15	Needle N.S. Mag. N. Mag. S. Direct.	-75 46 -75 56 -76 16 -76 26	S.E. S.E. S.E.	_23	-26	77 04	Very unsteady.
7.	-61 23	91 15	Direct. Needle N. Needle S. Needle N.S. Mag. N.	$ \begin{array}{c cccc} -76 & 26 \\ -77 & 02 \\ -76 & 12 \\ -76 & 28 \\ -76 & 13 \end{array} $	s.s.w. s.s.w. s.s.w. s.s.w.	-46	-26	-77 41	Aurora visible.
8.	—61 07	92 10	Mag. S. Direct. Direct. Needle N. Needle S.	-76 35 -76 26 -78 11 -77 39 -76 55	s.s.w. s.s.w. e. by s. e. s.e. e.s.e.	$\left. egin{array}{c} +13 \\ > 00 \end{array} ight.$	-26 -26	$-78 \ 24$ $-77 \ 29$ $-77 \ 5$	7 Aurora visible; table unsteady; snow.
all of the second			Needle N.S. Direct.	$ \begin{array}{c c} -76 & 39 \\ -76 & 59 \end{array} $	E.S.E.			·	

·						Correc	ctions.		* * * * * * * * * * * * * * * * * * *
Date.	Lat.	Long.	Method. employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.	-6° 30	92° 34	Direct.	-77 [°] 12	E.S.E.	01	စင်	−7 [°] 7 3 [°] 77	,
Mar. 9.	-00 30	92 34	Needle N.	$-77 12 \\ -77 31$	s.e. by e.	7 -01		77 99	Very unsteady,
			Needle S.	-7649	s.e. by e.	-10	-26	-77 28 -77 38	aurora visible.
	•	V 1	Needle N.S.		s.e. by e.	- 10	-20	-11 200	
10	Ca 00	96 03	Direct.	$-76 ext{ 41} \\ -77 ext{ 10}$	s.E. by E.	K I			
10.	-60 03	90 03	Direct. Needle N.	-77 10 $-77 25$	s.e. by e.		~ 0		
1			Needle S.	-76 45	s.e. by E.	>-10	-26	-77 38	Table unsteady, aurora still
			Direct.	-77 01	s.e. by e.	J			visible.
11	-5945	99 50	Direct.	-79 30	E. $\frac{1}{2}$ N.				
			Needle N. Needle S.	-79 13 $-79 29$	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.				
			Needle N.S.		E. $\frac{1}{2}$ N.	>+32	-26	-79 23	A heavy sea, very
			Mag. N.	-7945	E. $\frac{1}{2}$ N.				unsteady.
			Mag. S.	-7943	E. $\frac{1}{2}$ N.				-
12	-57 46	99 17	Direct.	$-79 35 \\ -78 30$	E. $\frac{1}{2}$ N. E. N. E.	\forall			
10.	37 40	33 17	Needle N.	-78 04	E.N.E.		o.C		
			Needle S.	-78 00	E.N.E.	>+50	26	-77 43	6 A.M. The aurora seen faintly, very
			Direct.	-78 20	E.N.E.	J			unsteady.
14.	-56 56	101 36	Direct. Needle N.	-78 04	E. by s.				
			Needle S.	-78 21 -77 33	E. by s. E. by s.	+13	-26	-78 11	A.M. Aurora visi-
1			Needle N.S.		E. by s.		~0	70 11	ble, unsteady; squally, with snow.
			Direct.	-77 58	E. by s.	j			1
15.	-55 40	103 18	Direct. Needle N.	$-78 \ 30$	E.N.E.				
			Needle S.	$ \begin{array}{c cccc} -78 & 53 \\ -78 & 31 \end{array} $	E.N.E.	+56	-26	-78 09	Unsteady.
			Needle N.S.		E.N.E.		~0	70 03	o nascady.
			Direct.	-78 30	E.N.E.	J .			
16.	-54 38	106 15	Direct.	-79 32	E	J			
			Needle N. Needle S.	$ \begin{array}{c c} -79 & 29 \\ -78 & 48 \end{array} $	E. E.	⊥ 25	- 26	-7 9 13	Heavy squalls, un-
1			Needle N.S.		E.	> T 20	~0	-13 10	steady.
			Direct.	-79 13	E •]			
17.	-54 10	108 15	Direct.	-79 17	E. by s.)			
			Needle N. Needle S.	$ \begin{array}{c c} -79 & 31 \\ -78 & 38 \end{array} $	E. by s. E. by s.	113	26	-7 9 19	A strong gale, very
.			Needle N.S.	-78 56	E. by s.	>+10	20	75 15	unsteady.
		, ·	Direct.	-79 10	E. by s.)			
18.	-53 00	110 35	Direct.	-78 38	N.E.	Ť			
			Needle N. Needle S.	$ \begin{array}{c cccc} -78 & 51 \\ -78 & 39 \end{array} $	N.E.	1			
1			Needle N.S.	-78 50	N.E.		-0	* • • • • • • • • • • • • • • • • • • •	
		•	Mag. N.	-78 25	N.E.	+80	-26	-77 39	Unsteady, a heavy swell from the
	1		Mag. S.	-7804	N.E.	.			westward, strong breeze.
10	51 00	111 00	Direct.	$ \begin{array}{c c} -78 & 26 \\ -78 & 30 \end{array} $	N.E.	J ₊₈₀	-26	-77 36	Too unsteady to
19. 20.	$-51 00 \\ -48 57$	111 29 112 56	Direct. Direct.	-78 30 $-77 14$	N.E. N.E. ¹ / ₂ N.	7 +00	-20	11 90	continue the
~ ~ •		222 00	Needle N.	-77 25	N.E. $\frac{1}{2}$ N.				observation.
			Needle S.	—77 01	N.E. $\frac{1}{2}$ N.	>+84	-26	-76 04	Very unsteady.
·			Needle N.S.	-76 55	N.E. $\frac{1}{2}$ N.	(104	~"		
	.	yr .	Mag. N. Mag. S.	-76 51 $-76 45$	N.E. $\frac{1}{2}$ N. N.E. $\frac{1}{2}$ N.				
			Luge D.	, 0 10	2 N	J			

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Inclination.	Remarks.
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0 /	
$egin{array}{c c c c c c c c c c c c c c c c c c c $		1
Needle S. $ -76 ext{ }11 $ N.w. $\frac{1}{2}$ N.		1
Needle N.S. $ -76 \ 28 \ $ N.W. $\frac{1}{2}$ N. $ >+85 \ -26 \ $ -7	5 32	Light breeze, table
Mag. N. $-76 \ 38$ N.W. $\frac{1}{2}$ N.		steady, thick fog.
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		
2445 08 116 50 Direct. -74 31 N. by E. 7		
	3 27	A heavy sea, ship pitching heavily,
Direct. $ -74 \ 37 $ N. by E.		very unsteady.
25. -43 22 116 49 Direct. $ -73$ 25 N. $\frac{1}{2}$ E.		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		
Needle N.S. $ -73 \ 18 $ N. $\frac{1}{2}$ E. $ > +70 \ -26 \ $	2 10	A heavy westerly swell, unsteady.
$\left \begin{array}{c cccc} Mag. \ N. & -72 & 26 \\ Mag. \ S. & -72 & 46 \\ \end{array}\right \left \begin{array}{cccccc} N. \frac{1}{2} E. \\ N. \frac{1}{2} E. \\ \end{array}\right \right $		
26. $-41 \ 00$ 116 42 Mag. S. $-72 \ 46$ N. $\frac{1}{2}$ E. $-72 \ 09$ N. by W.		
Needle N. -71 50 N. by w.		
$egin{array}{ c c c c c c c c c c c c c c c c c c c$	1 14	A heavy westerly
Mag. N. -72 00 N. by w.		swell.
$\left \begin{array}{c c} \text{Mag. S.} & -72 & 12 & \text{N. by w.} \\ \text{Direct.} & -72 & 09 & \text{N. by w.} \end{array}\right $		
2738 40 116 15 Direct72 09 N. by w. J Direct69 08 N. by E.		
Needle N. -69 08 N. by E.		
Needle S. $ -68 \ 38 $ N. by E. $ >+81 $ $ -26 $ $ -6 $ Needle N.S. $ -68 \ 59 $ N. by E. $ >+81 $	8 04	Table steady.
Direct. -69 03 N. by E. }		
2837 00 116 57 Direct67 24 N. by E. Needle N67 37 N. by E.		
Needle C 66 = 0 - 1 - 1	6 21	Wahlastandar slaveda
Needle N.S. $-67 14 \text{N}$. by E. $\frac{1}{2} \text{E}$. $(-730) -20 \text{M}$	00 21	Table steady, cloudy:
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		
2936 11 116 48 Direct. -66 53 N.N.E.		
	6 00	Unsteady.
$ \begin{vmatrix} Needle S. & -66 & 51 \\ Needle N.S. & -66 & 57 \end{vmatrix} $ N.N.E.		
3035 07 117 28 Direct66 15 N.N.E.		
	5 24	Unsteady.
Needle N.S65 59 N.N.E.		
April 735 02 117 56 Direct64 42 Needle N64 39		
N	64 55	At the tents, King
Needle N.S. -64 39	94 99	George's Sound.
Mag. N. -64 18 Mag. S. -64 29	. •	Covern
1135 02 117 56 Direct65 22	ſ	At the tents, King George's Sound.
Needle N. -65 04		The readings of needle A. being very
Needle N.S. $\begin{vmatrix} -04 & 48 \\ -65 & 13 \end{vmatrix}$ $\rightarrow \dots + 18$	64 52 {	discordant put in needle B., the change having
Mag. N. -65 11		tween the 7th and
Mag. S. -65 15 J	(10th of April*.

						Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845. Apr. 12.	-35 02	117 56	Direct.	$-6\mathring{5} \ 3\mathring{4}$	1	,	. /	0 / 0 /	
			Needle N.	-65 39				÷	
			Needle S. Needle N.S.	$ \begin{array}{r rrrr} -65 & 07 \\ -65 & 25 \end{array} $	}		+18	-65 07	At the tents, King
			Mag. N.	-65 21					George's Sound.*
7.0	05.00	117 50	Mag. S.	-65 23	J · · ·	,			-
19.	-35 02	117 56	Direct. Needle N.	-65 15 $-64 55$	s.				
	·		Needle S.	-64 32	s. s.	>-21	+18	-65 02	
			Direct.	-65 15	s.				
20.	-35 06	117 55	Direct.	-6629	s.e. by e.	$+12 \\ -18$	+18	$\begin{bmatrix} -65 & 59 \\ -65 & 58 \end{bmatrix}$ 65 59	Unsteady.
23.	25 20	114 95	Direct.	-65 58 $-66 33$	s. by E.	-18	+18	$[-65 \ 58]$	Chistoady.
23.	-35 30	114 35	Direct. Needle N.	-67 30	N.W.				
			Needle S.	-66 30	N.W.	>+92	+18	-6454	Very unsteady.
			Needle N.S.	-66 35	N.W.		·		
2.		00	Direct.	$-66 \ 30$	N.W.	j			
25.	-32 24	111 26	Direct.	-64 03 $-64 22$	N.w. by N.				
			Needle N. Needle S.	$-63 \ 31$	n.w. by n. n.w. by n.				
ľ			Needle N.S.		n.w. by n.	>+88	+18	-62 22	Moderate breeze, table steady.
l			Mag. N.	$-64 \ 43$	n.w. by n.				•
			Mag. S.	-64 06	n.w. by n.				
27.	-29 16	106 49	Direct.	-64 13 $-60 10$	n.w. by n.	\forall [
21.	-zg 10	100 49	Needle N.	-60 56	W.N.W.			•	
			Needle S.	_60 16	W.N.W.	>+72	+18	-59 30	Very unsteady.
			Needle N.S.		W.N.W.				
00	05 05	106 20	Direct.	-60 53	w.n.w.	J.			
28.	-27 35	106 32	Direct. Needle N.	-58 47 $-58 46$	w. by n. w. by n.	1 1			
			Needle S.	-5851	w. by N.				A heavy swell, un-
			Needle N.S.	_58 24	w. by N.	>+61	+18	-57 26	steady.
			Mag. N.	-5853	w. by n.	1			
			Mag. S.	_58 53 _58 43	w. by N.			,	
29.	$-25 \ 46$	104 55	Direct.	-56 54	w. by n.	\exists 1			
~3.			Needle N.	_56 54	N.W.		. 10	EE 05	Y
			Needle S.	$-56 \ 41$	N.W.	>+88	+18	-55 0 5	Very unsteady.
	00.50	00.06	Direct.	_56 54	N.W.	7			
May 1.	-23 58	99 06	Direct.	$-55 48 \ -55 30$	N.W.				Ungtondy
			Needle N. Needle S.	-55 22	N.W.	>+87	+18	-53 46	Unsteady.
			Needle N.S.	_55 28	N.W.				
2.	-24 01	97 25	Direct.	$-55 \ 37$	$W. \frac{1}{2} N.$	ή l			
			Needle N.	-55 58	$W \cdot \frac{1}{2} N \cdot$	>+56	+18	-54 18	Unsteady.
			Needle S. Needle N.S.	-55 01 -55 32	W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N.				
			Treenie IV.D.	-00 0%	W • 2 N •	ノー			

^{*} Captain Fitzrov having left a memorandum at King George's Sound stating that he had found local magnetic disturbance at King George's Sound, the Inclination was observed on the opposite side of the bay, on the same day as at the tents: needle B gave as follows (no correction being here applied for Index in either case):—

The distance between the two stations was between three and four miles.

						Correc	tions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.		0 4		· /			,	0 / 0 /	
May 3.	-23 50	95 56	Direct. Needle N. Needle S. Needle N.S. Direct.	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$		$\left \begin{array}{c} +56 \end{array} \right $	+18	-54 26	Unsteady.
4.	-24 17	93 50	Direct. Needle N. Needle S. Needle N.S.	-55 43 -56 08 -55 08 -55 33	W. ½ N. W.N.W. W.N.W. W.N.W.	$\left \begin{array}{c} \\ \\ \\ \end{array} \right + 72 \left \begin{array}{c} \\ \end{array} \right $	+18	-54 07	Unsteady.
5.	-24 02	92 07	Direct. Direct. Needle N.	-55 35 -54 42 -54 39	W.N.W. N.W. N.W.) }+88	+18	-52 44	Cross sea, with rolling motion.
7.	-21 44	89 38	Needle S. Direct. Needle N.	$ \begin{array}{r} -54 & 10 \\ -53 & 33 \\ -53 & 47 \\ \end{array} $	N.W. $\frac{1}{2}$ W. N.W. $\frac{1}{2}$ W.	+83	+18	-51 45	Cross sea, with
8.	-20 38	87 50	Needle S. Needle N.S. Direct. Needle N.	$ \begin{array}{rrrr} -53 & 03 \\ -53 & 19 \\ -52 & 48 \\ -53 & 18 \end{array} $	N.W. $\frac{1}{2}$ W. N.W. $\frac{1}{2}$ W. W. $\frac{1}{2}$ N.		•		rolling motion.
			Needle S. Needle N.S. Direct.	-5158	W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N.	+54	+18	-51 33	Very unsteady.
9.	-20 37	85 02	Direct. Needle N. Needle S. Needle N.S.	$ \begin{array}{r} -52 & 37 \\ -53 & 16 \\ -52 & 18 \\ -52 & 20 \end{array} $	W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N.	$\left \begin{array}{c} \\ \\ \\ \end{array} \right + 55 \left \begin{array}{c} \\ \end{array} \right $	+18	-51 21	Unsteady.
10.	-20 25	82 00	Direct. Direct. Needle N. Needle S.	$ \begin{array}{rrrr} -52 & 20 \\ -52 & 31 \\ -52 & 30 \\ -52 & 48 \end{array} $	W. $\frac{1}{2}$ N. W. $\frac{3}{4}$ N. W. $\frac{3}{4}$ N. W. $\frac{3}{4}$ N.				
			Needle N.S. Direct. Mag. N. Mag. S.		$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+68	+18	-51 05	Fresh breeze, table unsteady.
11.	-20 36	79 10	Direct. Needle N. Needle S. Needle N.S.	-53 10 -53 03 -52 41 -53 18	W. $\frac{3}{4}$ N. W. $\frac{3}{4}$ N. W. $\frac{3}{4}$ N. W. $\frac{1}{4}$ N.	$\left \begin{array}{c} \\ \\ \\ \end{array} \right + 68$	+18	51 46	Steady.
12.	-20 44	78 31	Direct. Direct. Needle N. Direct.	$ \begin{array}{r} -53 & 17 \\ -52 & 15 \\ -52 & 46 \\ \hline 52 & 46 \end{array} $	W. ¼ N. S. S.			-52 00	
			Needle N. Direct.	$ \begin{array}{r} -52 & 42 \\ -53 & 05 \\ -53 & 10 \\ \hline 52 & 57 \\ \end{array} $	s.s.w. s.s.w.	$\begin{vmatrix} 1 \\ 1 \\ 3 \end{vmatrix} + 30$	+18 +18	-52 19 -52 15	
			Needle N. Direct. Needle N. Direct.	$ \begin{array}{r} -52 & 57 \\ -53 & 11 \\ -53 & 30 \\ -53 & 06 \end{array} $	s.w. w.s.w. w.s.w.	$\begin{vmatrix} 1 \\ +44 \\ +51 \end{vmatrix}$	+18 +18	$\begin{vmatrix} -52 & 18 \\ -52 & 11 \end{vmatrix} -52 & 00$	Light air, table
	•		Needle N. Direct. Needle N. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	W. W.N.W. W.N.W.	$\left rac{1}{2} + 72 \right $	+18	-51 45	steady. The observations at N.W., N.N.W., and N. have not been included in
	,		Needle N. Direct. Needle N.		N.W. N.W. N.N.W. N.N.W.	$\begin{vmatrix} +86 \\ +68 \end{vmatrix}$	+18 +18	-50 44 -50 53	the mean.
	·		Direct. Needle N.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N. N.	$\left \begin{array}{c} 1 \\ 1 \end{array} \right + 72$	+18	-51 10	

						Corre	ctions.		
Date		-	Method	Observed			1	~	
Date.	Lat.	Long.	employed.	Inclination.	Ship's head.	Ship's attrac-	Index.	Corrected Inclination.	Remarks.
						tion.	Indon.		
1845.									
May 12.	$-20 \ 44$	78 31	Direct.	$-52^{\circ}58$	N.N.E.	+68	110	-51 33	
			Needle N.	-53 04	N.N.E.	7 +08	+18	-31 33	
			Direct. Needle N.	-53 18 $-53 30$	N.E.	+86	+18	$ -51 \ 40 > -52 \ 00$	Light air, table
			Direct.	$-53 \ 15$	N.E. E.N.E.	{			steady. The observations at
			Needle N.	-5349	E.N.E.	+72	+18	$[-52 \ 02]$	N.W., N.N.W., and N. have not
13.	-20 39	. 77 43	Direct.	-53 15	S.E.	$\left.\right\} + 30$	+18	-52 34	been included in the mean.
			Needle N. Direct.	-53 29	S.E.	1	1 20	02 01	
			Needle N.	$\begin{bmatrix} -53 & 25 \\ -53 & 41 \end{bmatrix}$	E. E.	} +51	+18	-52 15	
			Direct.	-53 05	N.E.		. 10	71.40	t to
			Needle N.	-5347	N.E.	$+86$	+18	-51 42	A rolling motion,
			Direct.	-5242	N.	$ \} -72$	+18	-51 28	not very steady at some points.
			Needle N. Direct.	$ \begin{array}{r rrr} -53 & 13 \\ -52 & 58 \end{array} $	N.	1			•
			Needle N.	-52 38 $-53 30$	N.W.	+86	+18	-51 30	
			Direct.	-53 27	w.	1	110	$\begin{bmatrix} -52 & 16 \end{bmatrix}$	
,,,		#0 OC	Needle N.	-5341	w.	+51	+18	-52 10)	
16.	-20 26	70 36 69 00	Direct.	-5352	w. by n.		-		
		0,9 00	Needle S.	$ \begin{array}{r rrr} -53 & 49 \\ -53 & 15 \end{array} $	w. by n. w. by n.	$ $ \rangle_{+62}	+18	_52 19	Unsteady.
			Needle N.S.	$-53 \ 47$	w. by n.	+02	120		
		00.04	Direct.	-53 30	w. by n.	IJ.			
17.	-20 34	69 24	Direct.	-54 05	w. by n.	Ŋ			
			Needle N. Needle S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	w. by n. w. by n.	\ \>+62	+18	-52 447	Very unsteady.
			Needle N.S.	-53 52 $-54 01$	w. by N.	+02	7.10	32 11	
			Direct.	-54 10	w. by N.	IJ			
	-20 34	69 24	Direct.	$-54 \ 41$	s.w. by w.	Ŋ		}−53 01	
		•	Needle N. Needle S.	$\begin{vmatrix} -54 & 23 \\ -54 & 00 \end{vmatrix}$	s.w. by w.				
1			Needle N.S.	-53 58	s.w. by w.	$ \rangle + 37$	+18	_53 18	Very unsteady.
			Mag. N.	-54 15	s.w. by w.				
			Mag. S.	-5409	s.w. by w.				
18.	-21 08	68 04	Direct.	$\begin{vmatrix} -54 & 06 \\ -54 & 21 \end{vmatrix}$	s.w. by w. w. by n.	+62	+18	-53 01	Unsteady.
19.		67 54	Direct.	$-55 \ 10$	w. by n.	h +02	10	-35 01	Chalcady.
			N.	-5607	w. by N.				
			S.	-5454	w. by N.	$ \rangle + 62$	+18	-53 46	Steady.
			N.S. Mag. N.	$\begin{vmatrix} -55 & 09 \\ -55 & 10 \end{vmatrix}$	w. by n. w. by n.				
20.	-21 12	67 29	Direct.	-55 23	w. by N.	К			-
			Needle N.	-5546	w. by n.				Makla wood oo 3
			Needle S.	-54 56	w. by n.	>+62	+18	-53 59	Table unsteady.
			Needle N.S. Direct.	-55 11 -55 19	w. by n. w. by n.				
21.	-21 01	66 50	Direct.	-55 19	w. by N.	K			
			Needle N.	-55 35	w. by N.				
			Needle S.	-54 40	w. by N.		. 10	79.40	Unsteady.
			Needle N.S. Mag. N.	-55 11 -55 17	w. by n. w. by n.	+62	+18	-53 49	Onsteauy.
			Mag. S.	-54 40	w. by N.				
			Direct.	-55 17	w. by n.	لِ			ŧ
22.	$-20 \ 40$	62 58	Direct.	-55 13	w. by n.	1)			
			Needle N. Needle S.	$\begin{vmatrix} -55 & 32 \\ -54 & 59 \end{vmatrix}$	w. by n. w. by n.				
			Needle N.S.		w. by N.	+62	+18	-53 53	Table steady.
-			Needle N.S.	-55 14	w. by n.]			
			Needle N.S.	-55 12	w. by n.	J			.

						Corre	ctions.	·	
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845. May 27.	-20° 09	57 31	Direct. Needle N.	$-5\overset{\circ}{3} \ 5\overset{\prime}{3} \\ -54 \ 27$	7	,	,	0 / 0 /	
			Needle S. Needle N.S. Mag. N.	-5329	 	••••••	+18	_53 38	On shore at Mauritius.
30.	-21 50	53 25	Mag. S. Direct.	-53 52 $-55 50$	s.w. by w.	J			
			Needle N. Needle S. Needle N.S.	-56 20 $-55 05$ $-55 30$	s.w. by w. s.w. by w.	$\left \begin{array}{c} +32 \end{array} \right $	+18	-54 51	Unsteady.
June 3.	-26 26	48 20	Direct. Needle N. Needle S.	$ \begin{array}{r rrr} -60 & 20 \\ -60 & 40 \\ -59 & 57 \end{array} $	n.w. by w. n.w. by w. n.w. by w.	$\left \right\rangle + 80$	+18	-58 46	Unsteady.
4.	-27 14	45 50	Needle N.S. Direct. Needle N.	$ \begin{array}{rrrr} -60 & 02 \\ -60 & 46 \end{array} $	N.w. by w. N.w. by w. N.w. by w.	$\left\{\begin{array}{c} +80 \end{array}\right.$	+18	-58 32	Very unsteady.
5.	-28 02	42 40	Needle S. Needle N.S. Direct.		N.w. by w. N.w. by w. N.w. by w.	+80		-58 10	Very unsteady.
8.		37 45	Direct. Needle N. Needle S.	-60 02	w. w.				
			Needle N.S. Mag. N. Mag. S.		W. W.	$\left \begin{array}{c} +50 \\ \end{array} \right $	+18	-59 14	Steady.
	-30 27	33 41	Direct. Needle N.	-58 12 $-58 03$	w.n.w.	$\left.\right\} + 72$	+18	-56 37	Very unsteady, a heavy sea.
13.	-31 06	31 26	Direct. Needle N. Needle S. Mag. N.S.	-59 04 $-57 33$	w. by s. $\frac{1}{2}$ s. w. by s. $\frac{1}{2}$ s. w. by s. $\frac{1}{2}$ s. w. by s. $\frac{1}{2}$ s.	$ \ \ \ \ \ \ \ \ \ \$	+18	-57 24	Very unsteady.
17.	-35 40	21 40	Direct. Direct. Needle N. Mag. N.S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$			+18	-55 31	
23.	Good Hop	Bay, Cape of pe, for local	Direct. Direct. Needle N.	$ \begin{array}{r rrr} -56 & 49 \\ -53 & 29 \\ -54 & 55 \end{array} $	w. by n. s. s.	$\left igcellet + 27 ight $	+18	-53 45	
	attra	action.	Direct. Needle N. Direct.	$ \begin{array}{r rrr} -53 & 43 \\ -54 & 59 \\ -54 & 38 \\ \hline \end{array} $	S.E. E.	$\begin{vmatrix} 1 \\ 1 \\ 1 \end{vmatrix} + 26$	·	-53 37 -53 32	
			Needle N. Direct. Needle N.	$ \begin{array}{r rrrr} -54 & 44 \\ -54 & 40 \\ -55 & 01 \end{array} $	E. N.E. N.E.	$\left \begin{array}{c} 1 \\ +87 \end{array} \right $		$\begin{vmatrix} -53 & 06 \\ -53 & 24 \end{vmatrix}$	
			Direct. Needle N. Direct.		N. N. N.W.	$\left. \begin{array}{c} +75 \\ +88 \end{array} \right.$		$\begin{bmatrix} -53 & 12 \\ -53 & 00 \end{bmatrix}$	
			Needle N. Direct. Needle N.		N.W. W. W.	$\left \right. \right. \left. \right. \right. \left. \right. + 51$			
24.		in the Dock- imon's Bay.	Direct. Needle N. Needle S.		}	J	+18	-53 37	
			Mag. N.S.	-53 12 $-54 09$					

				-	<i>;</i>	Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attrac- tion.	Index.	Corrected Inclination.	Remarks.
1845. June 30. July 2.	-33 56	18 29 18 29	Direct. Needle N. Needle S. Mag. N.S. Mag. N. Mag. S. Direct. Needle S. Mag. N.S. Mag. N.S. Mag. N. Mag. S. Direct. Needle N. Needle S. Mag. N.S.	-52 55	} }		+18	$\begin{bmatrix} -53 & 22 \\ -53 & 27 \\ -53 & 37 \end{bmatrix}$	Observed at the Magnetic Observatory, Cape of Good Hope.

Observations of the Inclination made on board Her Majesty's hired Bark "Pagoda," with Needle 1 (Fox No. 1). Face West. Time usually two hours before Noon.

Observer, Lieut. H. CLERK, Royal Artillery.

						Correc	tions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1844. Nov.10.	tory, Good	c Observa- Cape of Hope.	Direct.	$-5\overset{\circ}{3} 5\overset{\circ}{6} \\ -53 25$	Observed on shore.		+08	•	Needle A. used as de- flector, adjusted at
21.	-33 56	18 29	S. Direct. N. S.		Observed on shore.	}	+08	-53 31	40° from the apparent dip.
Dec. 19.	-34 12	18 26	Direct. N. S.		Observed on shore.		+08	53 50	Observed in the dock-yard at Si- mon's Bay.
Jan. 9.		g out of Bay.	Direct. N. S. Direct.	-54 03	s.e. by s. $\frac{1}{2}$ s. s.e. by s. $\frac{1}{2}$ s. s.e. by s. $\frac{1}{2}$ s. w. $\frac{1}{2}$ s.	>+22	+08	$\left53\ 48 \right\} -53\ 34$	A strong south-east wind, table very unsteady 2 r.m.
	94.44	18 50	N. S.	-53 58 $-54 10$	$\begin{array}{c c} W \cdot \frac{1}{2} S \cdot \\ W \cdot \frac{1}{2} S \cdot \end{array}$	+51	+08	—53 20 J	Table very unsteady.
10.	-34 44	17 50	Direct. N. S.		w. by n. w. by n. w. by n.	+61	+08	—52 56	Table unsteady.
13.	-35 12	13 28	Direct. N. S.	$ \begin{array}{r rrr} -52 & 33 \\ -52 & 03 \\ -52 & 25 \end{array} $	s.w. by w. s.w. by w.	$\left.\right\}$ + 37	+08	-51 35	Table steady. Up to the 13th of
14.	-37 25	13 24	Direct. N. S. N.S.	$ \begin{array}{r rrrr} -52 & 48 \\ -51 & 54 \\ -52 & 05 \\ -52 & 08 \end{array} $	s.w. by w.	$\left \begin{array}{c} \\ \\ \end{array} \right + 17 \right $	+13	_51 44	Up to the 13th of January the deflectors were at 40°from dip; on and after the 14th they were at the dip, so that the same observations gave dip and
15.			Direct. N. S. N.S.	$ \begin{array}{r rrr} -54 & 58 \\ -53 & 48 \\ -54 & 03 \\ -53 & 58 \end{array} $	N.w. by w.	$\left. \right\} + 79$	+13	-52 39	intensity. Very unsteady.
16.	-39 10	14 41	Direct. N. S. N.S.	$ \begin{array}{r rrrr} -55 & 33 \\ -54 & 20 \\ -54 & 58 \\ -55 & 18 \end{array} $	s.w.byw. $\frac{1}{2}$ w.	$\left \begin{array}{c} +35 \end{array} \right $	+13	-54 14	Table steady.
17.	-40 21	14 29	Direct. N. S. N.S.	$ \begin{array}{c cccc} -56 & 18 \\ -55 & 40 \\ -55 & 52 \\ -56 & 00 \end{array} $	s.w. by w.	ħ l	+13	-55 10	Much motion.
18.	42 50	13 00	Direct. N. S.	$ \begin{vmatrix} -56 & 38 \\ -55 & 40 \\ -55 & 48 \end{vmatrix} $	s.s.w. s.s.w.	+12	+13	-55 34	Much motion.
19.	_44 50	13 19	N.S. Direct. N. S.	$ \begin{vmatrix} -55 & 50 \\ -57 & 18 \\ -56 & 25 \\ -56 & 35 \end{vmatrix} $	s.s.w. s.w. by s. s.w. by s. s.w. by s.	$\left \begin{array}{c} \downarrow \\ \downarrow \\ +15 \end{array} \right $	+13	_56 14	Much motion.
21.	_47 40	12 25	N.S. Direct. N.	$ \begin{array}{rrrr} -56 & 30 \\ -56 & 43 \\ -56 & 50 \end{array} $	s.w. by s. s. by E.	$\left.\right\} + 06$	+11	-56 29	A calm, very un- steady.

						Correc	tions.	,	ι .
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.	$-48 \ 35$	10° 51	D: .	-2 00			. ,	0 / 0 /	
Jan. 22.	$-48 \ 35$	10 51	Direct. N.	-57° 23	s.w. by s.				2000
	′		S.	$\begin{vmatrix} -57 & 17 \\ -57 & 03 \end{vmatrix}$	s.w. by s. s.w. by s.	>+15	+13	-56 44	Table steady.
			N.S.	$\begin{vmatrix} -57 & 05 \\ -57 & 05 \end{vmatrix}$	s.w. by s.				, •
23.	-50 30	10 25	Direct.	-57 33	$S.W. \frac{1}{2} S.$	イー			
		•	N.	-57 33	$s.w. \frac{2}{3} s.$	>+15	. 12	E7 00	Mahla stands
			S.	-5745	$s.w. \frac{1}{2} s.$	7+13	+13	-57 02	Table steady.
			N.S.	-57 10	$s.w. \frac{1}{2} s.$	J			
24.	-5148	9 33	Direct.	-5813	s.w. by w.				
			N. S.	-57 55	s.w. by w.	>+25	+13	-57 13	1 P.M. table steady.
			N.S.	$\begin{vmatrix} -57 & 37 \\ -57 & 40 \end{vmatrix}$	s.w. by w. s.w. by w.				
25	-5253	7 53	Direct.	$\begin{bmatrix} -57 & 40 \\ -58 & 13 \end{bmatrix}$	s.w. by w.	K I		·	
~0.	-02 00	, 00	N.	$\begin{bmatrix} -56 & 15 \\ -57 & 20 \end{bmatrix}$	s.w. by w.				
			S.	-57 40	s.w. by w.	+25	+13	-57 03	Table rather un- steady.
	·		N.S.	-57 30	s.w by w.				
26.	-5352	6 07	Direct.	-58 23	w. by s.	ήI			
			N.	-57 55	w. by s.	>+46	⊥13	-57 01	Table very steady.
1			S.	-57 40	w. by s.	(+ 10	1-10	0, 01	Table very steady.
2-	00	- -0	N.S.	-58 03	w. by s.	IJ I			
27.	-55 08	5 50	Direct.	-58 38	s.s.w. $\frac{1}{2}$ w.				
			N. S.	-57 28	S.S.W. ½ W.	>+16	+13	-57 26	Table very un-
			N.S.	$\begin{vmatrix} -57 & 25 \\ -58 & 10 \end{vmatrix}$	S.S.W. $\frac{1}{2}$ W. S.S.W. $\frac{1}{2}$ W.				steady.
30.	$-60 \ 43$	4 00	Direct.	-61 23	S. S. W. 2 W.	Н .			
	00 10		N.S.	-61 20	s.	-08	+24	-61 06	
			Direct.	-61 03	s.E. by E.	1	1.004	60 14 50 50	
			N.S.	-60 58	s.E. by E.	$\left.\right\} + 22$	+24	$-60 \ 14 > -59 \ 58$	Table unsteady.
ŀ	41.		Direct.	-60 08	N.	$+85$	+24	_58 35	
			N.S.	$-60 \ 40$	N.	J +00	1 21	-00 00)	
31.	-61 05	9 03	Direct.	-61 32	s.E. by s.				
			N. S.	$\begin{vmatrix} -61 & 35 \\ -61 & 13 \end{vmatrix}$	s.E. by s.	> 00	+13	-61 01	Table steady.
			N.S.	$\begin{bmatrix} -61 & 15 \\ -60 & 35 \end{bmatrix}$	s.e. by s.				
Feb. 2.	-61 54	16 23	Direct.	-64 18	E.S.E.	K			
I Cot 2.	-01 51	10 70	N.	$-63 \ 30$	E.S.E.		. 10	Co. 00	
			S.	-63 30	E.S.E.	>+30	+13	-63 00	Table unsteady.
,			N.S.	_63 33	E.S.E.				
3.	-61 50	19 13	Direct.	-65 13	E.S.E.	Ď l			
			N.	-64 18	E.S.E.	>+25	+13	-63 55	Table very steady.
			S.	-64 28	E.S.E	""		00 00	Lusic for stoudy.
4	60.00	20 25	N.S.	-64 13	E.S.E.	K			
4.	-62 00	20 20	Direct.	$\begin{vmatrix} -65 & 33 \\ -64 & 43 \end{vmatrix}$	S.S.E.				
			S.	$-64 \ 35$	S.S.E. S.S.E.	$\rangle -15$	+13	-64 55	Table very steady.
			N.S.	-64 40	S.S.E.				
6.	-64 20	24 05	Direct.	-67 03	S.S.E.	\preceq			
			N.	-66 13	S.S.E.	\ _18	1 12	_66 37	
			S.	-66 20	S.S.E.	7-18	+10	-00 57	Table very steady.
-	0	20.22	N.S.	-66 30	S.S.E.	Ŋ			
7.	-65 34	28 30	Direct.	-67 18	S.S.E. $\frac{1}{2}$ E.		-		
			N.	-67 00	S.S.E. 1 E.	>-16	+13	-66 59	Table very steady.
			S. N.S.	$\begin{vmatrix} -66 & 40 \\ -66 & 45 \end{vmatrix}$	S.S.E. $\frac{1}{2}$ E.				
a	-66 30	36 46	Direct.	-69 13	S.S.E. ½ E.	K			
3.	-00 00	50 10	N.	$\begin{bmatrix} -69 & 10 \\ -69 & 10 \end{bmatrix}$	E. E.			Co. 10	
•			S.	-69 03	E.	>+40	+13	-68 16	Table very steady.
	, 1		N.S.	-6908	E.	1 1		1	1 .

						Correc	tions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's		Corrected Inclination.	Remarks.
			empioyeu.	Inclination.		attrac- tion.	Index.	V 1	
1845.	$-66^{\circ} 43^{'}$		4.	00 /			· .	0 / 0 /	
Feb. 10.	-66 43	38 49	Direct. N.	$ \begin{array}{r rrrr} -69 & 28 \\ -69 & 08 \end{array} $	s.s.w.			1	
			S.	-69 08 $-69 03$	S.S.W.	>-26	+13	-69 22	Table very steady.
			N.S.	-68 58	s.s.w.	J ·			
11.	-67 35	39 31	Direct.	-71 28	N.E.	ا ا		Co. 40	
	1		N. S.	$ -71 ext{ } 43 $	N.E.	>+89	+13	-69 49	Table very steady 8 r.m.
12.	$-66 ext{ } 45$	39 23	Direct.	-71 23 $-70 08$	S.S.E.	K. 1	•	٠.	
			N.	-70 10	S.S.E.	>-30	+13	-70 12	Table very unsteady
			S.	$-69 \ 45$	S.S.E.		7-10	,0 12	
13.	-67 00	40 07	N.S. Direct.	$\begin{bmatrix} -69 & 35 \\ -70 & 43 \end{bmatrix}$	S.S.E. E.N.E.	K 1		,	
-00	0, 00	10 0,	N.	-71 10	E.N.E.	CC	. 10	Co. 20	
			S.	-7128	E.N.E.	>+66	+13	-69 39	Table steady.
16	C4 50	00.07	N.S.	$-70 \ 30$	E.N.E.	إيرا	. 00	CC 95#7	
16.	-6452	38 37	Direct. Direct.	$-68 32 \\ -68 53$	N.N.E. S. 3/4 E.	$^{+85}$	+32	68 40	Table very unsteady,
			N.	-68.08	S. $\frac{3}{4}$ E.	>-26	+13	$-68 \ 40 \ \int$	ship pitching much.
			S.	-68 20	S. 3/4 E.]			
17.	-6452	40 12	Direct. N.	-70 08	N. by w.	,			
			S.	$egin{array}{c c} -70 & 32 \\ -70 & 25 \\ \end{array}$	n. by w. n. by w.	>+80	+13	-68 44	Table very unsteady, heavy swell.
		:	N.S.	-70 02	n. by w.	JI			neavy swen.
18.	-6422	40 49	Direct.	$ -68 \ 13 $	s. by E.				
		-	N.	-68 25	s. by E.	}−29	+13	-68 40	Table very unsteady.
19.	-63 49	42 00	S. Direct.	$\begin{bmatrix} -68 & 35 \\ -70 & 33 \end{bmatrix}$	s. by E. E. by s.	$\langle \cdot \cdot \rangle$,		
-3.	00 13	12 00	N.	-70 03	E. by s.		. 10	Co ac	
			S.	-70 20	E. by s.	>+28	+13	-69 36	Table very unsteady б г.м.
20	-63 22	45 05	N.S.	$-70 \ 13$	E. by s.	7			
20.	-03 zz	45 35	Direct. S.		s.e. by e.½ e. s.e. by e.½ e.	>+13	+21	-70 03	Table very unsteady
			N.S.		s.e. by E. ½ E.	[10	, ~=	, 0 00	zuszo vory unsteady
21.	$-63 \ 36$	46 41	Direct.	-70 03	S.S.E.)			
		-	N. S.	$-70 \ 18$	S.S.E.	>-28	+13	-70 02	Table unsteady.
			N.S.	$\begin{bmatrix} -69 & 35 \\ -69 & 10 \end{bmatrix}$	S.S.E. S.S.E.				,
24.	$-62 \ 36$	51 40	Direct.	$-69 \ 48$	E.		+ 24	-68 3 97	Taken at 10 A.M.,
	-		N.S.	$-69 \ 40$	E.	+41	T 24	69 13	table very un- steady, ship
			Direct.	-70 28	Е.	ارزيا	112	60.46	pitching violently.
			N. S.	$-70 13 \\ -71 20$	E. E.	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	A 19	-69 46J	Taken at 5 P.M.
25.	-61 25	53 38	Direct.	-71 28	E.S.E.	j		•	
			N.	-71 18	E.S.E.	×+12	+13	-70 46	Table unsteady.
			S. N.S.	-71 00	E.S.E.		,	, .	
26.	-61 17	57 28	Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.S.E. S.E. ¹ / ₂ E.	\prec \mid			
			N.	$-72 \ 43$	S.E. $\frac{1}{2}$ E.	>-11	119	70 01	Table unsteady.
1			S.	-7148	S.E. ½ E.		+13	-72 01	ranc unsteatty.
97	-61 00	64 03	N.S. Direct.	-71 28	S.E. ½ E.	∤		**	
~1.	-01 00	07 U	N.	$ \begin{array}{r rrr} -73 & 28 \\ -73 & 15 \end{array} $	S.E. $\frac{1}{2}$ S. S.E. $\frac{1}{2}$ S.			FO. 07	
	-		S	-73 38	S.E. $\frac{1}{2}$ S.	>-21	+13	-73 27	Table steady.
90	61.00	70.40	N.S.	-7255	S.E. $\frac{1}{2}$ S.	\downarrow \downarrow			
28.	$-61 \ 36$	70 46	Direct. N.	$ \begin{array}{r rrr} -73 & 43 \\ -73 & 55 \end{array} $	S.S.E.				***
			S.	$-73 \ 35$ $-73 \ 35$	S.S.E.	>-38	+13	-74 02	Table unsteady, heavy swell.
. 1	.		N.S.	$-73 \ 15$	S.S.E.	j			- - -

^{*} Error, probably in the degree noted; result not included in the mean.

						Correc	ctions.		
.	T .	T	Method	Observed	Ship's	Cl.:/a		0	
Date.	Lat.	Long.	employed.	Inclination.	head.	Ship's attrac-	Index.	Corrected Inclination.	Remarks.
						tion.			
1845.								0 4	
Mar. 1.	$-62^{\circ}10$	72 25	Direct.	$-7\mathring{4}$ 1 $\mathring{3}$	S.S.E.	n 1			
		1	N.	-74 23	S.S.E.	-38	+13	-74 35	Table steady.
			S. N.S.	$\begin{vmatrix} -74 & 20 \\ -73 & 43 \end{vmatrix}$	S.S.E. S.S.E.		,		2.000
2.	-62 40	76 09	Direct.	-74 28	s.	K I			1 3 x x y x
,	,		N.	-74 13	s.	>-46	+13	-74 50	Table very steady.
			S.	-74 23	s.	(- 10	7.10	-7± 00	
3.	-64 20	79 38	N.S. Direct.	$\begin{bmatrix} -74 & 03 \\ -75 & 53 \end{bmatrix}$	s. by w. $\frac{1}{2}$ w.	K			
•/•	-04 20	19 50	N.	$-76 \ 45$				50 0.	
			S.		s. by $w.\frac{1}{2}w$.	-43	+13	-76 34	Table unsteady.
_		04.40	N.S.	$-75\ 10$	s. by w. $\frac{1}{2}$ w.	.IJ			
5.	-61 38	84 40	Direct. N.	$\begin{vmatrix} -76 & 13 \\ -76 & 10 \end{vmatrix}$	S.E.]			
			S.	$-76 \ 38$	S.E.	>-23	+13	-76 27	Table unsteady.
			N.S.	-7608	S.E.]]			
6.	-6042	80 12	Direct.	-77 23	N.E. $\frac{1}{2}$ N.	1			
			N. S.	-77 08	N.E. $\frac{1}{2}$ N.	+82	+13	-75 43	Table unsteady.
			N.S.	$\begin{vmatrix} -77 & 23 \\ -77 & 18 \end{vmatrix}$	1 7				1
7.	-61 20	91 09	Direct.	-7628	s. by E.	K			
-			N.	-77 20	s. by E.	-49	+13	-77 23	Table very unsteady,
			S. N.S.	-7718		1	'		taken at 10 A.M.
	_61 26	91 20	Direct.	$\begin{vmatrix} -76 & 02 \\ -77 & 18 \end{vmatrix}$	s. by E. s.w. by s.	K		>77 35	Taken at 5 P.M. in consequence of the
	-01 20	31 20	N.	-77 28	s.w. by s.	1		10	A.M. observations being unsatisfac-
			S.	-77 50	s.w. by s.	-35	+13	$[-77 \ 46]$	tory. The aurora was very brilliant
	0	00.00	N.S.	-7700		Ŋ			all the previous and succeeding
8.	-61 14	92 03	Direct. N.	$\begin{vmatrix} -79 & 03 \\ -79 & 43 \end{vmatrix}$		11 _			nights. Table steady.
			S.	-7905		+26	+13	-78 26	Table steady, light N.W. swell.
			N.S.	-78 30		IJ			N.W. Swell.
9.	$-60 \ 35$	92 25	Direct.	-78 13		Ŋ			
			N. S.	-78 25 $-78 15$		>+26	+13	-77 30	Table unsteady.
			N.S.	-7742					
10.	-60 03	95 36	Direct.	-76 27		ď.			
			N.	-7730		>-37	+13	-77 35	Table very unsteady.
11	_59 52	99 30	S. Direct.	$\begin{vmatrix} -77 & 35 \\ -80 & 03 \end{vmatrix}$		K			
- 11.	- 59 52	33 00	N.	-80 23				#0 01D	Table very unsteady,
			S.	-79 25	$E \cdot \frac{1}{2} S$.	+15	+13	-79 21	taken at 10 A.M.
		00.00	N.S.	-79 23		IJ		>79 36	Table steady, taken
	-59 59	99 39	Direct. N.	$\begin{vmatrix} -80 & 28 \\ -81 & 05 \end{vmatrix}$					at 6 P.M.
1			S.	-80 50	$E. \frac{1}{2} N.$	>+30	+13	-79 51	
İ			N.S.	-79 53	E. $\frac{1}{2}$ N.				
13	-57 35	99 28	Direct.	-7918		1 +11	+14	-78 36	Table very unsteady, taken at 6 P.M.
14	56 E	101 24	N.S.	$\begin{vmatrix} -79 & 03 \\ -78 & 33 \end{vmatrix}$		K			
14	56 53	101 24	Direct.	$-78 33 \\ -79 38$				70.40	1
			S.	-79 22	E. by s.	+12	+13	-78 40	Table very unsteady.
			N.S.	-7848	E. by s.	IJ			
15	-55 59	2 103 06	Direct.	-79 18 $-80 28$				_	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
1.			S.	-80 28 $-80 03$		+39	+13	-78 56	Table very unsteady.
l			N.S.	-79 23					
							1		

						Corre	ctions.		
Date.	Tet	Long	Method	Observed	Ship's head.	Ship's		Corrected Inclination.	Remarks.
Date.	Lat.	Long.	employed.	Inclination.	omp s nead.	attrac-	Index.	Corrected Inciniation.	Nemarks.
1845.				0 1			,	0 / 0 .	
Mar. 16.	$-54^{\circ}48$	106 04	Direct.	-7933	N.E.				
			N.	-80 03	N.E.	>+78	+13	-78 09	Table very unsteady.
			S. N.S.	$\begin{vmatrix} -79 & 25 \\ -79 & 38 \end{vmatrix}$	N.E.				
17.	-54 17	108 05	Direct.	-78 23	S.E.	K		*	
- ' '			N.	-79 38	S.E.	>-30	+13	−79 16)	
			S.	-78 55	S.E.	١		78 49	Table very unsteady,
			Direct. N.	-78 38	E.	$\left \right\rangle + 24$. 19		ship pitching vio- lently.
			S.	-78 58 -79 18	E. E.	7+24	+13	-78 21 J	lentry.
18.	-53 00	110 08	Direct.	-79 28	N.N.E. $\frac{1}{2}$ E.	Κ Ι			
-0.			N.	-7855	N.N.E. $\frac{1}{2}$ E.	>+82	. 19	77 00	
	1		S.	-7848	N.N.E. $\frac{1}{2}$ E.	7+02	+15	-77 28	Table very unsteady.
	F 3 00	111 00	N.S.	-7900	N.N.E. $\frac{1}{2}$ E.				
19.	-51 20	111 23	Direct. S.	$-78 08 \\ -78 48$	N.N.E. $\frac{1}{2}$ E. N.N.E. $\frac{1}{2}$ E.	>+85	⊥ 21	-76 41	L
			N.S.	-78 25	N.N.E. $\frac{1}{2}$ E.	(100	T 21	-70 41	Table very unsteady, heavy swell.
20.	-49 01	111 47	Direct.	-77 38	N.E. by N.	ň l			
			N.	-78 38	n.e. by n.	>+82	+13	-76 30	Table unsteady, very
	Ī		S.	-78 30	N.E. by N.	(, 5	, 20	70 00	heavy swell.
90	-47 21	115 15	N.S. Direct.	$-77 33 \\ -76 43$	n.e. by n.	\forall 1			
22.	-4/ 21	115 15	N.	$-70 43 \\ -77 13$	E.N.E.				
			S.	-77 03	E.N.E.	>+58	+13	-75 31	Table steady, light
			N.S.	-7548	E.N.E.	J			swell.
25.	-43 20	116 52	Direct.	-73 23	N. $\frac{1}{2}$ E.)			
			N. S.	-75 45	$N \cdot \frac{1}{2} E \cdot$	>+76	+13	-7245	Table very unsteady,
	l		N.S.	$-74 ext{ } 48 \ -72 ext{ } 58$	N. $\frac{1}{2}$ E. N. $\frac{1}{2}$ E.				heavy swell from W.
26.	-41 18	116 09	Direct.	$-71 \ 33$	N. by w.	۲ ۱		·	
			N.	-71 33	N. by w.	>+80	⊥13	-70 11	Table unsteady,light
			S.	-72 15	N. by w.	7+00	1 10	,0 11	swell.
07	-38.52	116 15	N.S. Direct.	$-71 \ 33 \ -70 \ 23$	N. by w.	1			
27.	- 36 32	110 10	N.	-70 25 $-70 45$	N. by w.				
			S.	-70 50	N. by w.	>+80	+13	-68 49	Table steady.
		İ	N.S.	-6928	n. by w.	J			
28.	—37 03	116 57	Direct.	$-68 \ 33$	N. by E.)			
j i			N. S.	$-68 \ 48 \ -68 \ 13$	n. by E. n. by E.	>+83	+13	-66 46	Table very steady,
		- 1	N.S.	-67 53	N. by E.	1			nearly calm.
29.	-36 12	-116 50	Direct.	-67 30	N.N.E.	ή			
			N.	-67 13	N.N.E.	>+84	+13	-65 28	Table unsteady.
		.	S.	-66 55	N.N.E.		,	32 70	
30	-35 18	117 07	N.S. Direct.	$-66 ext{ } 43 \\ -67 ext{ } 28$	N.N.E. N.E. ½ E.	۲ ۱		,	
50.	00 10	11, 0,	N.	-68 00	N.E. $\frac{1}{2}$ E.	1	. 10	6r 40	
			S.	-67 48	N.E. $\frac{1}{2}$ E.	+86	+13	-65 48	Table unsteady.
	27.25		N.S.	-66 30	N.E. $\frac{1}{2}$ E.	J			
April 7.	-35 02		Direct.	-65 28 65 36	Observed	,			:
	King G Sou		N. S.	$-65 36 \\ -65 30$	on shore.	}	+13	-65 11	
	Sou		N.S.	-65 03]	,		6.	em 1
11.	King G		Direct.	-65 28))	. :	>-65 11	The observations were made at the
	Sou	nd.	N.	-65 28	Observed	.	+13	-65 11	same place that was used by Captains
		. :	S.	$-65 \ 31 \\ -65 \ 09$	on shore.	1		· · ·	FLINDERS and FITZROY.
			N.S.	-00 09	J)			

						Correc	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845. April 1 9 .		nor in the und.	Direct. N.S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.s.w. s.s.w.	} –16	+24	-64 46) · ·	
,			Direct. N.S.	$ \begin{array}{r rrr} -65 & 49 \\ -65 & 25 \end{array} $	s.w. s.w.	$\left.\right\} + 01$	+24	-65 12	
			Direct. N.S.		w.s.w. w.s.w.	$\left.\right\} + 23$	+24	-64 57	
	•	ion.	Direct. N.S. Direct.		W. W. W.N.W.	}+46	+24	-64 41	
		ttract	N.S. Direct.	$ \begin{array}{c cccc} -66 & 03 \\ -66 & 35 \end{array} $	W.N.W. N.W.	} +70	+24	-64 39	
		To obtain corrections for the ship's attraction.	N.S. Direct.	$\begin{vmatrix} -66 & 16 \\ -66 & 50 \end{vmatrix}$	N.W.		$+24 \\ +24$	$-64 \ 30$ $-64 \ 52$	
		the sh	N.S. Direct.	-66 29 $-66 29$	N.N.W. N.	$\begin{cases} +84 \\ +84 \end{cases}$	$+24 \\ +24$	-64 34	
		s for 1	N.S. Direct. N.S.	$ \begin{array}{r} -66 & 14 \\ -66 & 48 \\ -66 & 26 \end{array} $	N. N.N.E.	} +83	+24	$-64\ 50$ $-64\ 51$	The table was very steady during these observations.
	-	ection	Direct. N.S.		N.N.E. N.E. N.E.	+92	+24	-64 26	1
		corre	Direct. N.S.	$\begin{bmatrix} -66 & 27 \\ -66 & 00 \end{bmatrix}$	E.N.E. E.N.E.	+70	+24	-64 40	
		btain	Direct. N.S.	$\begin{vmatrix} -66 & 37 \\ -66 & 21 \end{vmatrix}$	E. E.	$\left.\right\} + 46$	+24	-65 19	÷
	ŕ	To 6	Direct. N.S. Direct.		E.S.E. E.S.E. S.E.	$\left. \left. \left. \right\} +23\right \right.$	+24	-65 11	·
			N.S. Direct.	$\begin{bmatrix} -65 & 19 \\ -65 & 13 \end{bmatrix}$	S.E. S.S.E.	$\left.\begin{array}{c} +01 \\ 1 \end{array}\right.$	+24	-65 11 C4 50	
			N.S. Direct.	-64 58 $-65 11$	S.S.E. S.	$\begin{cases} -16 \\ -21 \end{cases}$	$+24 \\ +24$	$ \begin{array}{c c} -64 & 58 \\ -64 & 57 \end{array} $	
23.	—35 36	114 44	N.S. Direct.	-64 46 $-66 53$	s. N.W.	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	T 22	01 01)	
,			N. S. N.S.	$ \begin{array}{r} -67 & 45 \\ -67 & 40 \\ -66 & 33 \end{array} $	N.W. N.W.	+92	+13	-65 28	Table unsteady.
24.	-34 16	113 01	Direct. N.	$ \begin{array}{r rrrr} -66 & 33 \\ -66 & 28 \end{array} $	n.w. by n. n.w. by n.	}		-64 44	
			S. N.S.		n.w. by n. n.w. by n.	}+88	+13	-04 44	Table unsteady.
25.	-32 32	111 36	Direct. N. S.	$ \begin{array}{r rrr} -63 & 48 \\ -64 & 25 \\ -63 & 55 \end{array} $	n.w. by n.	+88	+13	-62 14	Table unsteady.
27.	-29 20	106 55	N.S. Direct.		n.w. by n. n.w. by n. w.n.w.				
			N. S.		w.n.w.	>+72	+13	-59 19	Table steady.
28.	-27 47	106 36	N.S. Direct.	$\begin{bmatrix} -60 & 33 \\ -58 & 28 \end{bmatrix}$	w.n.w. n. by w. ½ w.	$\{ \ \ $		· · · · · · · · · · · · · · · · · · ·	. *
			N. S. N.S.	-58 25	N. by w. ½ w. N. by w. ½ w. N. by w. ½ w.	+76	+13	-57 17	Table very unsteady, heavy swell.
29.	—26 00	105 11	Direct. N.	-56 38 -56 48	N.W. N.W.	7	, 10	55 00	(Daldana
		1.41	S. N.S.	$-57 08 \\ -56 45$	N.W. N.W.	+88	+13	—55 09	Table very unsteady, very heavy swell.

						Correc	ctions.	- :	
Date.	Lat.	Long.	Method	Observed	Ship's head.	Ship's		Corrected Inclination	Remarks.
24.01			employed.	Inclination.	1	attrac- tion.	Index.		
1845. Mars 1	$-2\mathring{4} 00$	റ്റ് ഒ	Direct.	-55 [°] 18	777	5 4	,	0 / 0	,
May 1.	-24 00	99 20	N.	-55 55	w. w.			74.00	
			S.	-56 13	w.	$\rangle + 51$	+13	-54 28	Table very unsteady, considerable mo-
	04.08	07 90	N.S.	-54 43	w.	Į			tion.
2.	-24 01	97 30	Direct. N.	$-55 03 \\ -55 20$	w. w.				
			S.	-55 28	w.	$\rangle + 51$	+13	-54 03	Table steady.
_		00.00	N.S.	$-54 \ 35$	w.	Į			
3.	-24 00	96 06	Direct. N.	-55 18	$W \cdot \frac{1}{2} N \cdot W \cdot \frac{1}{2} N \cdot$				
			S.	-55 30	$W \cdot \frac{1}{2} N \cdot$	> +56	+13	-54 16	Table steady.
			N.S.	-55 38	$W \cdot \frac{1}{2} N \cdot$				
6.	$-22 \ 47$	91 00	Direct. N.	-54 28	N.W.	Π.			
			S.	$-54 40 \\ -54 28$	N.W.	>+87	+13	-52 49	Table very unsteady, heavy swell from W.
		,	N.S.	-54 18	N.W.	IJ			neavy swen from w.
7.	-21 50	89 44	Direct.	-5328	N.W.	n	·		
			N. S.	$-53 53 \\ -54 08$	N.W.	>+86	+13	-52 17	Table very unsteady,
			N.S.	-54 13	N.W.				heavy W. swell.
8.	-20 46	87 59	Direct.	-52 28	n.w. by w.	ň.			
			N. S.	$\begin{bmatrix} -53 & 03 \\ -52 & 58 \end{bmatrix}$	n.w. by w.	>+82	+13	-51 067	
			N.S.	-52 38 $-52 13$	n.w. by w.				_
			Direct.	-52 13	N.w. by w.	K		\rightarrow -50 5	7 Table steady. Observer Mr. Bur-
		·	N.	-5233	n.w. by w.	+82	+13	-50 48	DON, R.N. Table steady.
			S. N.S.	$\begin{vmatrix} -52 & 30 \\ -52 & 15 \end{vmatrix}$	n.w. by w.				Table steady.
9.	-20 38	85 26	Direct.	-52 03	$W \cdot \frac{1}{2} N \cdot$	K			
			N.	-52 35	$W_{\bullet} = \frac{1}{2} N_{\bullet}$	+56	+13	-51 14	Table very unsteady,
			S. N.S.	$\begin{vmatrix} -52 & 15 \\ -52 & 38 \end{vmatrix}$	$W \cdot \frac{1}{2} N \cdot W \cdot \frac{1}{2} N \cdot$	Ι (΄	'		heavy swell.
10.	-20 26	82 22	Direct.	-5243	$W \cdot \frac{1}{2} N \cdot$	K		v v de e	
	1.1		N.	-53 00	$W \cdot \frac{1}{2} N \cdot$	+56	+13	-51 40	Table very unsteady.
			S. N.S.	$\begin{vmatrix} -52 & 58 \\ -52 & 33 \end{vmatrix}$	$\begin{array}{c c} W \cdot \frac{1}{2} N \cdot \\ W \cdot \frac{1}{2} N \cdot \end{array}$		'		
			Direct.	-52 49	$\begin{array}{c} W \cdot \frac{1}{2} N \cdot \\ W \cdot \frac{1}{4} N \cdot \end{array}$	K	į	>-51 3	9
			N.	-5247	$W \cdot \frac{1}{4} N \cdot$	+53	+13	_51 37	Table very unsteady.
		·	S.	-52 25	W. 1 N.	16,00	+10	1 0. 0,	Observer Mr. Bur- Don, R.N.
11.	-20 36	79 22	N.S. Direct.	$\begin{bmatrix} -52 & 50 \\ -52 & 43 \end{bmatrix}$	$W \cdot \frac{1}{4} N \cdot W \cdot \frac{1}{4} N \cdot W \cdot \frac{1}{4} N \cdot \frac{1}$	K			
^^	~ 50		N.	-5245	$\mathbf{W} \cdot \frac{1}{4} \mathbf{N}$.	$\begin{vmatrix} \\ \\ \\ \\ \end{vmatrix} + 53$	+13	-51 55	Table very unsteady.
			S.	-53 05	$\mathbf{W} \cdot \frac{1}{4} \mathbf{N} \cdot$	\ + 33	719	01.00	Observer Mr. Bur- Don, R.N.
			N.S. Direct.	$\begin{vmatrix} -53 & 30 \\ -52 & 38 \end{vmatrix}$	$W \cdot \frac{1}{4} N \cdot W \cdot \frac{1}{4} N \cdot$	K			DON, IV.IV.
		*	N.	$-52 \ 40$	$\mathbf{w}. \frac{4}{4} \mathbf{N}.$		+13	-51 44	Table unsteady.
			S.	-5308	W. 1/4 N.	> + 33	T13	01 77	Lanc unsteady.
12.	-20 44	78 31	N.S. Direct.	$\begin{bmatrix} -52 & 53 \\ -54 & 08 \end{bmatrix}$	W. 1/4 N.	K	1:		
12.	20 44	10 01	N.S.	-53 55	w. w.	$+51$	+24	$ -52 \ 47$	
			Direct.	-53 38	w.n.w.	$\frac{1}{1} + 72$	+24	-51 55	
			N.S. Direct.	$\begin{bmatrix} -53 & 23 \\ -53 & 23 \end{bmatrix}$	W.N.W.	{			
			N.S.	-53 25 -53 30	N.W.	$ \} + 86$	+24	-51 37	
			Direct.	-5253	N.N.W.	$\left \right + 68$	+24	-51 20	
		-	N.S.	-5250	N.N.W.	11	1	$\begin{vmatrix} -51 & 20 \\ -51 & 01 \end{vmatrix} -52 & 0$	2
			Direct.	-52 43	N.	+70	+ 3%	-01 01 7-02 (

						Correc	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.				/		,	,	0 / 0 /	
May 12.	-20° 44	78 31	Direct. N.S.	$-5\overset{\circ}{3}4\overset{\circ}{8}$	N.N.E.	$ \} + 68$	+24	-51 54 > -52 03	1
			Direct.	$\begin{bmatrix} -53 & 03 \\ -52 & 48 \end{bmatrix}$	N.N.E. S.				
	l		N.S.	-52 33	s.	+15	+24	-52 01	
			Direct.	-5348	s.s.w.	$\frac{1}{1}$ + 19	+24	-52 46	l leaves
			N.S.	-53 10	s.s.w.	Į		-32 40	
	1		Direct. N.S.	$ \begin{array}{r rrr} -53 & 43 \\ -53 & 03 \end{array} $	S.W.	+30	+24	-52 29	
'			Direct.	-53 03 $-53 48$	S.W. W.S.W.	}	. 24		To obtain correc-
			N.S.	-53 38	w.s.w.	$\left \right. \right. \left. \right. + 44$	+24	-52 35	tions for the
13.	-20 39	77 43	Direct.	-5348	w.	$\frac{1}{2} + 51$	+24	_52 427	tion. Calm, table very unsteady,
			N.S.	-54 05	w.	1		0.2 1.2	considerable rolling motion.
			Direct. N.S.	$\begin{vmatrix} -53 & 28 \\ -53 & 13 \end{vmatrix}$	N.W.	+86	+24	-51 30	I Ioming motion.
			Direct.	-52 58	N.	, 70	. 04		
			N.S.	-5245	N.	$ \} + 70$	+24	$\begin{vmatrix} -51 & 18 \\ -51 & 59 \end{vmatrix}$	
			Direct.	-53 23	N.E.	} +86	+24	-51 24	
			N.S. Direct.	-53 05 $-53 53$	N.E.	ΙĮ			
			N.S.	-53 30 $-53 30$	E. E.		+24	-52 27	
			Direct.	-5348	S.E.	$\frac{1}{2} + 30$	101	50.94	
			_N.S.	-53 08	S.E.	+30	+24	-52 34	
14.	-20 29	76 22	Direct.	-53 08	$W \cdot \frac{1}{2} N \cdot$	ו		1	
			N. S.	$\begin{bmatrix} -53 & 00 \\ -53 & 35 \end{bmatrix}$	$W \cdot \frac{1}{2} N \cdot W \cdot \frac{1}{2} N \cdot$	>+56	+13	-52 13	Table very unsteady.
			N.S.	-53 43	W. 1 N.				
		1.	Direct.	-53 38	$W_{\bullet} = \frac{1}{2} N_{\bullet}$	ň.		\rightarrow -52 20	
			N.	-53 48	$W_{\bullet} = \frac{1}{2} N_{\bullet}$	+56	+13	-52 27	Table very unsteady.
			S. N.S.	-53 50	$W. \frac{1}{2} N.$			1	Observer Mr. Burdon, R.N.
16	-20 28	70 46	Direct.	-53 08 $-54 08$	$\begin{array}{c c} W \cdot \frac{1}{2} N \cdot \\ W \cdot \frac{1}{4} N \cdot \end{array}$	K			
10.	20 20	•••	N.	-53 48	$\mathbf{W} \cdot \frac{1}{4} \mathbf{N}$	+53	. 19	-52 51	
			S.	-53 53	$W. \frac{1}{4} N.$	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	+13	-52 51	Table steady.
,,	27.00	68 12	N.S.	-53 58	W. $\frac{1}{4}$ N.	Į			
18.	-21 06	08 12	Direct. N.	$\begin{bmatrix} -54 & 43 \\ -53 & 45 \end{bmatrix}$	w.s.w.				
			S.	-54 05	w.s.w.	+44	+13	-53 10	Table very unsteady.
	1 to		N.S.	-53 53	w.s.w.	IJ			
19.	-21 11	67 54	Direct.	-54 28	n.w. by n.)			
			N. S.	$-54 35 \\ -54 23$	n.w. by n.	\\ \+77	+13	$ -52 54\rangle$	Table steady, nearly
1			N.S.	-54 08	n.w. by n.				calm.
Ì			Direct.	-54 53	n.w. by n.	K		>-53 02	2 P.M.
			N.	-54 45	n.w. by n.	+77	+13	-53 10	Table steady. Ob-
			S. N.S.	-54 38	N.w. by N.		1		server Mr. Bur- bon, R.N.
20.	-21 12	67 29	Direct.	$\begin{bmatrix} -54 & 23 \\ -55 & 03 \end{bmatrix}$	w. by n.	K			DON, 16.14.
	~	٠, ٣٥	N.	-54 58	w. by N.	$\begin{vmatrix} \\ \\ \\ \end{vmatrix} + 63$	19	52 467	Table stee 3
			S.	-55 08	w. by N.	1>+03	+13	$[-53 \ 46]$	Table steady.
	.	. 4	N.S.	-54 58	w. by N.	Ŋ,		>−53 39	
	,		Direct. N.	-54 58 $-54 45$	w. by n. w. by n.				
			S.	-55 00	w. by N.	>+63	+13	$[-53 \ 32]$	Table steady. Ob- server Mr. Bur-
			N.S.	-54 28	w. by N.				DON, R.N.
		-		l .					

						Correc	tions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845. May 21.	—21°02	66° 02	Direct. N. S.	-55 28 -55 13 -55 23	w. by n. w. by n. w. by n.	$\left.\begin{array}{c} \\ \\ \\ \end{array}\right. + 63$	+13	-54 03	Table steady.
23.	-20 31	59 42	N.S. Direct. N. S. N.S.	$ \begin{array}{r rrrr} -55 & 13 \\ -55 & 28 \\ -55 & 00 \\ -55 & 23 \\ -55 & 07 \end{array} $	w. by n. w. by n. w. by n. w. by n. w. by n.	$\left.\right\rangle + 63$	+13	—53 59	Table very unsteady.
27.	Port Mau	57 31 Louis, critius.	Direct. N. S. N.S.	$ \begin{array}{r rrrr} -54 & 27 \\ -54 & 22 \\ -54 & 59 \\ -54 & 01 \end{array} $	Observed on shore.		+13	-54 14	Observed by Lieut. Moore, R.N.
	-21 44	-	Direct. N. S. N.S.	$ \begin{array}{r rrrr} -55 & 33 \\ -55 & 20 \\ -55 & 28 \\ -55 & 35 \end{array} $	$ \begin{array}{c} \text{W.S.W.} \frac{1}{2} \text{ W.} \\ \text{W.S.W.} \frac{1}{2} \text{ W.} \\ \text{W.S.W.} \frac{1}{2} \text{ W.} \\ \text{W.S.W.} \frac{1}{2} \text{ W.} \\ \end{array} $	+38	+13	-54 38	Table very unsteady, heavy swell.
June 2.	-26 25 -27 12		Direct. N. S. N.S. Direct.	$ \begin{array}{rrrr} -60 & 33 \\ -59 & 50 \\ -60 & 05 \\ -60 & 10 \\ -59 & 48 \end{array} $	N.w. by w. N.w. by w. N.w. by w. N.w. by w. w. by s.	+80	+13	-58 36	Table very unsteady, heavy swell.
5.			N. S. N.S. Direct.	$ \begin{array}{r rrr} -39 & 48 \\ -59 & 18 \\ -59 & 48 \\ -59 & 58 \\ -59 & 43 \end{array} $	w. by s. w. by s. w. by s. w. by s.	$\left ightharpoonup +46$	+13	-58 44	Table unsteady, fresh breeze.
6.			N. S. N.S. Direct.	$ \begin{array}{c cccc} -59 & 53 \\ -60 & 18 \\ -59 & 48 \\ -60 & 33 \end{array} $	W. W. W. W. N. W.	$\left \right> + 51$	+13	-58 52	Table very unsteady, fresh breeze.
7			N. S. N.S. Direct.	$ \begin{vmatrix} -60 & 25 \\ -60 & 23 \\ -60 & 23 \\ -59 & 58 \end{vmatrix} $	W.N.W. W.N.W. W.N.W. W. 1/2 N.	+72	+13	-59 01	Table very unsteady, fresh breeze,
	_28 57	37 52	N. S. N.S. Direct.	$ \begin{array}{r rrrr} -59 & 56 \\ -60 & 28 \\ -59 & 50 \\ -60 & 38 \end{array} $	$\begin{array}{c} W \cdot \frac{1}{2} N \cdot \\ W \cdot \frac{1}{2} N \cdot \\ W \cdot \frac{1}{2} N \cdot \\ W \cdot \frac{1}{2} N \cdot \\ \end{array}$	$\left \right\rangle + 56$	+13	-58 54	Table very unsteady.
12	30 33	33 19	N. S. N.S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	W. W. W. W.N.W.	$\left \right> + 51$	+13	-59 08	Table steady, nearly a calm.
13	31 06	31 34	N. S. N.S. Direct.		w.n.w. w.n.w. w. by s. ½ s		+13	-57 19	Table unsteady.
14	33 01	29 36	N. S. N.S. Direct.			. \ \ \ + 4%	+13	-57 28	Table steady, nearly a calm.
15	34 3	27 04	N. S. N.S. Direct.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{array}{c} W \cdot \\ W \cdot \\ W \cdot \frac{1}{2} N \cdot \end{array}$	+51	+13	-57 34	Table unsteady, fresh breeze.
			N. S. N.S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$W. \frac{1}{2} N.$	+56	+13	-57 06	Table very unsteady, long heavy swell.

						Correc	tions.			
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Correcte	d Inclination.	Remarks.
1835.	0 /			0 /		,			, , ,	
June 16.	$-35^{\circ} 46^{\circ}$	23° 35	Direct. N. S.	$ \begin{vmatrix} -57 & 38 \\ -57 & 23 \\ -57 & 15 \end{vmatrix} $	w. by n. w. by n. w. by n.	$\left.\right\}$ + 63		_56 O		Table steady, fresh breeze.
17.	—35 36	21 40	N.S. Direct. N.	$ \begin{array}{r rrr} -57 & 20 \\ -56 & 48 \\ -56 & 43 \end{array} $	w. by n. w. by n. w. by n.	J]	. 10			
18.	-35 07	20 46	S. N.S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	w. by n. w. by n. w. by s.	$\left \begin{array}{c} +72 \\ \end{array} \right $	+13	-55 1	8	Table steady.
		30 10	N. S. N.S.	$ \begin{array}{r rrrr} -55 & 45 \\ -56 & 08 \\ -56 & 18 \end{array} $	w. by s. w. by s. w. by s.	+46	+13	+55 0	8	Table steady.
23.	-34 12 $-33 56$		Direct. N.S.	$ \begin{array}{r rrr} -54 & 17 \\ -53 & 45 \\ -54 & 12 \end{array} $	Observed on shore.	}	+24	-53 3	7 —53 37	Observed in the dockyard at Simon's Bay.
30.		ο.	Direct. N. S.		Observed on shore.	}	+13	-53 3	2	Monthly mean dip by Robinson's needles
July 2.	vatory	ic Obser- Cape of Hope.	N.S. Direct. N. S.		Observed on shore.	}	+13	-53 3	0 $\left53 \ 34 \right.$	A 1 53 24 A 2 53 24 Mean 53 24
June 23.	-34 12	18 26	N.S. Direct. N.S.	$\begin{vmatrix} -53 & 44 \\ -53 & 59 \\ -53 & 46 \end{vmatrix}$	s. s.	+ 09	+24	-53 2	0	
			Direct. N.S. Direct.	$\begin{vmatrix} -53 & 50 \\ -53 & 17 \\ -54 & 25 \end{vmatrix}$	S.S.W. S.S.W. S.W.	$\begin{vmatrix} 1 \\ 1 \end{vmatrix} + 14$		-52 5		
		pe.	N.S. Direct. N.S.	$ \begin{array}{r rrr} -53 & 54 \\ -55 & 04 \\ -54 & 46 \end{array} $	S.W. W.S.W. W.S.W.	$\begin{vmatrix} 1 \\ +26 \\ +41 \end{vmatrix}$		-53 2 $-53 5$	1	
		он п	Direct. N.S.	-55 18 -55 01	w. w.	$\left \right + 51$	+24	-53 5	4	
		's Bay, Cape of Good Hope.	Direct. N.S.	-55 34 $-54 49$	W.N.W. W.N.W.	$\left \right + 72$		-53 3	66	
ľ		ape c	Direct. N.S.	$ \begin{array}{r rrr} -55 & 30 \\ -55 & 10 \\ -55 & 07 \end{array} $	N.W.	$\left \right\} + 88$	1	-53 %		
		ay, C	Direct. N.S. Direct.	$ \begin{array}{r rrrr} -53 & 07 \\ -54 & 52 \\ -54 & 36 \end{array} $		$\left \right\} + 71$		-53 2	>-53 28	To obtain corrections for the ship's
		or's E	N.S. Direct.	$ \begin{array}{r rrr} & -54 & 14 \\ & -55 & 10 \end{array} $		$\left \right +75$		-52 4		attraction.
		Simo	N.S. Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.N.E.	\		-53 1	į	
		or in	N.S. Direct.	-54 46 -55 34	N.E.	$\left \right + 87$		-53 1	1	
		At anchor in Sinon	N.S. Direct.	$ \begin{array}{r rrr} -54 & 59 \\ -55 & 22 \end{array} $	E.N.E.	$\left \right +72$		-53 4 -53 5		
		At	N.S. Direct.	-54 58 $-55 05$	E.	$\begin{vmatrix} +51 \\ +41 \end{vmatrix}$		-53 4	į.	
			N.S. Direct.	$\begin{vmatrix} -54 & 31 \\ -54 & 24 \end{vmatrix}$		$\left \right + 26$	1	-53 8	l	
			N.S. Direct.	$\begin{bmatrix} -54 & 07 \\ -54 & 39 \\ 52 & 50 \end{bmatrix}$	S.S.E.	$\left \right + 14$				
			N.S.	-53 50	S.S.E.	J			_	

Observations of the Magnetic Force made on board Her Majesty's hired Bark "Pagoda," from the 10th of January 1845 to the 20th of June 1845, with Needle A. of C. 9. one hour after Noon.

Observer, Lieut. T. E. L. MOORE, R.N.

1845. Jan. 10. -3\$\frac{4}{4}\$ 6 17 46 Def. N. 48 17 19 15 10 10 10 10 10 10 10	÷ 50
Jan. 10 34 46 17 46 Def. N. 48 19 64 w. by N. 0.988008 - 000 0.980 Def. S. 49 15 64 w. by N. 0.985008 - 000 0.980 Def. N. 46 11 64 w. by N. 0.988008 - 001 0.979 Def. N. 46 11 64 w. by N. 0.988008 - 001 0.979 Def. N. 46 11 64 w. by N. 0.986008 - 001 0.993 Def. N. 46 11 64 w. by N. 0.960 + -002 - 001 0.991 Def. N. 49 22 68 N.w. by w. 0.960 + -002 - 001 0.994 Def. N. 49 22 68 N.w. by w. 0.973 + -002 - 001 0.997 Mag. N. 47 00 66 N.w. by w. 0.966 + -002 - 001 0.997 Mag. N. 47 00 66 N.w. by w. 0.966 + -002 - 001 0.997 Mag. N. 47 00 66 N.w. by w. 0.928 + -002 + -001 0.995 wt. 1 gr. 19 56 66 N.w. by w. 0.928 + -002 + -001 0.995 tw. 2 grs. 42 14 66 N.w. by w. 0.9928 + -002 + -001 0.993 Def. N. 50 42 78 w. ½ s. 0.990016001 0.933 Def. N. 50 42 78 w. ½ s. 0.994016001 0.933 Mag. N. 48 59 72 s.w. ½ s. 0.995016001 0.933 Mag. N. 48 71 67 78 w. ½ s. 0.995016001 0.933 Mag. N. 48 89 72 s.w. ½ s. 0.995016001 0.933 Mag. N. 48 89 72 s.w. ½ s. 0.995016001 0.933 Mag. N. 48 89 72 s.w. ½ s. 0.995033001 0.937 Mag. N. 48 89 72 s.w. ½ s. 0.952033001 0.937 Mag. N. 48 89 72 s.w. ½ s. 0.966033001 0.937 Mag. N. 48 89 72 s.w. ½ s. 0.966033001 0.937 Mag. N. 47 13 72 s.w. ½ s. 0.966033001 0.932 wt. 1 gr. 19 17 72 s.w. ½ s. 0.966033001 0.932 wt. 1 gr. 30 42 76 s.w. ½ s. 0.966033001 0.936 Def. N. S. 66 86 72 s.w. ½ s. 0.966033001 0.997 Mag. N. 47 18 64 s.by w. ½ w. 1.019033001 0.997 Mag. N. 48 87 70 s.w.by w. w. 1.019033001 0.996 Mag. N. 46 87 70 s.w.by w. w. 1.098024001 0.996 Mag. N. 46 87 70 s.w.by w. w. 1.098024001 0.996 Mag. N. 46 87 70 s.w.by w. w. 1.098024001 0.996 Mag. N. 46 42 45 s.w. by w. w. 1.018033 - 000 0.993 Def. N. S. 66 22 68 s.by w. ½ w. 1.006033 - 001 0.997 Mag. N. 46 49 64 s.by w. ½ w. 1.099024001 0.996 Mag. N. 46 47 58 s.w.by w. w. 1.006032 + -001 0.996 Mag. N. 44 54 48 s.w.by w. w. 1.006032 + -001 0.996 Mag. N. 44 54 48 s.w.by w. w	Remarks.
Def. S. 49 15 64 w. by N. 0.975 -008 -000 0.967 0.967 0.968 0.968 -001 0.977 0.998 0.908 0.909 0.993	
Def. N. S. 67 36 64 w. by n. 0.988 -008 -001 0.979 0.910 0.979 0.910	
Def. N. 46 11 64 w. by n. 1-001 008 -000 0-993 Def. S. 45 42 64 w. by n. 1-014 008 0-001 0-961 Def. S. 49 22 68 n.w. by w. 0-960 +-002 001 0-961 Def. S. 68 57 68 n.w. by w. 0-960 +-002 001 0-961 Def. S. 68 57 68 n.w. by w. 0-960 +-002 001 0-961 Def. S. Mag. N. 47 00 66 n.w. by w. 0-960 +-002 001 0-967 wt. 1 gr. 19 56 66 n.w. by w. 0-960 +-002 001 0-967 wt. 2 grs. 42 14 66 n.w. by w. 0-962 +-001 0-967 wt. 2 grs. 42 14 66 n.w. by w. 0-978 +-002 +-001 0-967 wt. 2 grs. 42 14 66 n.w. by w. 0-978 +-002 +-001 0-967 wt. 2 grs. 42 14 66 n.w. by w. 0-978 +-002 +-001 0-967 wt. 2 grs. 42 16 66 n.w. by w. 0-978 +-002 +-001 0-967 wt. 2 grs. 42 16 66 n.w. by w. 0-978 +-002 +-001 0-967 wt. 2 grs. 42 16 66 n.w. by w. 0-978 +-002 +-001 0-967 wt. 2 grs. 42 16 66 n.w. by w. 0-978 +-002 +-001 0-967 wt. 2 grs. 48 03 78 w. \frac{1}{2} s. 0-950 016 001 0-913 wt. 2 grs. 48 03 78 w. \frac{1}{2} s. 0-950 016 001 0-913 wt. 2 grs. 47 16 78 w. \frac{1}{2} s. 0-952 016 001 0-913 wt. 2 grs. 46 58 72 s. w. \frac{1}{2} s. 0-952 033 001 0-937 wt. 1 gr. 19 17 72 s. w. \frac{1}{2} s. 0-956 033 001 0-937 wt. 1 gr. 19 17 72 s. w. \frac{1}{2} s. 0-956 033 001 0-936 031 0-920 wt. 1 gr. 19 17 72 s. w. \frac{1}{2} s. 0-956 033 001 0-936 031 0-93	
1135 09 15 09 Def. N. 49 23 68 N.w. by w. 0.956 +002 -001 0.961 Def. N. 49 23 68 N.w. by w. 0.973 +002 -001 0.974 Def. N. 68 57 68 N.w. by w. 0.956 +002 -001 0.974 Def. N. 68 57 68 N.w. by w. 0.956 +002 -001 0.967 Def. N. 47 00 66 N.w. by w. 0.956 +002 -001 0.967 Def. N. 65 00 N.w. by w. 0.966 +002 -001 0.967 Def. N. 65 00 N.w. by w. 0.966 +002 -001 0.967 Def. N. 65 00 N.w. by w. 0.966 +002 -001 0.967 Def. N. Def. N. 65 00 N.w. by w. 0.966 +002 -001 0.967 Def. N. Def. N. 65 00 N.w. by w. 0.966 +002 -001 0.967 Def. N.	sh breezes, a
1135 09 15 09 Def. N. 49 23 68 N.w. by w. 0.976 +-002001 0.961 Def. S. 49 22 68 N.w. by w. 0.973 +-002001 0.974 Def. S. 68 57 68 N.w. by w. 0.956 +-002001 0.974 Mag. N. 46 54 66 N.w. by w. 0.966 +-002001 0.967 wt. 1 gr. 19 56 66 N.w. by w. 0.966 +-002001 0.967 wt. 2 grs. 42 14 66 N.w. by w. 0.966 +-002001 0.933 Def. N. 69 27 78 Mag. N. 49 55 78 Mag. N. 49 55 78 Mag. N. 49 55 78 Mag. N. 48 59 72 Mag. N. 48 59 72 Mag. S. 47 16 78 Mag. N. 48 59 72 Mag. N. 46 58 72 Mag. N. 46 58 72 Mag. N. 47 13 72 Mag. N. 48 59 72 Mag. N. 49 55 78 Mag. N. 48 59 72 Mag. N. 40 55 78 Mag. N. 40 55 70 Mag. N. 4	ead swell.
Def. N.S. 49 22 68 N.w. by w. 0-973 +-002 001 0-974 0-976 Nag. N. 47 00 66 N.w. by w. 0-966 +-002 001 0-970 0-970 Nag. S. 46 54 66 N.w. by w. 0-966 +-002 001 0-970 0-970 N.w. by w. 0-966 +-002 001 0-970 0-970 N.w. by w. 0-966 +-002 001 0-970 0-970 N.w. by w. 0-978 +-002 001 0-970 0-970 N.w. by w. 0-978 +-002 001 0-928* 0-981 0-9	
Def. N.S. 68 57 68 N.w. by w. 0-966 +-002 001 0-970 N.w. by w. 0-981 N.w. by w. 0-982 N.w. by w. 0-983 N.w. by w. 0-982 N.w. by w. 0-983 N.w. by w. 0-985 N.w. by	
Mag. N. 47 00 66 N.w. by w. 0.969 +002 -001 0.970 0.968 december 1.00 0.910 0.925* wt. 1 gr. y. 156 66 N.w. by w. 0.978 +002 +001 0.925* v. 2 grs. 42 46 66 N.w. by w. 0.978 +002 +001 0.925* v. 2 grs. 42 46 66 N.w. by w. 0.978 +002 +001 0.931 0.933 0.929 N.w. by w. 0.929 +001 0.918 0.933	
1235 17	
1235 17	ttle motion.
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1235 17 14 00 Def. N. 49 55 78 W. \frac{1}{2} s. 0.950 -0.16 -0.01 0.933 0.929 0.938 0.929 0.965 0.916 -0.01 0.912 0.933 0.929 0.938 0.930 -0.16 0.916 0.915 0.933 0.929 0.938 0.930 -0.016 0.935 0.935 0.930 0.938 0.930 0.938 0.930 0.938 0.930 0.938 0.930 0.938 0.930 0.938 0.930 0.938 0.930 0.938 0.930 0.938 0.930 0.938 0.930 0.938 0.930 0.938 0.930 0.938 0.930 0.938 0.930	
1335 24 13 23 Def. S. 50 42 78 W. \frac{1}{2} s. 0.924 -0.06 -0.001 0.912 0.923 0.916 -0.001 0.912 0.923 0.916 -0.001 0.935 0.938 0.930 -0.016 -0.001 0.935 0.938 0.930 -0.016 -0.001 0.935 0.938 0.930 -0.016 -0.001 0.935 0.938 0.930 -0.016 -0.001 0.935 0.938 0.938 0.938 0.938 -0.001 0.935 0.938	
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Mag. N.s. 68 30 72 s.w. \frac{1}{2} s. 0.965 -0.033 -0.001 0.927 0.932 s.w. \frac{1}{2} s. 0.966 -0.033 -0.001 0.927 0.932 s.w. \frac{1}{2} s. 0.966 -0.033 -0.001 0.927 0.932 s.w. \frac{1}{2} s. 0.966 -0.033 -0.001 0.920 s.w. \frac{1}{2} s. 0.968 -0.033 -0.001 0.920 s.w. \frac{1}{2} s. 0.968 -0.033 -0.001 0.920 s.w. \frac{1}{2} s. 0.968 -0.033 -0.001 0.920 s.w. \frac{1}{2} s.w. \frac{1}{2} s. 0.968 -0.033 -0.001 0.920 s.w. \frac{1}{2} s.w. \frac{1}{2} s. 0.968 -0.033 -0.001 0.920 s.w. \frac{1}{2} s.w. \frac{1}{2} s. 0.968 -0.033 -0.001 0.920 s.w. \frac{1}{2} s.w. \frac{1}{2} s.w. \frac{1}{2} s.w. \frac{1}{2} s. 0.968 -0.033 -0.01 0.920 s.w. \frac{1}{2} s.w.	Taring Control
Mag. N. 47 13 72 s.w. \frac{1}{2} s. 0.961 -0.033 -0.01 0.927 -0.032 -0.033 -0.01 0.927 -0.033 -0.01 0.927 -0.033 -0.01 0.920* -0.024 -0.01 0.920* -0.024	
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15. -38 42 14 27 $\begin{array}{ c c c c c c c c c c c c c c c c c c c$	
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	le unsteady, a
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Mag. S. 43 42 s.w.byw. $\frac{1}{2}$ w. 1·112 $-\cdot 024$ $+\cdot 001$ 1·089	
2451 44 9 36 Mag. N. 44 15 49 s.w. by w. 1·128 -·024 +·001 1·105	
wt. 1 gr. 17 12 50 s.w.bvw. w. 1.063 024 001 1.038* 1.09 tables	mie sieauy.
wt 9 crs 35 90 50 s w by w 1 1 1 2 9 1004 1001 1 107 P.M. A 1	. A head swell, uch motion.

^{*} Omitted in mean.

Ì					÷			Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.	Tempera- ture.	Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected Intensity.	Remarks.
1845.	0 /	0 /			. 0						
Jan. 25.	$-53^{\circ} 21$	7 32	Def. N.	43 49		s.w.byw. $\frac{1}{2}$ w.					
			Def. S. Def. N.S.	43 59 61 56	41 41	s.w.byw. 1 w. s.w.byw. 1 w.			+.006	1.129	Table steady; pass-
			Mag. N.	42 39		s.w.by $w.\frac{1}{2}w$.			+ 000		ing through streams of ice.
,			Mag. S.	42 33		s.w.byw. $\frac{1}{2}$ w.			+.002		streams of ice.
26.	-5402	6 02	Def. N.	43 43	42		1.148		+.001		
			Def. S.	44 14	42	w. by N.	1.145		+.001	1.134	
			Def. N.S.	62 09	42		1.142		+.006		
	·		Mag. N.	43 00	40	w. by n.	1.142	1	+.002		Very steady, small pieces of loose ice
			Mag. S.	42 44	40	w. by N.	1.164	1	+.002		about the ship.
			wt. 1 gr. wt. 2 grs.	16 40 34 23	40		1·096 1·164	1	+.002	,	
27.	-55 18	5 55	Def. N.	42 50	39	S.S.W. $\frac{1}{2}$ W.			+.001		Ship pitching
31.			Def. N.	39 38	37		1.324		+.002		heavily, fresh
			Def. S.	40 08	37	S.S.E.	1.320	1	+.002	1.280	breezes.
			Def. N.S.	57 04	37	S.S.E.	1.331	042	+.008		Table steady, heavy
			Mag. N.	39 45	37	S.S.E.	1.310	1			snow, passing various icebergs.
	00.00		Mag. S.	39 30	37	S.S.E.	1.349	1	+.003	1	
Feb. 1.	-62 06	12 52	Def. N.	38 10	37	s.e. by s.	1.398		+.002		Much motion, table
2.	-61 56	16 26	Def. S. Def. N.	38 58 39 17	37 37	s.E. by s.	1·376 1·341		$ +.002 \\ +.002$		unsteady.
2.	-01 30	10 30	Def. N.	39 21	36	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	1.357	1	+.002		-
			Def. N.S.	56 28	36	S.E. ½ E.	1.358				Heavy snow, a head
			Mag. N.	39 21	36	S.E. $\frac{1}{2}$ E.	1.339				sea, ship pitching violently.
		1.	Mag. S.	39 08	35	S.E. $\frac{1}{2}$ E.	1.372	036	+.003		110101111
4.	-63 00	20 40	Def. N.	38 17	39	$S_{\bullet} \frac{1}{2} E_{\bullet}$	1.391	051	1		
			Def. S.	38 35	39	S. $\frac{1}{2}$ E.	1.395	1			
			Def. N.S.	56 04	39	S. 1/2 E.	1.406	1	+.008		Water very clear
			Mag. N.	38 17 38 35	39	S. $\frac{1}{2}$ E.	1.406 1.405		$ +.002 \\ +.002$		Water very clear from ice, a little
·			Mag. S. wt. 1 gr.	13 26	39	S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E.	1.353	1 .		1.300*	motion. Vibration great.
7		1.	wt. 2 grs.	27 58	39	S. ½ E.	1.402				
5.	-63 19	21 48	Def. N.	38 36	37	S.S.E.	1.376	1 -			
l			Def. S.	38 24	37	S.S.E.	1.405				
			Def. N.S.	55 38		S.S.E.	1.397	1	-] ".
ľ			Mag. N.	38 27	36	S.S.E.	1.396	1 -	1		A heavy swell from S.E., light breezes,
l			Mag. S.	38 38 13 51	36	S.S.E.	1·407 1·313	1 -		1.264*	table steady.
l ·		1.	wt. 1 gr. wt. 2 grs.	26 57	34	S.S.E.	1.450	1 -	1		
6	-64 25	5 24 18	Def. N.	37 17		S.S.E. 1/2 E.	1.447		+.001		
1	1		Def. S.	37 48		S.S.E. $\frac{1}{2}$ E.		-045			8 Water perfectly
1			Def. N.S.	54 51	39	S,S,E, $\frac{1}{2}$ E.	1.436	-045	+.008	1.399	smooth, very steady.
7	-65 39	9 28 48	Def. N.	36 34	h	s. by E. $\frac{1}{2}$ E.			+.001		
1			Def. S.	37 11		s. by E. $\frac{1}{2}$ E.	1.472	051		1.422	
1			Def. N.S.	54 15		s. by E. $\frac{1}{2}$ E.				1.423	O'Takla standar amatan
1		1	Mag. N.	37 00 37 20		s. by E. $\frac{1}{2}$ E. s. by E. $\frac{1}{2}$ E.	1.495	051		2 1·450 > 1·43 2 1·438	2 Table steady, water smooth, no ice in
1			Mag. S. wt. 1 gr.	13 03		S. by E. 7 E.	1.392			1.340*	sight.
1			wt. 2 grs.	26 28		S.S.E.	1.47			1.423	
8	-66 2	7 30 45	Def. N.	36 27			1.494		1	1.454	
			Def. S.	36 58	34	s.E. by E.	1.483	3 -042	+.002	1.443	
	Ī	1.	Def. N.S.	54 05			1.474				Fresh breeze, table unsteady.
1	1	1	Mag. N.	37 00		3	1.499			1.461	
1	1		Mag. S.	37 39	30	s.E. by E.	1.475	-042	+ 004	1.437	

^{*} Omitted in mean.

Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.	Tempera-	Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected Intensity.	Remarks.
1845. Feb. 9.	66° 36	36 5Ó	Def. N. Def. S. Def. N.S.	36 06 36 43 53 41	39 39 36	s.e. by e. s.e. by e.	1.514 1.508 1.505	042	+·001 +·010	1·473 1·467 1·473 \rightarrow 1·470	Light breeze, very
10.	67 11	38 51	Mag. N. Mag. S. Def. N. Def. S.	36 55 36 59 35 39 36 31	35 34 34 34	s.e. by e. s. by w. s. by w.	1.505 1.509 1.540 1.509		+·003 +·002 +·002	1.466 1.470 1.492 1.461	smooth.
11.			Def. N.S. Mag. N. Mag. S. Def. N.	52 45 36 27 37 02 36 10	34 34 34 35	s. by w. s. by w. s. by w. N.E.	1.549 1.540 1.509 1.510		+·009 +·003 +·003 +·002)	Steady, water very smooth. Sailing along a pack of ice, unsteady.
12.	-67 18	40 22	Def. N. Def. S. Def. N.S. Mag. N.	35 30 36 07 53 16 36 37	32 32 32 32	S. ½ E. S. ½ E. S. ½ E. S. ½ E.	1.548 1.533 1.520 1.529	050 050 050	+·003 +·003 +·013 +·004	1.483	Fresh breeze, table unsteady.
13.	66,55	14 16	Mag. S. Def. N. Def. S. Def. N.S.	36 03 36 00 36 37 53 29	32 34 34 33	S. ½ E. E.N.E. E.N.E.	1 (· 025 · 025 · 025	+ ·004 + ·002 + ·002 + ·011		Swell from E., table unsteady.
14. 16.	-66 24 $-64 52$		Mag. N. Mag. S. Def. N. Def. S. Def. N.	36 43 37 06 36 18 36 24 35 59	33 33 34 34 41	E.N.E. E.N.E. N.E. by N. N.E. by N. S. by E.	1.521 1.503 1.502 1.515 1.520	025 016 016	+ 004 + 004 + 002 + 002 + 001	$egin{array}{c c} 1.500 \\ 1.482 \\ 1.488 \\ 1.501 \\ 1.471 \\ \end{array}$	Table unsteady, very squally.
10.	-01 32	00 07	Def. N. Def. N.S. Mag. N. Mag. S.	36 56 53 48 37 07 37 15	41 41 40 40	s. by E. s. by E. s. by E.	1·487 1·490 1·493	050 050 050	+·003 +·003 +·001	1·438 1·448 1·446	Thick weather, a heavy swell, un- steady,
17.	-66 43	40 12	Def. N. Def. N.S. Mag. N.	36 34 37 08 53 18 36 53	36 36 38 38	s. by e. N. N. N.	1·487 1·475 1·518	018	$+002 \\ +002 \\ +010$	1·445 1·471 1·459 1·510 1·482	Calm, a heavy sea, not steady.
19. 20.	$ \begin{array}{cccc} -64 & 05 \\ -63 & 19 \end{array} $	41 09 45 52	Mag. S. Def. N. Def. N. Def. S.	37 13 36 35 36 12 37 10	37 37 45	N.	1.495 1.486 1.507	018 035 040	+ '003 + '002 + '001 + '001	1·480 1·453 1·453 1·468 1·435	Very unsteady, a swell from N.
	-63 22	45 58	Def. N.S. Def. N. Def. S. Def. N.S.	53 40 36 08 36 33 53 22		s.e. by e. ½ e. s.e. s.e.	1·497 1·511 1·507	040 046	+ .001 + .001	1.463	A heavy swell, strong breeze, with a heavy sea running.
21.	-63 36 -63 36		Def. N. Def. S. Def. N.S.	36 00 36 33 53 23 36 01	40 39 39 40	S.E. S.E.	1·519 - 1·507 - 1·513 -	046 046 046	+ · 001 + · 001 + · 001	1·474 \\ 1·462 1·476 1·473	
	00 00		Def. S. Def. N.S. Mag. N.	36 37 53 26 36 39 37 09	40 39 39 39	S.E. S.E.	1·505 - 1·511 - 1·525 -	046 046	+ ·003 + ·009 + ·001	1·473 1·470 1·474 1·482 1·457	Table unsteady, much motion.
25.	-61 34	53 49	Def. N. Def. S. Def. N.S.	35 41 36 13 53 21 36 14	42 42 40 39	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	1·537 - 1·527 - 1·515 -	-·044 -·044 -·044	+ ·001 + ·009	1·494 1·484	Fresh breeze, table steady.
				36 19	39			044	+ 003	1.516	

				· · · · · · · · · · · · · · · · · · ·			1						
		Ì	1			٤			Corre	ctions.			
		1		Method	Angle of	Tempera- ture.		Intensity.		·	Corre	Lotor	
Date.	Lat.	Lo	ng.	employed.	defiec-	はは	Ship's head.	en	Ship's	Tempe-	Inten		Remarks.
		1	1	cmployeds	tion.	Te		I I	attrac-	rature.	Invon	orty.	
									tion.				
1045		-		***************************************									
1845. Feb. 26.	_6i 2	6 5%	29	Def. N.	35 11	4 0	S.E. 1/2 E.	1.566	044	+.001	1.502	,	-
reb. 20.	-01 2	9 31	99	Def. S.	35 46	40		1.552		+.001			
		1					S.E. ½ E.						
	Cia	d		Def. N.S.	52 55	40	S.E. 1/2 E.	1.541	-044	+.009			
	-61 2	2 57	41	Def. N.	35 07	40	S.E.	1.571	046	+.001			
				Def. S.	35 57	40	S.E.	1.540	046	+.001		1.506	Fresh breezes, table
				Def. N.S.	52 58	40	S.E.	1.540	046	+.009			steady.
ii Q				Mag. N.	36 24	39	S.E.	1.543	046	+.003			
1				Mag. S.	36 22	38	S.E.	1.553	046	+.003	1.210		
				wt. 1 gr.	12 41	38	S.E.	1.432		003	1.383*		
	_	1		wt. 2 grs.	25 29	38	S.E.	1.528	-046	003			
27.	-61 1	0 64	20	Def. N.	34 35	39	S.S.E. 1 E.	1.602	 · 04 8	+.002	1.556	1.560	Von ungtoods
				Def. S.	34 49	39	S.S.E. 1/2 E.	1.610	048	+.002	1.564	T-200	Very unsteady.
28.	-614	9 71	30	Def. N.	33 47	38	S.S.E.	1.651		+.002			
	-	1.	-	Def. S.	34 15	38	S.S.E.	1.644	•04 9	+.002			Very unsteady.
	ĺ			Def. N.S.	51 17	37	S.S.E.	1.635	 · 049	+.010			
		İ		Mag. N.	34 35	37	S.S.E.	1.680		+.003	1.634	1.00-	
	. "			Mag. S.	35 15	35	S.S.E.	1.637	049	+.003	1.591	>1.002	Table steady.
	-614	9 71	32	Def. N.	33 26	35	S.S.E.	1.675	•049	+.002	1.628		
		1		Def. S.	34 27	35	S.S.E.	1.632	049	+.002		,	
Ĭ.				Def. N.S.	51 05	35	S.S.E.	1.646	049	+.011			
Mar. 1.	-621	0 72	25	Def. N.	33 14	46	s.e. by s.	1.687	047	+.002	1.642		
		1		Def. S.	33 31	46	s.e. by s.	1.692	047	+.002	1.647		
				Def. N.S.	50 33	46	s.E. by s.	1.680	047	+.006	1.639		
				Mag. N.	34 24	46	s.e. by s.	1.695	047	+.002	1.650	1.642	Calm, table steady.
				Mag. S.	34 49	46	s.e. by s.	1.673		+.002	1.628	1 0 2 10	1.1
			-	wt. 1 gr.	10 37	46		1.706		002	1.657*		
				wt. 2 grs.	22 49	46		1.695		002	1.646	ł	
2.	-62 4	7 76	14	Def. N.	33 15	42	s.e. by E. $\frac{1}{2}$ E.			+.001	1.641	, 1	
7	0~ 1	10	11	Def. S.	33 30	42	s.e. by E. $\frac{1}{2}$ E.	1.693	041	+.001	1.653		
	1			Def. N.S.	50 26	42	s.e. by $\mathbf{E} \cdot \frac{1}{2} \mathbf{E}$.	1.686	041	+.008	1.653		
				Mag. N.	34 15	42	s.e. by $\mathbf{E} \cdot \frac{1}{2} \mathbf{E}$.	1.706	041	+.003	1.668		
				Mag. S.	34 40	42	s.e. by $\mathbf{E} \cdot \frac{1}{2} \mathbf{E}$.	1.685	041	+.003			
	l			wt. 1 gr.	11 02	42	s.e. by $E \cdot \frac{1}{2} E$.	1.643	041	003	1.599*	≻1•653	Steady breeze, table
				wt. 2 grs.	22 31		s.E. by E. ½ E.	1.716	041	003	1.679	! •	steady.
	-62 4	0 76	16	Def. N.	32 46	42	S.E. Dy E. 7 E.	1.717	056	+.002	1.662	1	
	-02 4	3 10	10	Def. N.	33 30	42	s.	1.602	056	+.002	1.630		
	1			Def. N.S.	50 24	42	s. s.		056	+.008	1.640		
3.	-64 2	0 70	20	Def. N.S.	32 32	34	s. by w. $\frac{1}{2}$ w.			+.003	1.601	, 1	
3.	-04 2	V 79	99	Def. N. Def. S.	32 58	32	s. by $w \cdot \frac{1}{2} w$. s. by $w \cdot \frac{1}{2} w$.	1.700				1.670	77
	1				32 38 49 56	31	s. by $w.\frac{1}{2}w$. s. by $w.\frac{1}{2}w$.	1.717	-054	+ 014	1.677	71-078	Fresh breeze, un- steady, thick, with
-	61 4	0 0-	0.7	Def. N.S.	-	1		1.70=	•040	+ 0114	1.740		squalls of snow.
5.	-61 4	85	07	Def. N.	31 35	36	S.E. ½ E.		-·049 -·049	1.000	1.796	1.790	Tingtondu
				Def. S.	32 09	37	S.E. 1 E.	1.783	1	+.002	1.705	1.730	Unsteady; aurora visible.
	Ca	0 00	00	Def. N.S.	49 35 31 34	37	S.E. ½ E.	1.742		+.012	1.700	į	1
6.	-60 4	88 P	33	Def. N.	1	39	S.E.	1.796		+.002	1.747	-	
				Def. S.	32 27	39	S.E.	1.762	051	+.002	1.713	(. <u></u>	
	ľ			Def. N.S.	49 32	38	S.E.		-051	+.011	1.706	747ع	Very unsteady, with thick weather.
				Mag. N.	32 38	37	S.E.	1.833		+.004	1.780	İ	
50	C-			Mag. S.	33 01	37	S.E.	1.830	1	+.004	1.783		
7.	-61 2	3 91	15	Def. N.	31 46	41	s.s.w.	1.783		+.002	1.732)	
				Def. S.	32 14	42	s.s.w.	1.779	053		1.728		1
				Def. N.S.	49 00	42	s.s.w.	1.785		+.009		≻1•749	Unsteady.
	1	1		Mag. N.	32 54	42	s.s.w.	1.811		+.003			:
i				Mag. S.	32 57	42	s.s.w.	1.834	-053	+.003	1.784)	
i	1				!	1	1		1		1		<u> Lamente de la companya del companya del companya de la companya </u>

^{*} Omitted in mean.

Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.	Tempera- ture.	Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected Intensity.	Remarks,
1845. Mar. 8.	-61 07	92 10	Def. N. Def. S.	31 13 32 04	41 40	E.S.E. E.S.E.	1.824 1.790	046	+·002 +·002	1.746 >1.758	Unsteady, with
9.	-60 30	92 34	Def. N.S. Def. N. Def. S.	49 04 31 19 32 09	38 40 41	E.S.E. s.E. by E. s.E. by E.	1.782 1.817 1.784	046 048 048	+·011 +·002 +·002	1.771	very unsteady.
	00.00	20.00	Def. N.S.	49 08	41	s.E. by E.	1.780	048	+.010	1.742	
10.	-60 03		Def. N. Def. S. Def. N.	31 08 31 56 29 54	39 38 35	E.S.E. E.S.E. E. ¹ / ₂ N.	1.832 1.796 1.919	046 046 041	+·002 +·002	1.752	Aurora visible, table steady.
11.	-59 45	99 50	Def. N. Def. N.S.	30 31 48 58	34 34	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	1.908 1.788	 ·041	+.002 +.002 +.013	1.869	A heavy sea, very
			Mag. N. Mag. S.	32 21 32 23	34 34	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	1.855 1.888	-·041 -·041	$+.004 \\ +.004$	1.818 1.851	unsteady.
	-57 46		Def. N. Def. S.	30 34 31 28	46 46	E.N.E.	1.870 1.831	-·039 -·039	+.001	$\begin{vmatrix} 1.832 \\ 1.793 \end{vmatrix}$ 1.813	Very unsteady.
14.	—56 56	101 36	Def. N. Def. S. Def. N.S.	$\begin{vmatrix} 30 & 31 \\ 31 & 20 \\ 48 & 35 \end{vmatrix}$	40 41 41	E. by s. E. by s. E. by s.	1.876 1.842 1.816	047 047 047	+·002 +·002 +·010	1.797 >1.802	A.M. Aurora visible, unsteady.
15.	-55 40	103 18	Def. N. Def. S.	30 30 31 10	41	E.N.E. E.N.E.	1.876 1.854	039	+·002 +·002	1.839	Squally with snow, unsteady.
16.	-54 3 8	106 15	Def. N.S.	48 34 30 03	41 39	E.N.E. E.	1.817 1.909	045		1.866 7	Heavy squalls, un-
17	-54 10	100 15	Def. S. Def. N.S. Def. N.	31 18 48 34 29 59	38 38 39	E. E. by s.	1.844 1.817 1.913	045 045 047	+.002 +.012 +.002	1.784	steady, snow.
14.	-9 1 10	100 10	Def. S. Def. N.S.	31 05 48 34	40 40	E. by s. E. by s.	1.860 1.817	-·047 -·047	+.002	1.815 >1.821	A strong gale, very unsteady.
18.	—53 00	110 30	Def. N. Def. S.	30 28 31 14	44 44	N.E.	1.878 1.849	-·036 -·036	$+.002 \\ +.002$	1.844 5 1.815	
		-	Def. N.S. Mag. N. Mag. S.	48 30 31 55 32 48	43 43 43	N.E. N.E.	1.822 1.889 1.850	036 036 036	+·009 +·003 +·003	1.856	Unsteady, a heavy swell from west- ward. strong breeze.
20.	-48 57	112 56	Def. N. Def. S.	30 52 31 26	47 48	N.E. \frac{1}{2} N. N.E. \frac{1}{2} N.	1.849 1.834	-·035 -·035	$+001 \\ +001$	1.815 7	
			Def. N.S. Mag. N.	48 22 32 20	48 49	N.E. $\frac{1}{2}$ N. N.E. $\frac{1}{2}$ N.	1.831 1.857	-·035 -·035	+·006 +·002	1.802	Fresh breeze, very
			Mag. S. wt. 1 gr.	32 58 9 59 20 01	49 50 50	N.E. $\frac{1}{2}$ N. N.E. $\frac{1}{2}$ N.	1.835 1.813	-·035 -·035		1.776*	unsteady.
22.	-47 21	115 15	wt. 2 grs. wt. 3 grs. Def. N.	31 32 30 38	50 50	N.E. $\frac{1}{2}$ N. N.E. $\frac{1}{2}$ N. N.W. $\frac{1}{2}$ N.	1.920 1.859 1.866	035 035 029	002 002 +-001	1.822	
			Def. S. Def. N.S.	30 34 48 29	50 50	N.W. $\frac{1}{2}$ N. N.W. $\frac{1}{2}$ N.	1.897 1.821	-·029 -·029	+.001 + .005	1.869 1.797 1.842	Light breeze, table
24	45.00	116 50	Mag. N. Mag. S.	32 07 32 26 31 01	50 50	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.876	-·029 -·029	+·002 +·002	1.858	steady, thick fog.
24. 25.		116 50 116 49	Def. S.	31 01 31 21 31 06	49 50 55	N. by E. N. by E. N. \frac{1}{2} E.	1.840 1.838 1.833	-·020 -·020 -·020	, ,	1 11821	A heavy swell from westward, un- steady.
		-5	Def. S. Def. N.S.	31 49 48 57	55 55	$N_{\bullet} \frac{1}{2} E_{\bullet}$ $N_{\bullet} \frac{1}{2} E_{\bullet}$	1.807 1.789	020 020	+.002	1·787 1·771	
-			Mag. N. Mag. S.	32 33 33 24	55 56	N. \frac{1}{2} E. N. \frac{1}{2} E.	1.840		+.001	1.774	A heavy swell, um- steady.
			wt. 1 gr. wt. 2 grs.	10 20 20 30	56 56	N. $\frac{1}{2}$ E. N. $\frac{1}{2}$ E.	1.753 1.877	-·020 -·020	-·001	1·732* 1·856	

^{*} Omitted in mean.

	\$ 100 miles	4		Angle of	ģ		ty.	Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.	Temper ture.	Ship's head.	Intensity.	Ship's attrac- tion.	Tempe- rature.	Corrected Intensity.	Remarks.
1845.	0 00	116 42	D.C.M	31 40	56	1	1.500	020	-000	1-550	
Mar. 26.	-41 00	116 42	Def. N. Def. S.	31 40	56	n. by w.	1·790 1·821	-·020	l	$\begin{vmatrix} 1.770 \\ 1.801 \end{vmatrix}$	
1			Def. N.S.	49 41	56	n. by w.	1.736	020	+.002		A heavy westerly
			Mag. N.	33 19	56	n. by w.	1.780	020	+.001		swell.
			Mag. S.	33 46	56	N. by w.	1.759	020	+.001	1.740	
27.	-3840	116 15	Def. N.	32 33	62	n. by E.	1.731	012		1.719	
			Def. S.	32 35	62	N. by E.	1.752	012	•		Table steady.
90	27 00	116 50	Def. N.S.	49 55	62 63	1 .	1·720 1·689	-·012 -·012		1.677	
28.	-37 00	110 57	Def. N. Def. S.	33 12 33 34	64	n. by E. n. by E. ½ E.		-012	1	1.675	
			Def. N.S.	50 42	64	N. by E. $\frac{1}{2}$ E.		-012		1.656	·
			Mag. N.	34 06	68	N. by E. $\frac{1}{2}$ E.				1.704	
			Mag. S.	34 41	68	N. by E. \frac{1}{2} E.	1.681	-012	001	1.009	Unsteady.
		1	wt. 1 gr.	11 08	68	n. by E. ½ E.				1.617*	
		l	wt. 2 grs.	22 48	68	N. by E. $\frac{1}{2}$ E.		012	+.001		
20	06.11		wt. 3 grs.	35 19	65	N. by E. $\frac{1}{2}$ E.			+.001		
29.	—36 11	116 48	Def. N. Def. S.	33 12 33 21	67	N.N.E.	1.689 1.702	012 012	-·001		Unsteady.
			Def. N.S.	50 51	68	N.N.E.	1.661	-012	003		onsteauy.
30.	—35 07	117 38	Def. N.	32 54	66	N.N.E.	1.708	012	001		
00.	00 0,		Def. S.	33 13	66	N.N.E.	1.712	-012	001		Unsteady.
			Def. N.S.	50 12	66	N.N.E.	1.701	012	002	1.687	
April 7.			Def. N.	33 11	68	1	1.690		1	1.689	,
	King G		Def. S.	33 32	68		1.690			1.689	
	Sound,		Def. N.S.	50 24	68 68		1.689 1.687	•••••	-·003	1.686	
	Austr	ana.	Mag. N. Mag. S.	$\begin{vmatrix} 34 & 30 \\ 34 & 34 \end{vmatrix}$	69	Observed				1.600	
			wt. 1 gr.	10 44	69	on shore.			+.001		On the 8th needle A. was found to have
			wt. $1\frac{1}{2}$ gr.	17 16	69		1.688		+.001	1.689	been injured, needle B. was
	V		wt. 2 grs.	22 56	69		1.688		+.001	1.689	therefore used
			wt. $2\frac{1}{2}$ grs.	28 18	69	1 }	1.688		+.001		subsequently.
			wt. 3 grs.	35 11	69	J	1.688	<u> </u>	+.001	1.689	
						Needle B	• '				
12.	25 00	117 56	Def. N.	29 23	64	h	1.711	T	•000	1.711	
12.	King G		Def. S.	35 31	64		1.657			1.657	
	Sou		Def. N.S.	50 11	64	11	1.679			1.679 >1.679	2
			Mag. N.	31 37	64	Observed	1.658		.000	1.658	
			Mag. S.	36 25		on shore.				1.653	
			wt. 1 gr.	16 13			1.693			1.693	
			wt. $1\frac{1}{2}$ gr. wt. 2 grs.	24 39 33 27	62	11	1.672 1.698			1.672 \1.688	8
23.	-35 30	114 25		30 03	66	N.W.	1.670	_··011		1.658	
£U.	-30 30	114 00	Def. S.	35 01	66	N.W.	1.687	011			Very unsteady,
			Def. N.S.	49 55	66	N.W.	1.696	011		1.683 ∫	heavy south-west swell.
25.	-32 24	111 26	Def. N.	31 07	69	N.w. by N.					1
1			Def. S.	36 26	69	N.w. by N.	1.603	011	001		
			Def. N.S.	51 30	69	n.w. by n.			004		Moderate breeze, table steady.
			Mag. N. Mag. S.	33 14 37 23	69	n.w. by n.	1.547 1.577	-·011	-·001 -·001	1 - 1	
27.	20 16	106 49	Def. N.	32 17		w.N.W	1.534	1			
~1.		3	Def. S.	37 53	72	w.n.w.	1.515	015			Very unsteady.
as sign			Def. N.S.	53 15		w.N.w.	1.501				
				L	<u> </u>			<u> </u>			<u> </u>

^{*} Omitted in mean.

						1						
				1	ا د		١.	Correc	tions.			
	_		Method	Angle of	Tempera- ture.		Intensity.			C		
Date.	Lat.	Long.	employed.	deflec-	日間	Ship's head.	l g	Ship's	Tempe-		ected asity.	Remarks.
				tion.	Te		Ħ	attrac-	rature.	Inter	isity.	
							"	tion.				4
1045												
1845.	$-2\mathring{7} \ 3\mathring{5}$	106 36	Def. N.	33 30	7 5	n. by w.	1.467	+.002	001	1.468	1	
Ap. 28.	-21 33	100 32	Def. S.		76	N. by w.				1.533		1.
-							į.	+.002	-·001		1.470	
			Def. N.S	53 30	76	n. by w.		+.002	006	1.479	>1.478	Unsteady, a heavy swell.
			Mag. N.	34 36	76	n. by w.		+.002	002	1.459	1	swen.
			Mag. S.	39 06	76	n. by w.	1.451	1	002	1.451)	
29.	-25 46	104 55	Def. N.	33 47	68	N.W.	1.450		 ·001	1.446	1.447	Very unsteady.
			Def. S.	39 02	68	N.W.	1.453	003	001	1.449	1 44/	very unsteady.
May 1.	-2358	99 06	Def. N.	34 30	68	w.	1.414	022	001	1.391)	
.			Def. S.	39 54	68	w.	1.407	022	001	1.384	1.381	Unsteady.
			Def. N.S.	55 14	68	w.	1.394	022	003	1.369	1	
2.	-24 01	97 25	Def. N.	34 32	72	$W_{\bullet} = \frac{1}{2} N_{\bullet}$	1.412		001	1.392	í	
~•	W. V.	3, 20	Def. S.	40 02	72	$W \cdot \frac{1}{2} N \cdot$	•	019	001	1.382	1.391	Unsteady.
.]		1	Def. N.S.	55 15	72	$W \cdot \frac{1}{2} N$		019	 005	1.370		l additional to
	00 EV	05 50		35 00	76	, -	,					
3.	-23 50	95 56				$W \cdot \frac{1}{2} N \cdot$	1.388		001	1.368		
			Def. S.	40 16	76	$W \cdot \frac{1}{2} N \cdot$		019	001	1.369	Ì	
			Def. N.S.	55 38	76	$W_{\cdot} \frac{1}{2} N_{\cdot}$		019	 ∙006	1.353	>1.377	Steady.
			wt. 1 gr.	19 28	76	$W_{\bullet} \frac{1}{2} N_{\bullet}$			+.001	1.401	1.011	budy.
. 1		i i	wt. $1\frac{1}{2}$ gr.	29 58	76	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.396	-019	+.001	1.378		
			wt. 2 grs.	41 30	76	$W. \frac{1}{2} N.$	1.413	019	+.001	1.395		•
4.	-24 16	93 48	Def. N.	35 21	76	w.n.w.	1.371	-010	001	1.360)	
[Def. S.	41 05	76	w.n.w.	1.350	-010	 001	1.339	1.352	Unsteady.
			Def. N.S.	55 45	76	w.n.w.		010	001	1.358		
5.	-24 02	92 07	Def. N.	35 51	73	N.W.	1.347	1 1	001	1.354	`	
•	W 1 0 N	5~ 01	Def. S.	40 37	73	N.W.		+.008	 001	1.380	1.367	Cross sea, much rolling motion.
7.	-21 44	89 38	Def. N.	36 30	73	N.W. $\frac{1}{2}$ W.	1.316		-·001	1.319	{	Tolling motion,
1.	-21 44	09 00		1			1.	,				Table unsteady.
			Def. S.	42 13	73	N.W. $\frac{1}{2}$ W.	1.298		001		1.314	Labic ansociary.
_			Def. N.S.	56 45	73	N.W. $\frac{1}{2}$ W.	1.322	+.004	005	1.321	Į	1
8.	-20 38	87 50		36 39	77	N.W. $\frac{1}{2}$ W.	1.309	+.004	001	1.312	1	ĺ
		1	Def. S.	42 49	77	N.W. $\frac{1}{2}$ W.	1.270		 ·001		>1.298	Unsteady.
			Def. N.S.	56 58	77	N.W. $\frac{1}{2}$ W.	1.312	+.004	006	1.310	J	
9.	-20 37	85 02	Def. N.	36 56	77	$W_{\bullet} = \frac{1}{2} N_{\bullet}$	1.295	-015	001	1.279)	
			Def. S.	42 49	77	$W_{\bullet} \stackrel{\overline{1}}{\underline{2}} N_{\bullet}$	1.270	015	001	1.254	>1.263	Heavy swell.
			Def. N.S.	57 46	77	$W \cdot \frac{1}{2} N \cdot$	1.276		006	1.255		
10.	-20 25	82 10	Def. N.	37 46	77	$W \cdot \frac{3}{4} N$.	1.260	012	001	1.247	,	
			Def. S.	42 48	76	$W. \frac{3}{4} N.$	1.270	012	 001	1.257	1	
			Def. N.S.	57 46	76	W. $\frac{3}{4}$ N.	1.276	012	_·006		1.948	Heavy swell.
			Mag. N.	38 04	76	4	1.256	012	-·001	1.243	(250	
1			Mag. S.	42 13	76	$W_{\bullet} \frac{3}{4} N_{\bullet}$	1 1				1	
,,	20.00	70 10		1		$W_{\bullet} \frac{3}{4} N_{\bullet}$	1.249	012	001	1.236	,	
11.	-20 36	79 10	Def. N.	39 00	78	$W \cdot \frac{3}{4} N \cdot$	1.207		001	1.194	-	
l			Def. S.	43 29	78	$W_{\bullet} \frac{3}{4} N_{\bullet}$		012		1.226	1.213	Unsteady.
1			Def. N.S.	58 28	78	$W \cdot \frac{3}{4} N \cdot$	1.247	012	-:007	1.228	1 - 220	C.I.Stoway.
			Mag. S.	42 44	78	$W \cdot \frac{3}{4} N \cdot$	1.220	012	-002	1.206	j	
12.	-2044	78 31	Def. N.	37 23	87	8.	1.275	-040	_ 002	1.233)	
1			Def. N.	37 12	87	s.s.w.	1.283	036	002	1.245	İ	
,			Def. N.	37 14	87	s.w.	1.282	032	002	1.248	ĺ	
			Def. N.	38 13	87	w.s.w.	1.241	023	002	1.216		
			Def. N.	38 28	87	W.	1.229	016	002	1.211	1	Those shows the
ł			Def. N.	38 27	87		1.230	007	002	1.221	1	These observations were made to de-
1	1				1	W.N.W.					>1.234	termine the effect
ļ		[Def. N.	37 47	86		1.258	-·001	002	1.255		of the ship's iron at sea.
1			Def. N.	38 14	84	N.N.W.	1.240	.000	002	1.238		
			Def. N.	38 11	80		1.242	+.002	001	1.243		
ļ		.	Def. N.	38 28	78	N.N.E.	1.229	.000	001	1.228		
-			Def. N.	38 17	78	N.E.	1.236	001	001	1.234		A
. [Def. N.	38 00	78	E.N.E.	1.249	 007	 ∙001	1.241		

				Angle of	ra-		×	Corre	ctions.		
Date.	Lat.	Long.	Method employed.	deflec- tion.	Tempera- ture.	Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected Intensity.	Remarks.
1845.					Â						
May 13.	-20 39	77 43	Def. N.	37 41	$ {81}$	S.E.	1.262	032	001	, - ,	
-			Def. N.	38 00	81	E.	1.249	016	001		Made to determine the effect of the
			Def. N.	37 40	81	1	1.264		001	1 11933	_him!=i=======
			Def. N.	38 24	80	1	1.232	+.002	001	1.233	A rolling motion,
			Def. N.	38 31	79	N.W.	1.228	001	001	1 1	not very steady at
16.	-20 26	70 26	Def. N. Def. N.	38 20 38 40	79 78	w. w. by n.	1·235 1·221	-·016 -·011	-·001 -·001	. 2	some points.
10.	-20 20	70 30	Def. S.	43 52	78		1.221	011	001		Unsteady.
-			Def. N.S.	59 26	78		1.214		007		
17.	-20 34	69 24	Def. N.	38 37	78	w. by N.	1.222	011	001		
			Def. S.	43 59	78		1.217	011	001	1	
			Def. N.S.	59 09	78		1.222	011	007	1.204	r
	+ .		Def. N.	38 09	79	s.w.byw. $\frac{1}{2}$ w.	1.243	030	001	1.212 (1.210	Unsteady.
			Def. S.	43 17		s.w.byw. $\frac{1}{2}$ w.		÷.030	001	1.21/	
			Def. N.S.	58 34	80	$s.w.byw.\frac{1}{2}w.$	•	030	007	1	
			Mag. N.	38 23	80	s.w.byw. $\frac{1}{2}$ w.		030	002	1 1	
10	01 11	Cm ma	Mag. S.	42 07	80	$s.w.byw.\frac{1}{2}w.$		030	002		
19.	—21 11	67 54	Def. N. Def. S.	38 57	76 76	1	1·209 1·203	-·001	$\begin{bmatrix}001 \\001 \end{bmatrix}$	1.207	
			Def. N.S.	44 17 59 54	76	I .	1.196	-·001	005	1 6	Unsteady.
			Mag. N.	38 52	76		1.211	001	 001		1
			wt. 1 gr.	22 44	76	1	1.223	001	+.001	, , , , , , , , , , , , , , , , , , ,	
			wt. $1\frac{1}{2}$ gr.	35 01	76		1.215	001	+.001		
			wt. 2 grs.	51 35	76	1	1.195	001		1.195	Steady.
20.	-21 12	67 29	Def. N.	39 02	74	w. by N.	1.205	012	001	1.192 5	
			Def. S.	44 03	77	w. by N.	1.212	012	001	1.199 >1.190	Unsteady.
			Def. N.S.	59 59	77	w. by N.	1.194		004		
21.	-21 01	66 10	Def. N.	39 03	76	w. by N.	1.204	1	001		:
			Def. S.	44 29	76	w. by N.	1.195	012	001		
			Def. N.S.	59 40	76	w. by N.	1.204		005	1 . (Unsteady.
			Mag. N.	39 14	76 76	w. by N.	1·194 1·163	-·012 -·012	-·001	1 1	
22.	-20 40	60 50	Mag. S. Def. N.	43 48 39 28	74		1.189	-012	001		
22.	20 40	02 50	Def. S.	45 01	74		1.173	-012	001	1.160	
			Def. N.S.	59 41	74		1.203	012	005		Table steady.
			Mag. N.	39 28	74		1.181	012	001	1 - 1	
27.	-20 09	57 31	Def. N.	40 07	77		1.165			1.164	
			Def. S.	45 28	77		1.153		001	1.152	
		,	Def. N.S.	60 43	77	On shore	1.167		006	1.161 >1.155	Steady.
			Mag. N.	39 55	77	ot Man	1.158		001		
	1		Mag. S.	44 14	77	1	1.138		001		
			wt. 1 gr.	23 59	80		1.163		+.001	1.164	
			wt. 1½ gr.*	33 46	80		1.255			1.256* >1.156	Steady.
90	01 50	59 05	wt. 2 grs.	54 42	80		1.147	-027	+.001		
30.	-21 50	33 25	Def. N. Def. S.	$39 \ 41 \ 44 \ 25$	81 81	s.w. by w.	•	-027	001	1.170 1.161	Unsteady.
			Def. N.S.	59 59	80	s.w. by w.		-·027			,
June 3.	-26 26	48 20	Def. N.S.	39 39	79	N.w. by w.	1.187				
oune o.	-20 20	10 20	Def. S.	45 18	78	N.w. by w.			001	1.155 1.164	Unsteady.
			Def. N.S.	60 41	78	N.w. by w.		005	006	1.157	
4.	-27 14	45 50	Def. N.	39 44	69	w.	1.179			1.160	
			Def. S.	44 39	70	w.	1.188		l .		Unsteady,
			Def. N.S.	60 38	70	w.		018	1		
							<u> </u>	1	<u> </u>		L

^{*} This observation is evidently wrong, and is omitted in the mean.

					-b		٠	Corre	ctions.		·	
Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.		Ship's head.	Intensity.	Ship's attrac-	Tempe-	Corre Inter		Remarks.
							1	tion.				
1845.	0 /			0								
June 8.	-2857	37 55	Def. N.	40 36		w.	1.147	018	Į.	1.128] -	
			Der. S.	40 11		w.	1.124	018	001	-	!	
			Def. N.S.	61 44	1	w.	1.131	-·018	-:005		1111م	Steady.
			Mag. N. Mag. S.	40 27 44 33	1	w.	1.132 1.121	-·018	-·001	1	į.	
11.	-30 27	33 41	Def. N.	41 32	1	w. w.n.w.	1.114	008	001	} · -) 1•105	Very unsteady.
13.			Def. N.	41 58	1	w. by s. $\frac{1}{2}$ s.		-024	001		. 1;100 1	discounty.
10.	-51 00	51 20	Def. S.	47 30		w. by s. $\frac{1}{2}$ s.	1.079	-024		1.054	>1.063	
			Def. N.S.	61 41		w. by s. $\frac{1}{2}$ s.		1		1.101*	1	1
17.	-35 40	21 40	Def. N.	43 19		w. by N.	1.053	013		1.040	Í	
- • •	-,	,	Def. N.S.	64 49	62	w. by N.	1.038	013		1.025	1.033	Unsteady.
23.	Simon's	Bay,	Def. N.	43 29		s.	1.047	040	001	1.006	ĺ	
	Cape of		Def. N.	43 4		S.E.	1.036	-032	.000	1.004	1	
	Hope.		Def. N.	44 14	- 1 - •	E.	1.117	-016	•000	1.001		
	-		Def. N.	44 3		N.E.	1.004	001		1.003	1.001	
			Def. N.	44 40		N.	1.001	+.002		1.003	ſ. 00.	
			Def. N.	44 40	, -	N.W.	1.997	001		0.996	1	
			Def. N.	44 20	,	w.	1.013	-016		0.996	1	
	a. 1	T	Def. N.	43 50		s.w.	1.032	032	001	1 1	Į	
24.			Def. N.	44 3		FaceEast,	1.004			1.003	1.00	
	at the l	Dock	Def. S.	50 14 66 10		on shore.	լս•ցցս∽			0.989*	≻1.001	
90	Yard.		Def. N.S. Needle N.	i		K	1.002		-002	1.000	₹	
30.			Needle S.	45 0 49 5			0·989 0·996			0.989 0.996	1	,
			Mag. N.S.	66 2		On shore.	0.990		•000	0.996	1	
			Mag. N.	43 4		On shore.	0.989			0.989		
			Mag. S.	47 2		11	0.997			0.997	1	1
July 2.			Needle N.	44 3		K	1.005		1	1.005	1	1
our, a			Needle S.	49 4	1	1.1	1.005		•000			
			Needle N.S.	1 -		11	0.998			0.997	1	
			Mag. N.	43 1.	63	On ahama	1.006		•000		1	
			Mag. S.	47 2		On shore.	0.999		. 000	0.999		
			wt. 1 gr.	28 2			0.993		•000		>1.000)
			wt. 1½ gr.	44 1			0.999	ļ	. 000	0.999	1	
			wt. 2 grs.	69 1		Ŋ.	1.001		1	1.001	j	
11.	Magnet	ic Ob-	Def. N.	44 3		1)	1.006		1	1.005	1	
	servator		Def. S.	49 4		11	1.002			1.001	1	
	of Good	Hope.	Mag. N.S.	66 0	75		1.003	ļ		0.999	1	
			Mag. N.	43 2		On shore.	1.002	ļ	1	1.001		
			Mag. S.	47 1			1.004			1.003		
			wt. 1 gr.	28 0 44 1	1		1.007		+.001	1.008	}	
		. *	wt. $1\frac{1}{2}$ gr. wt. 2 grs.	69 3			1.001		+.001		1	1
			we. & grs.	109 3	10	Υ .	0.999	}	. +•001	1.000	J.	l

^{*} Not included in mean.

Observations of the Magnetic Force made on board Her Majesty's hired Bark "Pagoda," from the 1st of December 1844 to the 2nd of July 1845. Needle 1. Fox No. 1.; Face West; time usually two hours before Noon.

Observer, Lieut. H. CLERK, R.A.

								Corre	ctions.		
Date.	Lat.	Long.	Method	Angle of deflec- tion.	rmo-	Ship's head.	Intensity.	Ship's	m	Corrected	Remarks.
			employed.	tion.	The	Ship b noud	Inte	attrac-	Tempe- rature.	Intensity.	
1844.											
Dec. 1.	-33° 56	18 29	Def. N.	39°06	6ŝ	1	1.006		-000	1.006	
			Def. S.	40 38	67		1.001		-·001	1.000	· ·
				59 23 21 29	68 70		0·981 1·009		+.001	0.980 1.010	
				46 54	71		0.995		+.001	0.996	
	Magneti		wt. $2\frac{1}{2}$ grs.	65 22	72	Observed	1.000		+.001	1.001 0.999	
5.	servatory		Def. N.	39 01	72	on shore.			001	1.007	
	of Good	Hope.		40 37 59 22	72 73		1.001 0.983		-·001 -·003	1.000	
				21 34	74		1.006		+.001		
				46 33	74		1.001		+.001	1.002	
			wt. $2\frac{1}{2}$ grs.	65 19	74	IJ.	1.001		+.001	1.002	
21.	-34 12	18 26		39 04	74	n	1.007		001	1.006	
				40 25 59 11	76 78	Observed	1.007		-·001 -·004	1.006	
	Dock			21 04	78	on shore.			+.001	1.030 >1.005	
	Simon's	s Bay.		46 30	78		1.002		+.001	1.003	
			wt. $2\frac{1}{2}$ grs.	65 49	78	IJ.	0.997		+.001	0.908	
1845.	-34 44	17 50	Def. N.	39 42	70	w. by n.	0.986	009	001	0.9767	
Jan. 10.	-01 11	17 00		40 39	70	w. by N.	1.000				Table unsteady.
, i				59 11	70		0.988		002	0.977	Lusto ansound,
13.	-3512	13 28	Def. N.	40 02	72	s.w. by w.	0.976			0.945	
				40 40	72		0.999		001	0.968	
				59 25 22 00	75 70	1	0.980 0.987		-·003 +·001	$\begin{vmatrix} 0.937 \\ 0.948 \end{vmatrix} > 0.950$	Table steady.
				47 02	69		0.992	1		0.953	
		·	wt. $2\frac{1}{2}$ grs.		68		0.987	1	+.001	0.948	
14.	-37 25	13 24	Def. N.	38 52	65	s. by w.	1.013		.000	0.971	
				40 22	65	s. by w.	1.009	1	001	0.967 >0.965	Table unsteady.
15	—38 37	14 27		58 50 38 55	65 62	s. by w.	1.000		-000	1.015	
10.	000,	~ ~,		39 55	62	N.w. by w.			•000		Very unsteady.
			Def. N.S.	59 25	66	N.W. by W.	0.980	+.003	001	0.982	,
16.	-39 10	14 41		38 47	63	s.w.byw. $\frac{1}{2}$ w.	1.016	026	•000	0.990	
				39 35		s.w.byw. $\frac{1}{2}$ w.			-·000 -·001	1.008	
				58 30 21 32		s.w.byw. $\frac{1}{2}$ w.s.w.byw. $\frac{1}{2}$ w.			•000	$\begin{vmatrix} 0.982 \\ 0.982 \end{vmatrix} > 0.989$	Table steady.
				45 22		s.w.by $w.\frac{1}{2}w.$ s.w.by $w.\frac{1}{2}w.$		-026	.000	0.995	
			wt. $2\frac{1}{2}$ grs.			s.w.byw. $\frac{1}{2}$ w.	1.005	026	•000	0.979	·
17.	-40 21	14 29	Def. N.	38 42	64	s.w. by w.	1.019	029		0.9907	`
				39 25	65			029	-·000		Much motion.
12	-42 50	13 00		58 27 38 32	65 60			-·029 -·040	-000	0·981	
10.	1~ 00	10 00	Def. S.	38 35	5 9			040	.000	1.026 >0.997	Much motion.
				58 07	58		1.021		.000	0.981	*
19.	-44 50	13 19		38 17	48	s.w. by s.	1.033		+.001	0.997	
	-			39 02	45	_ •	1.051		+.001	1.015 >1.007	Much motion.
			Def. N.S.	57 27	44	s.w. by s.	1.044	037	T 003	1.010	·

								Correc	tions.		
Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.	Thermo meter.	Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected Intensity.	Remarks.
1845.		0 /		0 /							
Jan. 21.	$-4\mathring{7} \ 4\acute{0}$		Def. N.	36 30	43		1.091		+.001		Very unsteady.
22.	-48 35	10 51	Def. N.	36 15	48	s.w. by s.	1.101	1	+.001		m 11
			Def. S. Def. N.S.	37 35 56 28	48 47	s.w. by s.	1.090	-·037 -·037	+.003		Table steady.
23.	-50 30	10 25	Def. N.	35 10	43	S.W. $\frac{1}{2}$ S.	1.140	1	+.001	1.105	
~~.	-00 00	10 20	Def. S.	36 37	43	$s.w. \frac{1}{2} s.$	1.141		+.001		Table steady.
			Def. N.S.	55 47	43	$s.w. \frac{1}{2} s.$	1.105	1	+.003	1.072	
24.	-51 48	9 33	Def. N.	34 47	48	s.w. by w.	1.154	029	+.001	1.126	
			Def. S.	36 10	47	s.w. by w.			+.001		Table steady.
			Def. N.S.	55 07	47	s.w. by w.	1.131		+.003		
25.	-5253	7 53	Def. N. Def. S.	34 57	41	s.w. by w.	1.148		+.001	1.120	D 0
			Def. N.S.	35 47 55 17	40	s.w. by w.	1·173 1·125		+.001 + .004		Rather unsteady.
26.	-53 52	6 07	Def. N.	34 22	43	w. by s.	1.171		+.001	1.152	
""	00 0%		Def. S.	35 42	43	w. by s.	1.175	}	+.001	1.156	į
			Def. N.S.	54 30	42	w. by s.	1.155	020	+.003	1.138	Very steady.
ļ		*	wt. 1 gr.	18 12	41	w. by s.	1.185		001	1.104	very steady.
Ì			wt. 2 grs.	39 40	40	w. by s.	1.138		001	1.117	
07	FF 00	F 50	wt. $2\frac{1}{2}$ grs.	51 50	39	w: by s.	1.155		$ 001 \\ +.002$	1.134	
27.	-55 08	5 50	Def. N. Def. S.	$\begin{vmatrix} 33 & 05 \\ 35 & 52 \end{vmatrix}$	38	S.S.W. $\frac{1}{2}$ W.S.S.W. $\frac{1}{2}$ W.	1.221 1.201		+.002	$\begin{vmatrix} 1.185 \\ 1.165 \end{vmatrix}$ 1.161	Very unsteady.
			Def. N.S.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	37	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.167	,	+.005	1.134	very unsteady.
30.	$-60 \ 43$	4 00	Def. N.S.	51 57	35	s.	1.262			1.219	
1			Def. N.S.	51 35	34	s.e. by e.	1.282				Table unsteady.
1			Def. N.S.	52 22	34	N.	1.246		+.006	1.248	
31.	-61 05	9 03	Def. N.	30 57	42	s.E. by s.	1.320		+.002	1.278	
			Def. S.	31 55		s.E. by s.	1.339		+.002	1.297	
			Def. N.S.	$\begin{vmatrix} 51 & 22 \\ 16 & 02 \end{vmatrix}$		s.E. by s.	1.340		+·005 -·001	$\begin{vmatrix} 1.255 \\ 1.295 \end{vmatrix}$ 1.285	Table steady.
			wt. 1 gr. wt. 2 grs.	32 22	1	s.e. by s.	1.343		1	1.298	
			wt. $2\frac{1}{2}$ grs.	43 02	1 .	s.E. by s.	1.332			1.287	
Feb. 2	-61 54	16 23	Def. N.	29 57	40	E.S.E.	1.368	-032	+.003	1.339	
	}		Def. S.	30 57		E.S.E.	1.384	-032	+.003		Table unsteady.
	0	10.10	Def. N.S.	50 45		E.S.E.	1.325		+.006	1.299	
3.	-61 50	19 13		30 10	1	E.S.E.	1.348		+.002	1.318	
1			Def. S. Def. N.S.	31 20 50 20		E.S.E.	1.366 1.346	-032	+·002 +·006	1.336	
			wt. 1 gr.	15 05	1 -	E.S.E.	1.420				Very steady.
1			wt. 2 grs.	31 55		E.S.E.	1.376		1 .	1	
1			wt. $2\frac{1}{2}$ grs.	42 57		E.S.E.	1.336	-032	+.002	1.302	
4	-62 00	0 20 25	Def. N.	29 30		S.S.E.		-046	+.003	1.345	
1			Def. S.	30 37		S.S.E.	1.401	-046	+ 003	1.358 >1.353	Very steady.
6	_ GA 0	0 24 05	Def. N.S. Def. N.	49 27 28 00		S.S.E.	1.396	-·046 -·050			
	-04 2	24 03	Def. S.	29 57		S.S.E. S.S.E.	1.435		+.003	1.388	
			Def. N.S.	49 02		S.S.E.	1.422			11.270	
			wt. 1 gr.	14 17		S.S.E.	1.499	1			Very steady.
		1	wt. 2 grs.	30 00	36	S.S.E.	1.454	3	1	1.402	
	0	1 20 22	wt. $2\frac{1}{2}$ grs.	39 40		S.S.E.	1.425				
7	-65 3	4 28 30		27 3		S.S.E. $\frac{1}{2}$ E.	1.481		+.002		***************************************
			Def. S. Def. N.S.	28 57	7 42 7 42	S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E.	1.486				Very steady.
9	-663	0 36 46	Def. N.	26 59		E.	1.519				
1			Def. S.	28 3		E.	1.506			1.484 >1.482	Very steady.
1		1	Def. N.S.	48 00	32	E.	1.483		+.008	1.465	
10	$ -66 \ 4$	3 38 49		26 1		s.s.w.	1.553		1 -		
1 .	1	1	Def. S.	28 00		s.s.w.	1.538				Very steady.
	<u> </u>		Def. N.S.	47 30	34	S.S.W.	1.516	090	+.007	1.473	

			Mathad	Angle of	00- 2r.		sity.	Corre	ctions.	()	
Date.	Lat.	Long.	Method employed.	deflec- tion.	Thermo- meter.	Ship's head.	Intensity.	Ship's attrac- tion.	Tempe- rature.	Corrected Intensity.	Remarks.
1845.	م د	000	T) ()]	-2 -4	0			0.0			
Feb. 11.	-67° 35	39 31	Def. N.	26 35	33	i i	1.534				
			Def. S.	27 55	32	N.E.	1.544	016	, .		Very unsteady.
10	 66 45	20 00	Def. N.S.	47 35	31	N.E.	1.510	-016		1.50%	
12.	00 40	39 23	Def. N. Def. S.	26 12 28 17	37	S.S.E.	1.556 1.522	049	+·003		Very unsteady.
			Def. N.S.	28 17 47 12	37 37	S.S.E. S.S.E.	1.537		+.007		cry unsteady.
13.	-67 00	40 07	Def. N.	26 22	37	E.N.E.	1.547	025			2.5
01	0, 00	20 0,	Def. S.	28 10	36	E.N.E.	1.529	025	+.003		
			Def. N.S.	47 42	35	E.N.E.	1.504	025		1.486	
			wt. 1 gr.	14 00	32	E.N.E.	1.529	025	-002		Table steady.
			wt. 2 grs.	28 17	32	E.N.E.	1.534				
	,		wt. $2\frac{1}{2}$ grs.	37 27	32	E.N.E.	1.496	-025	002	1.469	l
16.	-64 52	38 37	Def. N.	27 10	37	S. 3/4 E.	1.504				Very unsteady.
	_		Def. S.	28 02	37	S. $\frac{3}{4}$ E.	1.536		+.003	1.480	very unsteady.
17.	-6452	40 12	Def. N.	27 34	38	N. by w.	1.488	019			
		1	Def. S.	29 12	38	n. by w.	1.473				Very unsteady.
10	C4 ac	1	Def. N.S.	48 10	38	N. by w.	1.473				
18.	-64 22	40 49		26 52	38	s. by E.	1.519				Very unsteady.
10	-63 49	10 00	Def. S. Def. N.	28 42	37	s. by E.	1.500 $ 1.431 $		+.003		
19.	-03 49	42 00	Def. N.	28 35 29 47	39 37	E. by s.	1.443		+·003		Very unsteady.
			Def. N.S.	48 15	36	E. by s.	1.468		+.006		very unsteady.
- 20.	-63 22	45 35		29 02	44	s.e. by $E \cdot \frac{1}{2}E$.				1.425 3	
~00	-05 22	10 00	Def. N.S.	48 00	45	s.E. by E. $\frac{1}{2}$ E.				1 - 1.437	Very unsteady.
21.	-63 36	46 41	Def. N.	27 00	42	S.S.E.	1.512			1	
		1	Def. S.	28 37	41	S.S.E.	1.505	1			Table unsteady.
			Def. N.S.	47 52	41	S.S.E.	1.491	049			
24.	$-62 \ 36$	51 40		47 54	36	E.	1.490	031	+.007	1.466	į
		1	Def. N.	26 45	36	E.	1.526				Very unsteady.
			Def. S.	29 27	34	E.	1.460	031	+.004	1.433	
25	-61 25	53 38		27 05	40	E.S.E.	1.507		+.003	1.471	
			Def. S.	28 32	39	E.S.E.	1.510		+.003		Unsteady.
~ 0	C	-	Def. N.S.	47 30	38	E.S.E.	1.516		+.006		}
26.	-61 17	7 57 28		25 30	41	S.E. 1 E.	1.595		+.002		
	1	1	Def. S. Def. N.S.	27 30	42	S.E. ½ E.	1.566 1.567		+·002 +·005		Table unsteady.
27	61 0	64 03		46 45 25 17	37	S.E. $\frac{1}{2}$ E.	1.607		+.003		
21	-01 0	04 03	Def. S.	26 30	36	S.E. $\frac{1}{2}$ S. S.E. $\frac{1}{2}$ S.	1.622	-050	+.004	1.576	Table steady.
			Def. N.S.	46 47	35	S.E. $\frac{1}{2}$ S.	1.564	050	+.008	1.522	, and a sound y
28	$-61 \ 30$	6 70 46		24 22	40	S.S.E.		-052	+.003	1:611 5	
	0	1.	Def. S.	25 57	39	S.S.E.	1.654	-052	+.003	1.605 1.604	Table unsteady.
	ĺ		Def. N.S.	45 42	38	S.S.E.	1.640	052	+.007	1.595	
Mar. 1	-62 10	72 25	Def. N.	23 10		S.S.E.	1.731	-052	+.002	1.681	
			Def. S.	25 37	44	S.S.E.	1.674	-052	+.002	1.624	1
		ļ	Def. N.S.	44 50	44	S.S.E.	1.705		+.005		Table steady.
			wt. 1 gr.	11 37	44	S.S.E.	1.837			1.784*	Table steady.
		1	wt. 2 grs.	25 00	43	S.S.E.	1.719			1.666	
_		1 -0 01	wt. $2\frac{1}{2}$ grs.	32 12	43	S.S.E.	1.602	1		1.655	
2	-02 4	0 76 09		23 50	42	s.	1.693			1.639	
			Def. S.	25 10	42	s.	1.699		+.002	11.660	1
		1	Def. N.S.	44 45	41	S.	1.710 $ 1.838$		+.006	1.781*	Very steady.
	1	1	wt. 1 gr. wt. 2 grs.	11 35 24 47	1	S.	1.733			1.676	-
		1	wt. $2 \frac{1}{2}$ grs.	32 00		S. S.	1.718			1.661	
	1		1 " " ~ 2 818.	52 00	1 33	6.	- •	1 000	""	ر ۱۰۰۰	1

^{*} Not included in the mean; angle of deflection become too small.

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1845. Mar. 364 20 79 38 Def. N. 22 38 33 s. by w. \frac{1}{2} w. 1.764 -0.55 +0.04 1.712 1.706 Table unsteady.					A mode of	٠. ٥	:	ty.	Correc	ctions.		
1845. Mar. 364 20 79 38 Def. N. 22 38 33 s. by w. \frac{1}{2} w. 1.764 -0.55 +0.04 1.712 1.706 Table unsteady.	D = 4 =		. 1	Method		E ii	Shin's head	ısı	Chi.	Tomana	Corrected	Remarks
1845 Mar. 363 20 79 36 Def. N. 22 38 33 s. by w. \frac{1}{2} w. 1.764 -0.55 +0.04 1.712 1.706 Table unsteady 1.706 Def. N. 24 17 32 s. by w. \frac{1}{2} w. 1.764 -0.55 +0.04 1.703 1.706 Table unsteady 1.706 Def. N. 24 20 40 s. k. 1.706 -0.55 +0.04 1.703 1.706 Table unsteady 1.706 Def. N. 24 20 40 s. k. 1.706 -0.55 +0.04 1.703 1.706 Table unsteady 1.706 Def. N. 24 20 40 s. k. 1.706 -0.55 +0.04 1.703 1.706 Table unsteady 1.706 Def. N. 24 20 40 s. k. 1.706 -0.55 +0.04 1.703 1.706 Table unsteady 1.706 Def. N. 24 20 40 s. k. 1.706 -0.55 +0.04 1.703 1.706 Table unsteady 1.706 Def. N. 24 20 40 s. k. 1.706 -0.55 +0.04 1.703 1.706 Table unsteady 1.706 Def. N. 24 20 40 s. k. 1.706 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 Def. N. 24 20 De	Date.	Lat.	Long.	employed.		ner	Ship's neau.	ţe.			Intensity.	itemarks.
Bis45. Mar. 3. -64 20 79 38 Def. N. 22 38 38 s. by w. \frac{1}{2} w. 1.763 -0.055 +0.04 1.712 1.706 Table unsteady 1.712 1.706 Table unsteady 1.712 1.706 Table unsteady 1.712 1.706 Table unsteady 1.712 1.706 Table unsteady 1.712 1.706 Table unsteady 1.712 1.706 Table unsteady 1.712 1.706 Table unsteady 1.712 1.706 Table unsteady 1.712 1.706 Table unsteady 1.712 1.706 Table unsteady 1.712 1.706 Table unsteady 1.706				- •	tion.	E		l a		rature.		
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Def. N.S. 44 12 32 32 32 32 33 34 32 32	Mai. 9.	-04 20	19 30									Table unsteads
561 38 8 44 40 Def. N. 23 02 39 S.E. 1.740 -0.61 1.903 1.704 Def. N. 24 20 40 Def. N. 24 20 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 25 40 Def. N. 26 40 Def. N. 26 40 Def. N. 26 40 Def. N. 27 40 Def. N. 28							s. by w. \frac{1}{2} w.	1.754	- 055	+ 004		Table unsteady,
Def. S. 24 20 40 S.E. 1.752 -0.051 -0.031 7.04						32				+.009	1.704	1
Def. S. 24 20 40 S.E. 1.752 -0.51 +0.03 1.704 1.704 Def. N. 29 40 36 N.E. 2 N. 1.761 -0.95 +0.04 1.749 1.7	5.	-61 38	84 40	Def. N.	23 02	39	S.E.	1.740	051	+.003	1.692	
Def. N.S. 44 40 41 S.E. 1716 -051 +007 1672 Def. N.S. 22 40 36 N.E. \frac{1}{2} \text{ N. 1760 -052 +004 1759 1729 Table unsteady Def. N.S. 43 50 35 N.E. \frac{1}{2} \text{ N. 1760 -025 +004 1759 1729 Table unsteady Def. N.S. 43 50 35 N.E. \frac{1}{2} \text{ N. 1765 -025 +004 1759 1779 1779 1761 Def. N.S. 43 30 42 S. by E. 1831 -055 +003 1779 1779 1770 Def. N.S. 43 30 42 S. by E. 1831 -055 +003 1779 1770 Def. N.S. 43 30 42 S. by E. 1830 -055 +003 1779 1770 Def. N.S. 43 30 42 S. by E. 1830 -055 +003 1779 1770 Def. N.S. 43 30 42 S. by E. 1800 -055 +003 1770 1770 Def. N.S. 43 30 42 S. by E. 1830 -055 +003 1770 1770 Def. N.S. 43 30 42 S. by E. 1830 -055 +003 1770 Def. N.S. 43 30 42 S. by E. 1800 -055 +003 1770 Def. N.S. 43 30 42 S. by E. 1800 -055 +004 1751 Def. N.S. 43 30 42 S. by E. 1800 -045 +004 1751 Def. N.S. 43 30 42 S. by E. 1800 -045 +004 1751 Def. N.S. 43 40 38 E. 1870 -045 +004 1758 Def. N.S. 43 40 38 E. 1870 -045 +004 1758 Def. N.S. 43 40 38 E. 1870 -045 +004 1758 Def. N.S. 43 40 38 E. 1870 -045 +004 1760 Def. N.S. 43 45 36 E. \frac{1}{2} S. 1867 -055 +004 1760 Def. N.S. 43 45 36 E. \frac{1}{2} S. 1867 -055 +004 1760 Def. N.S. 43 45 36 E. \frac{1}{2} S. 1867 -055 +004 1760 Def. N.S. 43 45 36 E. \frac{1}{2} S. 1867 -055 +004 1760 Def. N.S. 43 45 36 E. \frac{1}{2} S. 1867 -055 +004 1760 Def. N.S. 43 45 36 E. \frac{1}{2} S. 1867 -055 +004 1760 Def. N.S. 43 45 36 E. \frac{1}{2} S. 1867 -055 +004 1760 Def. N.S. 43 45 36 E. \frac{1}{2} S. 1867 -055 +004 1760 Def. N.S. 43 45 36 E. \frac{1}{2} S. 1860 Def. N.S. 43 45 36 E. \frac{1}{2} S. 181				Def. S.	24 20		S.E.	1.752	051	+.003	1.704 >1.689	Table unsteady.
Care Care									051	+.007	1.672	
Def. S. 23 55 36 N.E. \(\frac{1}{2} \) N. 1.780 -0.025 +-0.04 1.759 -0.795 -0.024 1.759 -0.025 -0.004 1.759 -0.025 -0.004 1.759 -0.025 -0.004 1.759 -0.025 -0.004 1.759 -0.025 -0.004 1.750 -0.025 -0.004 1.751 -0.025 -0.025 -0.004 1.751 -0.025 -0.02	6.	_60 42	88 19							+.004	1.740 5	
Def. N.S. 44 50 35 So. N.E. 1.765 N. 1.	9.	00 12	00 12									Table unsteady
761 20 91 09 Def. N. 22 02 40 s. by E. 1-800055 +-003 1.748 Def. N. Def. N. S. 43 30 42 s. by E. 1-831055 +-003 1.779 1.761 Def. N. 22 00 40 s. by E. 1-835055 +-007 1.757 Def. N. S. 43 30 42 s. by E. 1-805055 +-007 1.757 Def. N. S. 32 32 40 s. by S. 1-800054 +-004 1.762 Def. N. S. 43 37 39 s. b. by S. 1-800054 +-004 1.762 Def. N. S. 43 37 39 s. b. by S. 1-800054 +-004 1.755 Def. N. S. 43 32 37 s. d. 1-796042 +-004 1.755 Def. N. S. 43 32 37 s. d. 1-796042 +-004 1.755 Def. N. S. 43 32 37 s. d. 1-804042 +-004 1.755 Def. N. 2 95 34 E. 1-801045002 1.843* wt. 2 grs. 29 05 35 E. 1-801045002 1.843* wt. 2 grs. 29 05 34 E. 1-870045002 1.843* dw. 2 grs. 29 05 34 E. 1-870045002 1.843* dw. 2 grs. 29 05 34 E. 1-870045002 1.843* dw. 2 grs. 29 05 34 E. 1-870045002 1.754* dw. 2 grs. 23 50 35 E. 1-801045002 1.754* dw. 2 grs. 23 50 35 E. 1-801045002 1.754* dw. 2 grs. 23 50 35 E. 1-801045002 1.754* dw. 2 grs. 23 50 35 E. 1-801045002 1.754* dw. 2 grs. 23 50 35 E. 1-801045002 1.754* dw. 2 grs. 23 50 35 E. 1-801045002 1.754* dw. 2 grs. 23 50 35 E. 1-801045002 1.754* dw. 2 grs. 23 50 35 E. 1-801045002 1.754* dw. 2 grs. 23 50 35 E. 1-801045002 1.754* dw. 2 grs. 23 50 35 E. 1-801045002 1.754* dw. 2 grs. 23 50 35 E. 1-801045003 1.753* dw. 2 grs. 23 42 35 G. 1-810047004 1.759 Def. N. 22 57 37 E. 5 s. 1-810047 +-004 1.759 Def. N. 22 32 42 35 E. § N. 1-810042003 1.763* dw. 2 grs. 23 42 35 G. E. § N. 1-810042003 1.765* dw. 2 grs. 23 42 35 G. E. § N. 1-810042003 1.765* dw. 2 grs. 23 42 35 G. E. § N. 1-810042003 1.765* dw. 2 grs. 23 42 35 G. E. § N. 1-810042003 1.765* dw. 2 grs. 23 42 35 G. E. § N. 1-810042003 1.765* dw. 2 grs. 23 42 35 G. E. § N. 1-810042003 1.765* dw. 2 grs. 23 42 35 G. E. § N. 1-810042003 1.765* dw. 2 grs. 23 42 35 G. E. § N. 1-810042003 1.765* dw. 2 grs. 23 42 35 G. E. § N. 1-810042003 1.765* dw. 2 grs. 23 42 35 G. E. § N.		*								7.000		Table unsecauy.
Def. N.S. 23 05 41 s. by E. 1-831 -055 +003 1-779 1-757	,	0. 00								+ 000	1.088	
Def. N.S. 43 30 42 S. b. by E. 1-805 -055 +-007 1-757 1-751 1-756	7.	-61 20	91 09									
Color Colo	-			Def. S.	23 05	41	s. by E.	1.831	-055	+.003	1.779 >1.761	
Color Colo				Def. N.S.	43 30		s. by E.	1.805	055	+.007	1.757	1 .
Second Continue	•	-61 26	91 20					1.801	054	+.004	1.751	
861 14 92 03 Def. N. 22 05 39 Def. N. 22 05 39 Def. N. 22 05 39 Def. N. 23 37 38 E. 1795042 +-004 1758 Def. N. 24 33 32 37 E. 1796042 +-004 1758 Def. N. 25 35 35 Def. N. 22 17 41 E. 1780045002 1754 Def. N. 22 17 41 Def. N. 23 55 37 Def. N. 23 55 37 Def. N. 24 35 58 37 Def. N. 24 35 58 37 Def. N. 26 57 36 Def. N. 20 57 36 Se. \frac{1}{2}\$S. \frac{1}{			J. 7.						054	+.004	1.762 >1.756	Table unsteady.
861 14 92 03 Def. N. 22 05 36 Def. N. 23 37 38 Def. N. S. 23 37 38 Def. N. S. 43 32 37 wt. 1 gr. 11 17 36 E. 1:890042 +-004 1:757 wt. 2 grs. 23 50 35 E. 1:890045002 1:823* Def. N. S. 43 32 37 E. 1:870045002 1:823* Def. N. S. 21 7 41 E. 1:870045002 1:823* Def. N. S. 23 55 37 Def. N. S. 23 55 37 Def. N. S. 24 05 36 E. 1:870045002 1:823* Def. N. S. 24 17 41 E. 1:783045 +-003 1:741 Def. S. 23 57 36 S.E. \frac{1}{2} \text{ N. S. 1045} \text{ -004 1:739} \text{ -1.45 Table unsteady.} \text{ 1:70045} \text{ -004 1:739} \text{ -045 +-004 1:739} \text{ -1.45 Table unsteady.} \text{ -045 +-004 1:739} \text{ -045 +-004 1:739} \text{ -045 +-004 1:739} \text{ -045 +-004 1:739} \text{ -045 +-004 1:739} \text{ -045 +-004 1:739} \text{ -045 +-004 1:739} \text{ -045 +-004 1:739} \text{ -045 +-004 1:739} \text{ -045 +-004 1:739} \text{ -045 +-004 1:739} \text{ -1.45004 1:739} \text{ -045 +-004 1:739} \text{ -045 +-004 1:739} \text{ -1.45004 1:739} \text{ -045 +-004 1:739} \text{ -1.45004 1:739} \text{ -045 +-004 1:739} \text{ -1.45004 1:739} \text{ -045 +-004 1:739} \text{ -1.45004 1:739} \text{ -045 +-004 1:739} \text{ -1.45004 1:739} \text{ -045 +-004 1:739} \text{ -1.45004 1:739} \text{ -045 +-004 1:739} \text{ -1.45004 1:739} \text{ -045 +-004 1:739} \text{ -1.45004 1:739}								1	.054	1.008	1.754	
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	٥.	-01 14	92 03	Der. N.					042	+ 004	1.737	
Wt. 1 gr. 11 17 36 E. 1.890 -0.45 -0.02 1.843* 1.702 1.003 according to the content of the co							1					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				Def. N.S.	43 32	37	E.	1.804	-042	+.008	1.770 \1.769	Table steady.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				wt. 1 gr.	11 17	36	E.	1.890			1.843*	, and a second
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				wt. 2 grs.	23 50		Е.	1.801	045	002	1.754*	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				wt. 21 grs.			1	1				
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.	-60 03	95 36					1				Very unsteady.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				Def. S.	23 07	36	S.E. $\frac{1}{2}$ S.	1.831	055	+.004	1.780	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.	-5952	99 30	Def. N.	21 05	38	E. 1/2 S.	1.810	047	+.004	1.767)	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5											Very unsteady.
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												Table unsteady
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				wt. 1 gr.	11 20	35	E. 1 N.	1.884	-042		1.839*	5 P.M.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				wt. 2 grs.	23 42	35	E. $\frac{1}{2}$ N.	1.810	-042	003	1.763	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												
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$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	15.	-5552	103 06	1				1.848	-·042	+.004	1.810	<u>.</u>
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E C				22 35	39	E. by N.	1.864	-042	 +.004		Very unsteady.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				Def. N.S.	43 00		E. by N.	1.845	042	+.008	1.811	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	16.	-5448	106 04		1				036	+.004	1.800 5	1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							1	1	036	+.004	1.812 1.801	Very unsteady.
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			1			•	i .					
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.7	EA 15	100 0		3	1 .	1	1 .				
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1/.	-54 17	100 09			1	ī	1			1- 000 1	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							1					Very unsteady, ship
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$							E.				1.785	pitching heavily.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				Def. S.	23 10	40	E.	1.830				
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	18.	-53 00	110 08	Def. N.		40	N.N.E. 1 E.					
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	T. C.	1		Def. S.								Very unsteady, a
1951 20 111 23 Def. S. 23 20 41 N.N.E. \(\frac{1}{2}\) E. 1.816 034 +.004 1.786 1.787 Very Insteady									024	1.008		heavy swell.
	10	E1 00	111 00									1
I TO CATO LAB GOLLAND TO STAND CALL MADE TO 17/07/Very unsteady,	19.	- 31 20	111 23			1 '						Very unsteady, a
Def. N.S. 43 22 41 N.N.E. $\frac{1}{2}$ E. 1.818 -0.034 $+0.04$ 1.788 $\frac{1}{2}$ 1.707 heavy swell.	1	,		Det. N.S.	43 22	41	N.N.E. $\frac{1}{2}$ E.	1.818	-034	+.004	1.488	heavy swell.

^{*} Not included in the mean.

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.798	Remarks. Table unsteady, swell from west.
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.798	Table unsteady,
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		Table unsteady, swell from west.
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		Table unsteady, swell from west.
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		Table unsteady, swell from west.
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		Table unsteady, swell from west.
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		Table unsteady, swell from west.
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.825	swen nom west.
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.825	1 1
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.825	
	1.825	
	7 - 020	Steady, light swell from west.
Def. N.S. 43 20 48 E.N.E. 1.821035 +.005 1.791	Į	Hom west.
2543 20 16 52 Def. N. 23 27* 51 N. $\frac{1}{2}$ E. $1 \cdot 712$ $- \cdot 025$ $+ \cdot 002$ $1 \cdot 689 \uparrow$ Def. S. 23 35 51 N. $\frac{1}{2}$ E. $1 \cdot 799$ $- \cdot 025$ $+ \cdot 002$ $1 \cdot 776$		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1	
wt. 1 gr. $\begin{vmatrix} 12 & 07 \\ 12 & 07 \end{vmatrix}$ $\begin{vmatrix} 50 \\ 50 \end{vmatrix}$ N. $\frac{1}{2}$ E. $\begin{vmatrix} 1783 \\ -025 \end{vmatrix}$ $\begin{vmatrix} -003 \\ -001 \end{vmatrix}$ $\begin{vmatrix} 1783 \\ 1\cdot784 \end{vmatrix}$	>1.760	Very unsteady, heavy swell from west.
wt. 2 grs. $\begin{vmatrix} 23 & 32 \\ 23 & 32 \end{vmatrix}$ 50 N. $\frac{1}{2}$ E. $\begin{vmatrix} 1.823 \\025 \end{vmatrix}$ 001 $\begin{vmatrix} 1.797 \\ 1.797 \end{vmatrix}$		Sweet I on west
wt. $2\frac{1}{2}$ grs. 31 17 50 N. $\frac{1}{2}$ E. 1.752 025 001 1.726]	
2641 18 116 09 Def. N. 22 30 54 N. by w. 1·771 -·020 +·001 1·752])	
Def. S. 23 57 54 N. by w. $ 1.776 020 + .001 1.757$	>1·74 6	Unsteady, light swell.
Def. N.S. 44 15 54 N. by w. 1.747 020 +.002 1.729)	Swc.ii.
2738 52 116 15 Def. N. 22 37 58 N. by w. 1.765 012 .000 1.753 Def. S. 23 52 58 N. by w. 1.770 012 .000 1.758	1.720	Table steady.
Def. N.S. 23 52 58 N. by w. 1.770 012 .000 1.758 0.00 1.704 0.000 0.00	>1.738	Table steady.
2837 03 116 57 Def. N. 23 25 59 N. by E. 1.718 -012 000 1.706)	
Def. S. 24 45 60 N. by E. 1.725012 .000 1.713		
Def. N.S. 44 30 61 N. by E. 1.728012 .000 1.716	1.00	
wt. 1 gr. 12 45 62 N. by E. 1.678 012 .000 1.666	>1.099	Table very steady, nearly a calm.
wt. 2 grs. $ 25 \ 40 \ 62 $ N. by E. $ 1.678 - 012 \ 000 1.666 $		
wt. $2\frac{1}{2}$ grs. 32 07 63 N. by E. $ 1.714 012 .000 1.702 $)	
2936 12 116 50 Def. N. 23 40 66 N.N.E. 1.701 -012 -001 1.688	1.000	(II-1-1 / I
Def. S. 25 37 67 N.N.E. 1.673 012 001 1.660 1.670	>1.673	Table unsteady.
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$)	
Def. S. $\begin{vmatrix} 24 & 45 \end{vmatrix} & 66 \begin{vmatrix} \text{N.E.} & \frac{1}{2} & \text{E.} \end{vmatrix} \begin{vmatrix} 1 \cdot 725 \end{vmatrix} = \cdot 012 \begin{vmatrix} -\cdot 001 \end{vmatrix} \cdot 712 \end{vmatrix} \cdot 712 \begin{vmatrix} -\cdot 001 \end{vmatrix} \cdot 712 \begin{vmatrix} -\cdot 001 \end{vmatrix} \cdot 712 \end{vmatrix} \cdot 71$	1.702	Table unsteady.
Def. N.S. $ 44 52 66$ N.E. $\frac{1}{2}$ E. $ 1.701 012 002 1.687$	(- ,	,
April 735 02 117 56 Def. N. 23 50 68 7 1.692001 1.691	i ·	
Def. S. 25 18 68		
Def. N.S. 45 06 69		
11. King George's Def. N. 23 42 82 On shore 1.700 002 1.698	≻¹·6 88	The observations were made on the
Sound, West Def. S. 25 12 82		same spot where Captains Flin-
Australia. Def. N.S. 44 59 83		DERS and FITZ-
wt. 1 gr. 12 37 84		ROY had pre- viously observed.
wt. 2 grs. 25 30 84 1 1.689 + .001 1.690		
wt. $2\frac{1}{2}$ grs. $33 \ 01 \ 85 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	1	
19. At Anchor in Def. N.S. $ 44 09 $ 54 s.s.w. $ 1.754 056 +.001 1.699$ 1.699 54 s.w. $ 1.740 051 +.001 1.690$. :	
the Sound Def. N.S. 44 20 54 s.w. 1.740051 +.001 1.690 Swinging the Def. N.S. 44 30 54 w.s.w. 1.728041 +.001 1.688		ľ
ship for local Def. N.S. 44 44 54 w. 1.710032 +.001 1.679		
attraction. Def. N.S. 44 50 54 w.n.w. 1.702022 +.001 1.681		
Def. N.S. $ 45\ 04\ 54\ $ N.W. $ 1\cdot687\ -\cdot012\ +\cdot001\ 1\cdot676\ $		
Def. N.S. $ 45\ 01 $ 54 N.N.W. $ 1.691 012 + .001 1.680 $		
Def. N.S. 44 59 57 N. 1.692 012 +.001 1.681		The table was very steady during
Def. N.S. 45 03 58 N.N.E. 1.688 012 .000 1.676	>1·683	these observations.

^{*} The degree should probably be 22°; not included.

[†] Not included in the mean.

								Corre	ctions.		
_		_	Method	Angle of deflec- tion.	no- er.		Intensity.			Corrected	
Date.	Lat.	Long.	employed.	deflec-	heri net	Ship's head.	ıten	Ship's attrac-	Tempe-	Intensity.	Remarks.
1 .				aon.	T		H	tion.	rature.		
7045	ļ		**************************************								
1845. A pr. 19	. Swingin	ng the	Def. N.S.	45° 01	5 <u>9</u>	N.E.	1.691	012	-000	1.679 >1.683	Inton-it- b- D-C
11p1.13	ship for	r local	Def. N.S.	44 49	60	E.N.E.	1.702	022	.000	1.680	Intensity by Def. N.S. on shore
1	attrac		Def. N.S.	44 47	60	E.	1.705	032	.000	1.673	1.685.
	1		Def. N.S.	44 33	63	E.S.E.	1.723	041	001	1.681	
			Def. N.S.	44 20	63	S.E.	1.740	051	001	1.688	
l	1		Def. N.S.	44 14	63	S.S.E.	1.748	056	001	1.691	
]	Def. N.S.	44 11	63	s.	1.751	 061	001	1.689	
23	-35 36	114 44	Def. N.	23 57	64	N.W.	1.686	-012	•000	1.6747	
			Def. S.	24 47	64	N.W.	1.722	012	•000	1.710 >1.688	Table unsteady.
		1	Def. N.S.	45 00	64		1.692	012	001	1.679	
24	-34 16	113 01	Def. N.	24 40	67	n.w. by n.		012	001	1.630	
ł			Def. S.	25 37	69	n.w. by n.		012	001	1.661 >1.641	Table unsteady.
25	00.00		Def. N.S.	45 37	70	n.w. by n.		-012	002	1.633	
25	-32 32	111 36	Def. N.	25 02	67	N.w. by N.		008	001	1.614	
			Def. S. Def. N.S.	26 17 46 05	69	n.w. by n.	1.634	-·008	-·001	1.625 >1.613	Table unsteady.
27	90 90	106 55	Def. N.	25 07	70 72	w.n.w.	1.612	016	002	1.601	
~1	-29 20	100 55	Def. S.	27 32	72		1.566	016			Table steady.
ŀ			Def. N.S.	47 15	72		1.531	016	004	1.511	Table steady.
28	_27 47	106 36		27 17		N. by $w \cdot \frac{1}{2} w$.		.000	001	1.4967	·
_~~	7 ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		Def. S.	29 02		N. by $w.\frac{1}{2}w$.		.000		1.481 >1.490	Very unsteady,
	1	1	Def. N.S.	47 47	69	N. by $w \cdot \frac{1}{2} w$.		•000	003	1.494	heavy swell.
29	-2600	105 11	Def. N.	27 30	72	N.W.	1.486	005	 001	1.4807	
1			Def. S.	29 10	74	N.W.	1.474	005	001	1.468 >1.470	Very unsteady,
			Def. N.S.	48 12	75	N.W.	1.471	-005	 • 004	1.462	heavy swell.
May 1	-24 00	99 23	Def. N.	29 07	69	w.	1.396	021	 001	1.374)	
			Def. S.	31 00	69	ţ.	1.381	021	001	1.359 >1.367	Very unsteady,
			Def. N.S.	49 30	70	w.	1.393	021	003	1.369	much motion.
2	-24 01	97 30	Def. N.	29 02	70	$W \cdot \frac{1}{2} N \cdot$	1.410	017	001	1.392	
			Def. S. Def. N.S.	30 50	71	$W_{\bullet} \stackrel{1}{\stackrel{1}{2}} N_{\bullet}$	1.390	-·017 -·017	-·001 -·003	1.372 >1.379	Table steady, little motion.
3	_24 00	96 06		49 32 29 40	71 76	$W. \frac{1}{2} N.$ $W. \frac{1}{2} N.$	1·392 1·381	017	001	$\begin{pmatrix} 1.372 \\ 1.363 \end{pmatrix}$	motion.
ľ	-24 00	90 00	Def. S.	29 40 31 02	76	$\begin{array}{c} W \cdot \frac{1}{2} N \cdot \\ W \cdot \frac{1}{2} N \cdot \end{array}$	1.380	-017	001	1.362	
		1	Def. N.S.	50 15	77	$\begin{array}{c} W \cdot \frac{1}{2} N \cdot \\ W \cdot \frac{1}{2} N \cdot \end{array}$	1.350	017	004	1.300	
			wt. 1 gr.	15 02	77	$W \cdot \frac{1}{2} N$.	1.423		+.001	$\binom{1329}{1\cdot407}$ > 1·365	Table steady, no
	1		wt. 2 grs.	31 47	76	$W.\frac{1}{2}N.$	1.380	1 -		1.364	swell.
1			wt. $2\frac{1}{2}$ grs.	41 10	76	$W_{\bullet} \stackrel{1}{\stackrel{1}{2}} N_{\bullet}$	1.383	, -	+.001	1.367	
6	-22 47	91 00	Def. N.	30 57	76	N.W.	1.320			1.327	
	1		Def. S.	32 25	79	N.W.	1.315	+.008	002	1.321 >1.324	Very unsteady,
1			Def. N.S.	60 50	80	N.W.	1.321	+.008	005	1.324	heavy westerly swell.
7	-21 50	89 44		30 45	72	t	1.329		001		
I			Def. S.	32 15	74	N.W.	1.322		001		
			Def. N.S.	51 10	75	N.W.	1.308				
8	$-20 \ 46$	87 59		31 45	75	N.w. by w.				1.282	
-	1		Def. S.	32 20	76	N.w. by w.		+.004		1.321	
l		1	Def. N.S.	51 25	77	N.w. by w.		+.004	004	1 - 110004	W. Burdon, Esq.,
	Ì		Def. N.	32 00	78	N.w. by w.			-:002	1.2/0	R.N., observer.
I		1	Def. S. Def. N.S.	32 37 51 27	77	N.w. by w.			-·001 -·004	1.309	
	20 38	85 26		51 27 31 42	77	W. $\frac{1}{2}$ N.	1.286			1·291 J 1·271 \	1
1		1 00 20	Def. S.	33 02	77	$\begin{array}{c} W \cdot \frac{1}{2} N \cdot \\ W \cdot \frac{1}{2} N \cdot \end{array}$	1.286			1.271 >1.265	Very unsteady.
	1	1	Def. N.S.	51 50		$W \cdot \frac{1}{2} N \cdot$	1.270				heavy swell.
	<u> </u>	1	1	1	<u> </u>	1 2 2				1	<u> </u>

							T				T
1		1					<u>;</u>	Corre	ctions.		
1			Method	Angle of	Thermo- meter.		Intensity.	I	ı	Corrected	
Date.	Lat.	Long.	employed.	deflec-	ete	Ship's head.	en	Ship's	Tempe-	Intensity.	Remarks.
i . 1		-	employeu.	tion.	E a	_	l t	attrac-	rature.	intensity.	
								tion.	100000		
1845.	0 4	0 /		0 /	٥	_	ĺ				
May 10.	-20 26	82 22	Def. N.	31 37	77̈́	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.288	-014	001	1.273	1
1		1	Def. S.	33 15	78	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.277	-014	001	1.262	
			Def. N.S.	52 10	80	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.260	014	005	1.241	77 J.
1		1	Def. N.	31 35	75	$W \cdot \frac{1}{4} N \cdot$	1.289	016	001	$ \frac{1.272}{1.272}\rangle^{1.257}$	Very unsteady.
1			Def. S.	33 27	75	$W. \frac{1}{4} N.$	1.269	- ⋅016	001	1.252	W. Burdon, Esq.,
			Def. N.S.	52 07	74	$W_{\bullet} \stackrel{1}{\stackrel{1}{\stackrel{1}{\stackrel{1}{\stackrel{1}{\stackrel{1}{\stackrel{1}{1$	1.260	016	003	1.241	R.N., observer.
11.	-20 36	79 22	Def. N.	31 52	77	$W. \frac{1}{4} N.$	1.274	016	001	1.257	
1	-20 50	19 22	Def. S.	33 37			1 -	_·016	-·001	1 1	W D Fl.
1					77	$W_{\bullet} \frac{1}{4} N_{\bullet}$	1.262		}	1.245	W. Burdon, Esq., R.N., observer.
1.			Def. N.S.	52 07	78	$W_{\bullet} \frac{1}{4} N_{\bullet}$	1.260	016	005	1.239	Table unsteady.
			Def. N.	31 52	78	W. $\frac{1}{4}$ N.	1.274	016	002	1.250	
			Def. S.	33 40	77	$W_{\bullet} \frac{1}{4} N_{\bullet}$	1.260	016	002	1.242	
			Def. N.S.	52 00	78	$W_{\bullet} \frac{1}{4} N_{\bullet}$	1.262	016	005		
12.	-2044	78 31	Def. N.S.	52 17	84	w.	1.249	018	006	1.225	
4			Def. N.S.	52 20	86	w.n.w.	1.248	004	006	1.238	
			Def. N.S.	52 32	88	N.W.	1.239	+.008	006	1.241	
1			Def. N.S.	52 50	91	N.N.W.	1.226	+.006	008	1.224	
			Def. N.S.	51 20	80	s.	1.296	046	005		Table very unsteady,
			Def. N.S.	51 22	82	l	1.294	043	005	1.246	calm.
1			Def. N.S.	51 30		s.s.w.		_·037	005	1.245	
					82	s.w.	1.287		i	1 - 1	
l			Def. N.S.	51 55	83	w.s.w.	1.267	-026	005	1.236	
			Def. N.S.	52 25	82	N.N.E.	1.242	+.006	005	1.243	
13.	-20 39	77 43		52 42	77	w.	1.227	-018	-004	1.205	
1			Def. N.S.	52 15	77	N.W.	1.250	+.008	004	1.254	
l .			Def. N.S.	52 32	77	Ň.	1.239	+.008	004	1.243	Very unsteady ;
1.			Def. N.S.	52 22	77	N.E.	1.247	+.008	004	1.251	calm.
1			Def. N.S.	52 07	78	Е.	1.260	018	005	1.237	
Í			Def. N.S.	51 45	77	S.E.	1.275	037	004	1.234	
14.	-20 29	76 22	Def. N.	32 27	76	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.249	1 0	001	1.232	
1			Def. S.	33 52	76	$W \cdot \frac{1}{2} N$	1.252		001	1.235	
l			Def. N.S.	52 50	76	$W. \frac{1}{2} N.$	1.226	1	004	1.206	
i			Def. N.	33 20	76	$W \cdot \frac{1}{2} N$.	1.212	1 -	001	1.195	Very unsteady.
1			Def. S.	33 37	76	$W. \frac{1}{2} N.$	1.262	1 _	001	1.245	1
1			Def. N.S.	52 30			1.238			1.218	W. Burdon, Esq., R.N., observer.
16	00 00	70 46	;	1	75	$W \cdot \frac{1}{2} N \cdot$					Ti.Iv., Observer.
16.	-20 28	70 46		1 .	78	$W \cdot \frac{1}{4} N \cdot$	1.236	1	3	1.217	
I			Def. S.	34 05	78	$W \cdot \frac{1}{4} N \cdot$	1.200	1	002	1.181 >1.199	Table steady.
	0- 00	Co	Def. N.S.	52 55	78	W. $\frac{1}{4}$ N.	1.222	1	005	1.200	
18.	-21 06	68 12		32 57	80	w.s.w.	1.227		002	1.199	
1		1 .	Def. S.	34 37	80	w.s.w.	1.221	1	002	1.193 >1.191	Very unsteady.
			Def. N.S.	53 10	83	w.s.w.	1.212			1.181	
19.	-21 11	67 54	Def. N.	33 12	75	n.w. by n.		001		1.215	
1	1		Def. S.	34 45	76	N.w. by N.	1.215	 001	001	1.213	
1			Def. N.S.	53 10	75	N.W. by N.	1.212	001	004	1.207	,
1			wt. 1 gr.	18 00		N.W. by N.		001	+.001	1.197	
1			wt. 2 grs.	37 52		n.w. by n.	1.183		+.001	1.183 >1.203	Table steady, nearly
1			wt. $2\frac{1}{2}$ grs.	49 32		N.w. by N.	1.196			1.196	a calm.
1	1		Def. N.	33 37		n.w. by n.	1.202		_·001	1.200	
1	1		Def. S.	34 45	76		1.215	1	001	1.213	
1			Def. N.S.			N.W. by N.					W. Burdon, Esq.,
	01.10	C# 00		53 20	75	n.w. by n.	1.204			()	R.N., observer.
20.	-21 12	67 29		33 25	76	w. by N.	1.200			1.186	
			Def. S.	34 45		w. by N.	1.215			1.201	1
1	,		Def. N.S.	53 05	1	w. by n.	1.214	1		1.196	Table steady.
1			Def. N.	33 32	1	w. by N.	1.205			1.190	- word steady!
1			Def. S.	34 02		w. by N.	1.243				W. Burdon, Esq.,
1			Def. N.S.	52 55	81	w. by N.	1.223	-013	-005	1.205	R.N., observer.
*	I	1	1	1	1	1	1		1	1 -	1

Observations of the Magnetic Force. (Continued.)

								Corre	ctions.		
	_	7	Method	Angle of	Thermo- meter.		Intensity.			Corrected	
Date.	Lat.	Long.	employed.	deflec-	net	Ship's head.	ten	Ship's	Tempe-	Intensity.	Remarks.
				tion.	Ε.		1 1	attrac-	rature.		
		<u> </u>				<u> </u>					
1845.	-21°02	ငင္ငံ ဝင္ခံ	D.C.N	33° 40′	7 6		1.001	.012	.001	1.107	
May 21.	-21 UZ	00 02	Def. N. Def. S.	33 40 34 40	76 76	w. by n. w. by n.	1·201 1·216	_·013	001		
				53 15	76	w. by N.	1.201	-013		1.184	
	٠			18 22	76	w. by n.	1.175		+.001		Table steady.
'				37 37	76	w. by N.	1.191		+.001		
				50 20	76	w. by N.	1.182		+.001		
23.	$-20 \ 31$	59 42		33 47	77	w. by n.	1.194	013			
				35 30	77	w. by n.	1.185	1	001		Very unsteady.
/ 05	20.05			53 55	78	w. by n.	1.179	013	004		
27.				34 58	81		1.147		002	1 _ 1	
	Port I Mauri			35 52 55 32*	81 81	Observed	1·170 1·115	••••	002		Lieut. Moore,
	Maur	ittus.		19 01	81	on shore.	1.135		+.001		R.N., observer.
				38 12	81	-	1.175		+.001		
30.	-21 44	53 34		33 27	80	w.s.w. ½ w.		024			1
				34 40	82	$w.s.w. \frac{1}{2} w.$					Very unsteady.
				53 37	82	w.s.w. $\frac{1}{2}$ w.		-024	 ∙005	1.163	
June 2.	-26 25	49 12		34 27	79	n.w. by w.			002		
	.			35 47	79	n.w. by w.			002		Very unsteady.
	05.10	46 00		54 22	79	N.w. by w.		005	004		
4.	-27 12	40 09		34 45	68		1.156	024	001		Timetee du
		1		36 20 54 30	68 68		1·152 1·155	-·024 -·024	001		Unsteady.
5.	-28 24	43 00	I	34 55	74	w. by s. w.	1.150	-·020	_·001		
	~ ~ ~ ~	10 00		36 30	74	w.	1.145	020	001		Very unsteady.
	ĺ	1		54 45	76			020	 ·003		
6.	-28 44	42 01		35 47	73	w.n.w.	1.116	009	_ .001		
		. [Def. S.	36 55	76	w.n.w.	1.129	009	001		Very unsteady.
				54 55	78	w.n.w.	1.139	009	003		
7-	-28 35	40 24		34 47	73		1.156	017	- .001		
	1	. 1	Def. S.	36 40	74		1.138	017			Very unsteady.
8.	—28 57	37 59		54 47 35 42	74 72	W. ½ N. W.	1·145 1·120	-·017 -·020	003 001		
	-20 07	0, 02		37 47	76		1.095	-·020	001		
				55 10	78	1.	1.128	020	004	1.104	
	l	I		19 45	80		1.100	020	+.002	1.082 >1.094	Table steady, nearly calm.
	ł	1	wt. 2 grs.	40 30	80	l i	1.118	-020	+.002	1.100	.*
			wt. $2\frac{1}{2}$ grs.	53 57	82		1.125	020	+.002	1.107	
12.	-30 33	33 19		36 17	66		1.098		001		
	.			37 40	66			009			Table unsteady.
12	-31 06	21 94		56 15	65			009			
10.	-91 00	01 04		36 27 37 52	_ 1	w. by s. $\frac{1}{2}$ s.		-·026	001 001		Table steady.
l . I		-		56 32	1	w. by s. ½ s. w. by s. ½ s.		026	001		- ante areatif.
14.	-33 01	29 36		36 57	71		1.075	020	001		
- "				38 35	72		1.067	020	001		Table unsteady.
				56 57	73		1.062	020	 ·003	1.039	
15.	-34 31	27 04	Def. N.	36 40	74		1.085	014	001		
				38 42	76	· ·	1.063	014	 ·001	1.048	
	. [56 47	78		1.067		004		Table very unsteady,
				19 47	80	= 1	1.092	014	+.001	1013))	long heavy swell.
		. 1		45 02	80	~ 1	1.027	014	+.001	1.014	
			wt. 2½ grs.	00 01	82	W. $\frac{1}{2}$ N.	1.063	014	+.001	1.090)	_

^{*} Probably the degree is erroneous; the result is not included in the mean.

[†] Not included.

Observations of the Magnetic Force. (Continued.)

					<u>.</u>	·	y.	Correc	ctions.		
Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.	Thermo- meter.	Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected Intensity.	Remarks.
1845.				-						PROPERTY OF THE PROPERTY OF TH	
June 16.	$-3\mathring{5} \ 4\acute{6}$	23 35	Def. N.	38 0Ó	7 Š	w. by n.	1.042	012	001	1.029	
			Def. S.	39 17	77	w. by n.	1.043	012	001	1.030 >1.033	Table steady.
			Def. N.S.	57 02	78	w. by n.	1.057	012	004	1.041	
17.	-35 36	21 40	Def. N.	38 45	67	W.N.W.	1.020	 007	 ·001	1.012	
1			Def. S.	39 47	67	W.N.W.	1.026	007	001		Table steady.
			Def. N.S.	57 12	67	W.N.W.	1.053	 007	001	1.045	
18.	-35 07	20 46	Def. N.	38 22	64		1.031	019	.000	1.012	
			Def. S.	39 50	63		1.024	019	.000	1.005 >1.013	Table steady, nearly calm.
600	0.4 - 0		Def. N.S.	57 30	63		1.042	019	001	1.022	
23.	-34 12		Def. N.S.	57 01	62	S.	1.060	040	.000	1.020	
	At anc		Def. N.S.	57 08	66		1.056	037	001	1.018	
ĺ	Simon'	s Bay.	Def. N.S.	57 29	68	s.w.	1.042	-·031 -·022	001	1.010	
			Def. N.S.	57 52	68	w.s.w.	1.030		002	1.007	
			Def. N.S.	58 07	70	w.	1·021 1·019	-·014 -·003	002	1.005	
	_		Def. N.S.	58 11	70		1.020	-·002	002	1.014	
			Def. N.S.	58 07	82	N.W.	1.020	-000	$\begin{bmatrix}004 \\004 \end{bmatrix}$	1.014	
			Def. N.S.	58 16 58 09	82 83	N.N.W.	1.020	+.002	004	$\begin{vmatrix} 1.014 \\ 1.017 \end{vmatrix} > 1.012$	Swinging ship for
			Def. N.S.	58 10	84	N.	1.020	+ 002	005	1.017	local attraction.
			Def. N.S.	58 09	85	N.N.E.	1.020	002	005	1.013	
			Def. N.S. Def. N.S.	58 07	85	N.E.	1.021	002	005	1.013	
			Def. N.S.	57 58	86	E.N.E.	1.026	014	005	1.007	
			Def. N.S.	57 53	87	E.S.E.	1.030	022	005	1.003	
	,		Def. N.S.	57 30	88	S.E.	1.042	031	006	1.005	
			Def. N.S.	57 10	90	S.S.E.	1.055		006	1.012	
			Def. N.S.	58 08	68	On shore.	1.021		001	1.020	In the Dock Yard.
30.	-33 56	18 90	Def. N.	39 31	59	Sin sinoite.	0.992			0.992	
	35 50	10 29	Def. S.	40 39	61		1.000			1.000	
			Def. N.S.	58 16	62		1.016			1.016	
			wt. 1 gr.	21 38	63		1.004			1.004	
3			wt. 2 grs.	46 31	64	11	1.001			1.001	
			wt. $2\frac{1}{2}$ grs.	65 30	65	Observed	0.999			0.999 >1.001	
July 2	Magnet	tic Ob-	Def. N.	39 22	59	on shore.	0.997			0.997	
and and and and and and and and and and	servator		Def. S.	40 39	60		1.000			1.000	1
1	of Good		Def. N.S.	58 21	61		1.013			1.013	
			wt. 1 gr.	22 06	63		0.986			0.986	
			wt. 2 grs.	46 21	64.		1.004			1.004	
		1	wt. 2½ grs.	65 30	64	IJ	0.999			0.999	-
			1 ~ 0	<u> </u>							1

General Table of the Declinations observed on board Her Majesty's hired Bark "Pagoda."

			No of					No. of	
Date.	Lat.	Long.	No. of observations.	Declination.	Date.	Lat.	Long.	observations.	Declination.
1845. Jan. 10. 11. 12. 13. 15. 16. 17. 19. 20. 22. 23. 24. 25. 26. 27. 29. 31. Feb. 1. 12. 13. 14. 16. 17. 18. 19. 20. 21. 22. 25. 26. 27. 28. March 1. 22. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 16. 17. 18. 19. 20. 21. 22. 25. 26. 27. 28. March 1. 20. 21. 22. 25. 26. 27. 28. March 1. 12. 13. 14. 15. 16. 17. 18. 20. 21. 22. 25. 26. 27. 28. March 1. 22. 25. 26. 27. 28. 28. March 1. 29. 20. 21. 22. 25. 26. 27. 28. 28. 29. 20. 20. 20. 20. 20. 20. 20. 20. 20. 20	-34 42 -35 26 -35 17 -35 10 -38 43 -39 18 -40 24 -46 24 -46 24 -46 27 -51 47 -52 56 -53 52 -55 52 -55 52 -61 12 -62 05 -61 54 -62 05 -63 18 -64 52 -63 67 54 -67 06 -67 52 -63 52 -63 52 -63 43 -61 18 -61 23 -61 16 -60 46 -60 93 -58 30 -58 30 -58 30 -58 30 -58 30 -58 45 -59 05 -48 59 -48 59 -48 59 -48 40 -41 02 -88 40	17 36 15 08 14 00 13 25 14 28 14 28 14 35 13 19 13 34 10 51 10 51	4 4 3 3 1 11 11 4 3 4 8 17 4 10 4 8 27 9 6 9 9 11 3 5 7 3 5 2 6 6 6 4 7 1 1 1 1 7 7 1 7 1 7 1 7 1 7 1 7 1 7	+29 51 +28 39 +27 15 +25 40 +25 99 +27 40 +26 34 +25 54 +26 34 +21 33 46 +21 33 47 +23 55 +23 55 +23 55 +23 57 +23 11 +26 16 +28 56 +31 37 43 +37 43 +37 43 +37 43 +37 43 +37 43 +37 34 +36 59 +37 34 +36 59 +37 34 +37 34 +36 59 +37 34 +37 37 +45 51 +46 01 +45 51 +47 47 +49 02 +48 01 +47 47 +49 02 +49 02 +49 02 +49 03 +41 03 +41 03 +41 03 +41 03 +41 03 +41 03 +42 15 +43 15 +44 10 +45 17 +45 51 +47 47 +49 02 +48 01 +47 47 +49 02 +49 02 +49 02 +49 03 +41 03 +43 03 +43 03 +44 03 +44 03 +45 03 +46 01 +47 47 +47 47 +49 02 +48 01 +47 63 +48 01 +46 01 +46 01 +46 01 +47 63 +47 04 +47 05 +47 04 +47 05 +47 04 +47 04 +47 05 +47	1845. March 28. 29. 30. 31. April 11. 14. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. May 1. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 30. June 1. 24. 27. 29. 30. 31. June 1. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. 27. 29. 30. 30. 31. June 1. 22. 23. 24. 27. 29. 30. 31. June 1. 22. 23. 24. 27. 29. 30. 31. June 1. 22. 23. 24. 27. 29. 30. 31. June 1. 22. 23. 24. 27. 29. 30. 31. June 1. 22. 23. 24. 27. 29. 30. 31. June 1. 22. 23. 24. 27. 29. 30. 31. June 2. 24. 27. 29. 30. 31. June 1. 22. 23. 24. 27. 29. 30. 31. June 2. 24. 27. 29. 30. 30. 31. June 2. 24. 27. 29. 30. 30. 31. June 2. 24. 27. 29. 30. 30. 31. June 2. 24. 27. 29. 30. 30. 31. June 2. 24. 27. 29. 30. 30. 31. June 2. 24. 27. 29. 30. 30. 31. June 2. 24. 27. 29. 30. 30. 31. June 2. 24. 27. 29. 30. 30. 31. June 2. 24. 27. 29. 30. 30. 31. June 2. 24. 25. 66. 77. 88. 99. 91. 91. 92. 92. 92. 92. 92. 92. 92. 92. 92. 92	-36 51 -36 10 -35 12 -35 28 -35 02 -35 10 -35 33 -34 18 -35 32 -35 33 -34 18 -32 42 -30 25 -29 20 -27 41 -24 07 -23 58 -24 07 -23 58 -24 17 -24 05 -22 46 -21 53 -20 36 -20 37 -20 25 -20 36 -20 34 -20 39 -20 28 -20 27 -20 34 -20 39 -20 28 -21 11 -21 12 -21 01 -20 39 -20 39 -20 30 -21 54 -20 39 -20 30 -21 54 -21 54 -23 44 -25 47 -26 30 -27 12 -28 19 -28 49 -28 36 -28 19 -28 49 -28 36 -36 30 -37 30 -3	116 36 116 43 117 41 117 04 117 56 118 06 115 40 114 42 113 12 111 43 109 07 106 55 106 35 105 16 102 28 99 21 97 346 94 06 92 11 90 40 88 06 85 32 82 32 79 20 78 34 77 45 76 23 73 20 70 49 66 24 67 29 68 12 67 55 57 31 55 30 51 48 49 40 49 20 40 14 37 45 57 31 55 32 53 34 55 32 57 34 68 53 73 20 70 49 69 37 68 12 67 54 68 24 69 37 68 12 67 54 68 24 69 37 68 12 67 29 68 31 59 40 69 37 68 55 32 32 53 30 53 42 55 30 51 48 49 40 49 20 40 14 37 40 14 38 31 31 31 31 31 31 31 31 31 31 31 31 32 40 12 33 35 21 37 40 20 24 19 33 18 27	3851 3 113454223244641925357213312225323122432353457261949521236	$\begin{array}{c} 4 & 31 \\ 2 & 4 & 52 \\ 2 & 55 \\ 3 & 4 \\ 4 & 52 \\ 2 & 55 \\ 4 & 5 \\ 5 & 57 \\ 5 & 51 \\ 4 & 6 \\ 6 & 36 \\ 6 & 20 \\ 6 & 30 \\ 3 & 30 \\ 2 & 4 \\ 6 & 36 \\ 6 & 30 \\ 6 & 20 \\ 6 & 30 \\ 6 & 30 \\ 6 & 20 \\ 6 & 30 \\ 6 & 20 \\ 7 \\ 7 \\ 8 & 20 \\ 7 \\ 8 & 20 \\ 8 \\ 8 & 20 \\ 8 \\ 8 & 20 \\ 8 \\ 8 & 20 \\ 8 \\ 8 & 20 \\ 8 \\ 8 & 20 \\ 8 \\ 8 & 20 \\ 8 \\ 8 & 20 \\ 8 \\ 8 \\ 8 & 20 \\ 8 \\ 8 \\ 8 \\ 8 \\ 8 \\ 8 \\ 8 \\ 8 \\ 8 \\ $

^{*} On shore at King George's Sound.

[†] On shore at Port Louis, Mauritius.

General Table of the Inclinations observed on board Her Majesty's hired Bark "Pagoda."

-					ľ				Y 1'		
Date.	Lat.	Long.	Inclina		Mean.	Date.	Lat.	Long.	Inclinat		Mean.
			Fox, F. 1.	Fox, C. 9.		~			Fox, F. 1.	Fox, C. 9.	
11 13 14 15 16	-33 56 -34 12 -34 14 -34 45 -35 29 -35 17 -35 18 -37 25 -38 40 -40 31 -42 50 -44 50 -49 01 -48 35 -50 39 -51 49 -53 07 -55 13 -60 43 -61 10 -62 06 -61 55 -61 50 -62 30 -63 19 -64 23 -65 37 -66 27 -66 33 -66 57 -67 37 -67 02 -66 58 -64 48 -64 52 -64 48 -64 52 -64 48 -64 52 -64 48 -64 52 -64 48 -64 52 -64 48 -64 52 -64 48 -64 52 -64 48 -64 52 -64 48 -64 52 -64 48 -64 52 -64 48 -64 52 -64 48 -64 52 -64 48 -64 52 -64 48 -64 52 -65 36 -61 19 -61 05 -61 19 -61 05 -61 10 -62 44 -64 20 -61 40 -63 36 -62 36 -61 19 -61 05 -61 43 -62 44 -64 52 -64 52 -65 56 -61 50 -65 56 -61 50 -61 50 -62 44 -64 52 -63 56 -6	18 29 18 29 18 29 18 26 18 32 17 48 32 17 48 32 17 49 40 13 26 13 26 13 27 14 40 14 23 13 09 11 28 10 51 10 22 9 7 43 6 05 5 5 5 5 4 00 9 05 12 52 16 30 9 05 17 6 05 18 40 19 14 10 40 10 40 10 40 10 53 10 54 10 55 10 56 10 -53 31 -53 31 -53 30 -53 39 -52 56 * -51 35 -51 35 -52 56 * -51 35 -52 56 -53 39 -54 14 -55 10 -55 10 -56 14 -57 02 -57 03 -57 01 -57 26 -57 03 -57 01 -57 26 -63 35 -64 55 -64 55 -68 16 -69 22 -69 49 -70 12 -69 39 -68 40 -69 36 -70 03 -70 02 -72 01 -73 27 -74 02 -74 02 -74 02 -74 03 -77 35 -77 35 -78 42‡ -77 35 -78 49 -78 59 -78 49	-7741	\begin{array}{c} -53 & 31* \\ -53 & 30* \\ -53 & 50† \\ -53 & 15 \\ -51 & 27 \\ -51 & 16 \\ -51 & 27 \\ -51 & 16 \\ -55 & 53 \\ -55 & 54 \\ 13 \\ -55 & 05 \\ -56 & 14 \\ -57 & 39 \\ -57 & 14 \\ -57 & 49 \\ -57 & 57 \\ 14 \\ -57 & 49 \\ -63 & 17 \\ -63 & 17 \\ -63 & 17 \\ -63 & 17 \\ -63 & 17 \\ -64 & 20 \\ -64 & 40 \\ -65 & 35 \\ -66 & 41 \\ -67 & 61 \\ 30 \\ -67 & 28 \\ -68 & 31 \\ -68 & 49 \\ -69 & 38 \\ -70 & 16 \\ -69 & 35 \\ -69 & 13 \\ -70 & 08 \\ -69 & 13 \\ -70 & 09 \\ -70 & 08 \\ -71 & 44 \\ -72 & 53 \\ -73 & 50 \\ -74 & 38 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -77 & 37 \\ -78 & 20 \\ -78 & 31 \\ -79 & 31 \\ -78 & 31 \\ -79	1845. March 18. 19. 20. 222. 244. 255. 266. 27. 28. 299. 300. April 7. 11. 12. 20. 23. 244. 255. 277. 28. 299. May 1, 2. 3. 44. 55. 66. 77. 88. 99. 100. 111. 122. 133. 144. 166. 177. 188. 199. 200. 211. 222. 233. 247. 300. June 2. 33. 44. 55. 66. 77. 88. 11. 12. 13. 14. 155. 166. 77. 88. 111. 122. 133. 144. 155. 166. 77. 88. 111. 122. 133. 144. 155. 166. 77. 88. 111. 121. 138. 149. 240. 251. 252. 253. 277. 300. June 12. 233. 241. 253. 354. 455. 66. 77. 88. 811. 112. 113. 114. 115. 115. 116. 117. 118. 233. Magnetic Obegood Hopulith of Julith	servatory, e, on the	Cape of	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	- 77 39 / - 77 36 / - 76 32 / - 77 36 / - 76 32 / - 77 36 / - 77 32 / - 77 36 / - 77 32 / - 77 36 / - 77 36 / - 77 36 / - 77 36 / - 77 36 / - 77 36 / - 77 36 / - 77 36 / - 77 36 / - 77 36 / - 77 36 / - 68 21 / - 66 21 / - 66 21 / - 66 21 / - 66 21 / - 66 21 / - 66 21 / - 66 21 / - 66 21 / - 66 21 / - 66 21 / - 66 21 / - 66 21 / - 66 21 / - 66 21 / - 67 30 / - 67 30 / - 67 30 / - 67 30 / - 57 3	-77 34 -77 09 -76 17 -75 32 -72 28 -70 43 -68 27 -66 38 -65 36 -65 36 -65 14 -65 51 -65 51 -65 51 -65 51 -65 14 -65 51 -65 11 -64 44 -62 18 -59 22 -51 22 -51 15 -51 12 -51 15 -51 12 -51 22 -51 20 -52 49 -52 01 -51 15 -51 12 -51 22 -51 30 -53 36 -53 36 -53 36 -53 36 -58 38 -58 38 -59 01 -57 06 -58 38 -58 37 -57 06 -58 37 -57 06 -58 37 -57 06 -58 37 -57 06 -58 37 -57 06 -58 37 -57 39 -57 39	

^{*} Magnetic Observatory, Cape of Good Hope.

[‡] Probably a wrong degree; omitted in the mean.

[|] King George's Sound.

[†] Dock Yard, Simon's Bay.

[§] Needle A. ¶ Needle B.

^{**} Port Louis, Mauritius.

General Table of the Intensities of the Magnetic Force observed on board Her Majesty's hired Bark "Pagoda."

			Inter	isity.					Inter	isity.	
Date.	Lat.	Long.	Fox, F. 1.	Fox, C. 9.	Mean.	Date.	Lat.	Long.	Fox, F. 1.	Fox, C. 9.	Mean.
Dec. 1 and 5. 21.	-33 56 -34 12	18 29 18 26	0·999* 1·005†		0·999 1·005	1845. March 19. 20.	-51 10 -48 59	111 26 112 22	1·787 1·798	1.821	1·787 1·810
1845. January 10.	-34 45	17 48	0.981	0.985	0.983	$egin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{vmatrix} -47 & 21 \\ -45 & 08 \end{vmatrix}$	115 15 116 50	1.825	1.842	1·834 1·820
11. 12.	$-35 29 \\ -35 17$	15 09 14 00	•••••	0.968 0.923	$0.968 \\ 0.923$	25.	$ \begin{array}{r rrrr} -43 & 21 \\ -41 & 09 \end{array} $	116 50	1·760 1·746	1.804 1.758	1.782
13.	-35 18	13 26	0.950	0.933	0.942	26. 27.	-38 46	116 26 116 15	1.738	1.722	1·752 1 730
14. 15.	$\begin{vmatrix} -37 & 25 \\ -38 & 40 \end{vmatrix}$	$13 24 \\ 14 27$	0.965 1.008	0.978	0·965 0·993	28.	-37 02	116 57	1.695	1.677	1.686
16.	-39 10	14 40	0.989	0.964	0.977	29. 30.	$\begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	116 49 117 18	1·673 1·702	1.670 1.694	1.672 1.698
17. 18.	$-40 \ 31 \\ -42 \ 50$	$\begin{array}{ccc} 14 & 23 \\ 13 & 00 \end{array}$	0.994	0.984	0·989 0·997	April 7.	-35 02	117 56	1.688	1.688]
19.	-42 50 $-44 50$	13 19	0·997 1·007		1.007	11. 12.	$ \begin{array}{c cccc} -35 & 02 \\ -35 & 05 \end{array} $	117 56 117 56	1.688	1.688	1.688§
21.	-49 01	11 28	1.051	1.051	1.051	23.	-35 33	114 40	1.688	1.672	1.680
22. 23.	$-48 \ 35 \ -50 \ 39$	$10 51 \\ 10 22$	1·060 1·094	1.093	$1.060 \\ 1.094$	24. 25.	$\begin{vmatrix} -34 & 16 \\ -32 & 28 \end{vmatrix}$	113 01 111 31	1.641 1.613	1.573	$1.641 \\ 1.593$
24.	-51 49	9 33	1.120	1.109	1.115	27.	-29 18	106 52	1.553	1.499	1.526
25. 26.	$-53 07 \\ -53 57$	7 43 6 05	1·122 1·143	1·134 1·141	1·128 1·142	28. 29.	$\begin{vmatrix} -27 & 41 \\ -25 & 53 \end{vmatrix}$	106 34 105 03	1·490 1·470	1·478 1·447	1·484 1·459
27.	-55 13	5 53	1.161	1.143	1.152	May 1.	-23 59	99 15	1.367	1.381	1.374
30. 31.	$-60 \ 43$ $-61 \ 10$	4 00 9 05	1·240 1·285	1.288	$1.240 \\ 1.287$	2.	-24 01	97 28	1.379	1.381	1.380
February 1.		12 52		1.349	1.349	3. 4.	$ \begin{array}{r rrrr} -23 & 55 \\ -24 & 17 \end{array} $	96 01 93 50	1.365	$\begin{array}{c c} 1.377 \\ 1.352 \end{array}$	1·371 1·352
2. 3.	$-61 55 \\ -61 50$	16 30	1.331	1.321	1.326	5.	-24 02	92 07		1.367	1.367
4.	$-62 \ 30$	$\frac{19}{20} \frac{14}{33}$	1·334 1·353	1.347	1·334 1·350	6. 7.	$\begin{vmatrix} -22 & 47 \\ -21 & 47 \end{vmatrix}$	91 00 89 41	1·324 1·326	1.314	$1.324 \\ 1.320$
5.	-63 19	21 48	1.401	1.362	1.362	8.	-20 42	87 55	1.294	1.298	1.296
6. 7.	$-64 23 \\ -65 37$	$\frac{24}{28} \frac{12}{39}$	1·401 1·432	1·398 1·432	$1.400 \\ 1.432$	9. 10.	$\begin{bmatrix} -20 & 38 \\ -20 & 26 \end{bmatrix}$	85 14 82 11	1·265 1·257	1·263 1·248	$1.264 \\ 1.253$
8.	-66 27	30 45	•••••	1.448	1.448	11.	$\begin{bmatrix} -20 & 20 \\ -20 & 36 \end{bmatrix}$	79 16	1.247	1.213	1.230
9. 10.	$-66 33 \\ -66 57$	$\frac{36}{38} \frac{48}{50}$	1·482 1·491	1·47() 1·483	1·476 1·487	12.	-20 44	78 31	1.238	1·234 1·233	1·236 1·235
11.	-67 37	40 00	1.519	1.496	1.508	13. 14.	$\begin{bmatrix} -20 & 39 \\ -20 & 29 \end{bmatrix}$	77 43 76 22	1·237 1·222	1 200	1.222
12. 13.	$-67 02 \\ -66 58$	$\frac{39}{40} \frac{53}{12}$	1·494 1·499	1·496 1·490	1·495 1·495	16.	$-20 \ 27$	70 41	1.199	1.205	1.202
14.	-6624	40 01		1.494	1.494	17. 18.	$ \begin{array}{r rrrr} -20 & 34 \\ -21 & 07 \end{array} $	69 24 68 08	1.191	1.210	1·210 1·191
16. 17.	$ \begin{array}{r rrr} -64 & 52 \\ -64 & 48 \end{array} $	38 37 40 12	1·470 1·463	1·450 1·482	1.460	19.	-21 11	67 54	1.203	1.206	1.205
18.	-64 22	40 49	1.460	1.402	1·473 1·460	20. 21.	$\begin{bmatrix} -21 & 12 \\ -21 & 02 \end{bmatrix}$	67 29 66 26	1·201 1·181	1·190 1·178	1·196 1·180
19.	-63 56	41 35	1.416	1.453	1.434	22.	-20 40	62 58		1.173	1.173
$\frac{20.}{21.}$	$ \begin{array}{r} -63 & 20 \\ -63 & 36 \end{array} $	$\begin{array}{c} 45 & 44 \\ 46 & 46 \end{array}$	1·437 1·457	$1.462 \\ 1.470$	1·450 1·464	23. 27.	$\begin{bmatrix} -20 & 31 \\ -20 & 09 \end{bmatrix}$	59 42 57 31	1·171 1·156	1.156	1·171 1·156
24.	$-62 \ 36$	51 40	1.466	••••	1.466	30.	-21 47	53 30	1.179	1.161	1.170
25. 26.	$-61 30 \\ -61 19$	53 44 57 34	1·476 1·535	1·498 1·506	1·487 1·521	June 2. 3.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	49 12	1.160	1.164	1.160
27.	-61 05	64 12	1.553	1.560	1.557	4.	$-20 \ 20$ $-27 \ 13$	48 20 46 00	1.129	1·164 1·159	1·164 1·144
28. March 1.	$ \begin{array}{r r} -61 & 43 \\ -62 & 10 \end{array} $	$71 08 \\ 72 25$	1·604 1·657	1.605 1.642	1.605 1.650	5.	-28 13	42 50	1.125		1.125
2.	-6244	76 12	1.656	1.653	1.655	6. 7.	$-28 44 \\ -28 35$	$\begin{array}{ c c c c c }\hline 42 & 01 \\ 40 & 24 \\ \hline \end{array}$	1·117 1·128		1·117 1·128
3. 5.	-64 20 61 40	79 38 84 54	1.706	1.678	1.692	8.	-28 57	37 49	1.094	1.111	1.103
6.	$-60 \ 45$	88 23	1.689 1.729	1·730 1·747	1·710 1·738	11. 12.	-30 33	33 41 33 19	1.085	1.105	1·105 1·085
7. 8.	$ \begin{array}{rrr} -61 & 22 \\ -61 & 10 \end{array} $	91 14	1.759	1.749	1.754	13.	-31 06	31 30	1.061	1.063	1.062
9.	$-60 \ 33$	92 07 92 30	1·762 1·745	1·758 1·750	1·760 1·748	14. 15.	-33 01 $-34 31$	29 36 27 04	1·046 1·059		1.046 1.059
10.	-60 03	95 50	1.798	1.770	1.784	16.	$-35 \ 46$	23 35	1.033	•••••	1.033
11. 13.		99 40 99 23	1.772 1.968‡	1.836 1.813	1·804 1·813	17. 18.	-35 38	21 40 20 46	1·025 1·013	1.033	1·029 1·013
14.	-56 55	101 30	1.786	1.802	1.794	23.	$ -34 \ 12$	18 26	1 012	1.001	1.0079
15. 16.	-54 43	103 12 106 10	1.816 1.801	1.815 1.817	1·816 1·809	Magnetic Ob Good Hope, 2	servatory,	Cape of	} 1.001	1.000	1.000
1 7 .	-54 14	108 10	1.816	1.821	1.819	Good Hope, 2	na ana 11t	n or July.	J		
18.	-53 00	110 22	1.814	1.825	1.820						

^{*} Observed on shore, Magnetic Observatory, Cape of Good Hope.

[†] Observed on shore, Dock-yard, Simon's Bay.

[‡] Not included in the mean.

[§] King George's Sound; observed on shore.

^{||} Port Louis, Mauritius; observed on shore.

[¶] Simon's Bay, on board.

Observations of the Magnetic Inclination between the Cape of Good Hope and Van Diemen Island, by Lieut. Alexander Smith, R.N.

Date.	Lat.	Long.	Corrected Inclination.	Date.	Lat.	Long.	Corrected Inclination.
1844. July 29. 30. 31. August 1. 2. 4. 5. 6. 7. 8. 9. 10. 11. 13. 14. 15. 16. 17. 18.	-38 00 -38 28 -39 06 -39 42 -39 33 -39 33 -39 50 -40 01 -40 32 -41 06 -41 00 -40 43 -40 56 -39 34 -39 00 -38 31 -38 22 -38 08 -38 10	4 20 7 45 12 00 15 44 23 05 26 52 28 36 32 22 36 40 41 40 46 13 49 12 53 30 60 55 65 44 68 45 70 10 73 35 75 22	-52 00 -53 03 -55 42 -57 06 -59 32 -61 47 -62 08 -62 56 -64 09 -64 42 -65 19 -66 08 -67 27 -67 18 -67 19 -66 45 -67 06 -66 45 -66 42	1844. Aug. 20. 21. 22. 23. 24. 25. 26. 27. 28. 30. 31. Sept. 1. 2. 3. 4. 5. 6.	-38 25 -38 48 -39 04 -39 58 -40 06 -40 02 -39 52 -39 54 -40 08 -40 31 -41 16 -41 54 -41 58 -42 17 -42 35 -43 00 -43 16 -43 28 -44 06	76 44 77 50 79 45 84 00 87 00 90 52 95 10 99 22 102 00 105 55 109 06 113 25 117 40 119 00 122 30 125 40 129 36 133 44 137 10 141 37	$\begin{array}{c} -6\mathring{6} & 5\mathring{4} \\ -67 & 14 \\ -67 & 17 \\ -67 & 43 \\ -68 & 13 \\ -68 & 41 \\ -69 & 08 \\ -69 & 00 \\ -69 & 22 \\ -70 & 02 \\ -70 & 02 \\ -70 & 30 \\ -71 & 20 \\ -71 & 33 \\ -71 & 45 \\ -72 & 08 \\ -72 & 13 \\ -71 & 55 \\ -72 & 14 \\ \end{array}$

Observations of the Magnetic Force between the Cape of Good Hope and Van Diemen Island, by Lieut. Alexander Smith, R.N.

Date.	Lat.	Long.	Method employed.	Angle of deflection.	Thermo- meter.	Ship's head.	Intensity. Hobarton = 1.800 .	Remarks.
1844. July 30.	$-38\ 28$	2 [°] 7 45	wt. 2 grs.	20° 13′	5°2	S.E. ½ E.	0.953 0.953	
Aug. 5.	-39 50	28 36	wt. 2 grs.	17 04	60	s.e. by e.	$1.121 \} 1.117$	
	-3950	$\begin{array}{c} 28 & 36 \\ 46 & 13 \end{array}$	wt. 3 grs.	26 35	59 60	s.e. by e.	1.119]	
9.	$-41 00 \\ -41 00$	46 13 46 13	wt. 2 grs. wt. 3 grs.	$\begin{array}{cc} 14 & 50 \\ 22 & 46 \end{array}$	61	E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S.	$\left\{\begin{array}{c} 1.288 \\ 1.289 \end{array}\right\}$ 1.288	
15.	-39 00	$\begin{array}{c} 40 & 13 \\ 65 & 44 \end{array}$	wt. 2 grs.	13 35	47	s.e. by e.	1.4031	
	-39 00	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	wt. 3 grs.	21 26	44	s.e. by e.	1.364 1.383	Much motion.
18.	-38 08	73 35	wt. 2 grs.	12 57	58	E.	1.471 1.454	Smooth water.
	-38 08	73 35	wt. 3 grs.	20 18	59	Ε.	1.437	
19.	$-38\ 10$	75 22	wt. 2 grs.	13 28	66	S.E. \(\frac{1}{2}\) E.	$\{\begin{array}{c} 1.415 \\ 1.450 \\ \end{array}\} 1.435$	Smooth.
24.	-38 10 $-40 06$	75 22 87 00	wt. 3 grs. wt. 2 grs.	20 02 12 14	66 64	S.E. ½ E.	1.456 1.555	
24.	-40 06	87 00 87 00	wt. 2 grs. wt. 3 grs.	17 42	60	E.S.E.	$\begin{array}{c c} 1.333 \\ 1.640 \end{array}$ 1.597	
28.	-39 54	102 00	wt. 2 grs.	11 13	51	E.S.E.	1.6045	
	-39 54	102 00	wt. 3 grs.	16 31	51	E.S.E.	$\begin{vmatrix} 1.094 \\ 1.754 \end{vmatrix} 1.724$	
30.	$-40 \ 31$	109 06	wt. 2 grs.	11 04	58	E.S.E.	1.717 1 1.751	
1	$-40 \ 31$	109 06	wt. 3 grs.	16 14	59	E.S.E.	1.789]	
Sept 3.	$-42 \ 35$	125 40	wt. 2 grs.	10 04	56	E. by s.	1.886 } 1.894	
_	$-42 \ 35$	125 40	wt. 3 grs.	15 12 10 21	55	E. by s.	1.834	·
5.	$\begin{vmatrix} -43 & 14 \\ -43 & 14 \end{vmatrix}$	$133 22 \\ 133 22$	wt. 2 grs. wt. 3 grs.	15 11	49	E. by s.	1.904	
6.	$-43 \ 28$	137 10	wt. 2 grs.	10 06	51	E. by S. E. $\frac{1}{2}$ S.	1.0705	
	-43 28	137 10	wt. 3 grs.	15 36	51	E. ½ S.	$\begin{vmatrix} 1.879 \\ 1.854 \end{vmatrix}$ 1.866	
Oct. 2.	-4252	147 24	wt. 2 grs.	10 33	54	On shore.	1.800 1.800	Hobarton: Magnetic
	-42 52	147 24	wt. 3 grs.	16 05	54	I Shore.	1.800	Observatory.

Hobarton is taken as the base station; no correction has been applied for the effect of the ship's iron. In the results entered in the map of the Magnetic Force from Lieut. SMITH's observations on the 24th, 28th, and 30th of August, the determinations with 2 grains only have been used; those with 3 grains are so discordant with other results as necessarily to indicate an error in them.

Observations of the Magnetic Inclination between Van Diemen Island and the Cape of Good Hope, by Lieut. Joseph Dayman, R.N.

Date.	Lat.	Long.	Corrected Inclination.	Date.	Lat.	Long.	Corrected Inclination.
1844. Dec. 6. 16. 17. 18. 19. 20. 21. 23. 24. 26. 27. 28. 30. 31. 1845. Jan. 1. 2. 3. 4. 6. 7. 9. 10. 11, 13. 14. 15. 16. 17. 18. 20. 21. 22. 23. 24.	Hobarton O -44 48 -44 30 -44 34 -44 34 -43 21 -42 24 -41 46 -42 02 -41 24 -42 08 -40 05 -38 21 -37 52 -37 14 -37 13 -36 28 -35 22 -36 42 -36 58 -36 96 -36 24 -37 00 -35 46 -36 24 -37 00 -35 46 -36 24 -37 00 -35 46 -36 24 -37 00 -35 46 -36 24 -37 00 -35 46 -36 42 -37 00 -35 46 -36 42 -37 00 -35 46 -36 42 -37 00 -35 46 -36 44 -37 00 -35 46 -36 44 -37 00 -38 47 -32 37 -29 40 -28 04 -26 44 -25 52 -24 50	0 /	Trelination.	1845. Jan. 25. 27. 28. 29. 30. 31. Feb. 1. 5. 6. 7. 8. 10. 11. 12. 13. 14. 15. 17. 18. 19. 20. 21. 22. 24. 25. 26. 27. 28. March 1. 3. 4. 5.	-24 00 -23 11 -22 54 -22 19 -22 17 -22 11 -22 08 -22 34 -22 35 -22 38 -22 38 -22 38 -22 41 -23 52 -24 23 -24 50 -24 43 -24 45 -25 13 -25 42 -26 54 -28 15 -29 21 -30 10 -31 19 -32 17 -34 02 -34 35 -34 36 -34 40 -34 29 -34 48	99 33 95 40 93 48 91 16 89 57 86 30 84 17 80 10 78 08 76 10 74 18 72 00 69 54 64 59 62 54 61 11 59 46 58 37 57 03 51 29 49 06 45 47 42 18 39 06 36 17 32 21 29 34 26 53 25 31 25 23 24 16 22 45 21 44 19 33	-54 20 -53 44 -53 26 -53 11 -53 11 -53 11 -53 52 -54 26 -54 26 -54 26 -54 41 -55 04 -55 54 -56 52 -57 57 -58 15 -57 59 -58 17 -59 13 -58 34 -58 34 -58 34 -59 37 -60 01 -59 08 -58 32 -56 45 -56 32 -56 35 -56 32 -56 32 -56 35 -56 32 -56 35 -56 35 -56 35 -56 35 -56 35 -56 35 -56 35 -56 35 -56 35 -56 35 -56 35

Observations of the Magnetic Force between Van Diemen Island and the Cape of Good Hope, by Lieut. Joseph Dayman, R.N.

Date.		Lat.		Lon	g.	Weights.	Angle deflecti	of	Thermo- meter.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity. Hobarton = 1.800.	Remarks.
1944	-							_						
1844. Dec.		-42°	50	149	01	grs.	10 4	3	71°	1	1.800	1		
Dec.	٠.			147		2				On shore.	1.800	}	1.800	Magnetic Observa- tory, Hobarton.
١,	6	-42		147		3	16 1		71	J		{		tory, Hobarton.
1	16.	-44		144		2	10 2		55	w. by s.	1.863	} •041	1.827	
١.		-44		144		3	15 3		55	w. by s.	1.873	₹.		
1 1	17.	-44		143		2	10 3		67	w. by s.	1.834	-041	1.815	
Ι.		-44		143		3	15 2		67	w. by s.	1.879	Į	-	
	18.	44		142		2	10 2		69	w. by s.	1.866	-041	1.818	
_		-44		142		3	15 4		70	w. by s.	1.851)		
	19.		34	139		3	15 1	- (63	s.w. by s.	1.901	—·05 3	1.848	
2	21.		24	137		2		9	69	w.	1.840	-037	1.828	
1	- 1	42		137		3		4	70	w.	1.889)	- 0.00	
2	23.	-41	46	133	26	2	10 3	2	58	N.	1.831	}020	1.846	
1	j	-41	46	133	26	3	15 1	8	57	N.	1.901)	1010	
2	28.	-40	05	128		2	10 0	5	63	n.w. by n.	1.912	}020	1.856	A long heavy swell.
l	1	 40	05	128		3	15 4	9	63	n.w. by n.	1.840	\[\]	1 000	long neavy swell.
3	30.	-39		124		2	10 3	8	65	n. by w.	1.814	$\frac{1}{2} - 020$	1.793	A long heave and?
1			25	124		3	16 0	4	65	м. by w.	1.813	-020	1.790	A long heavy swell.
3	31.	-38		123		2	10 2		62	N.N.W.	1.852	1 .000	1,700	A long bears
ĺ		-38		123		3	16 1		62	N.N.W.	1.786	} 020	1.799	A long heavy swell.
1845.	. 1	00						١ ١			•	,		
Jan.	1.	-38	21	122	46	2	10 4	9	71	n.w. by w.	1.783	1 .005	1.777	
ŀ	1	-38		122	46	3	15 5	9	72	n.w. by w.	1.822	-025	1.777	
1.	3.	-37		124		2	10 5		69	N.W.	1.767	1 .000	1.77	
ľ	- 1	-37		124		3	16 0		69	N.W.	1.815	\ \rightarrow \cdot \cdot 020	1.771	
ľ	6.	-36		118		2	11 1		67	N.N.W.	1.725	1 000		
		-36		118	57	3	16 4		67	N.N.W.	1.747	 }020	1.716	
· .	7.	-35		117		2	11 0			N.N.W. $\frac{1}{2}$ W.	1.743	1	7 500	
,	•		22	117		$\tilde{3}$	16 4			N.N.W. $\frac{1}{2}$ W.	1.742	} 020	1.722	
١,	11.	-36	. 1	116		2	10 5		68	s.s.w.	1.767	1		
1 1	• • •	-36		116		3		6	68	s.s.w.	1.773	} - •055	1.715	
,	16.	$-30 \\ -34$		112		2		24	66	N.W.	1.693	1		
1 1	10.	-34		112			17 0		66	N.W.	1.704	} • 012	1.686	
١,						3				1	1.623	1		
1 1	17.	-33		111		2	•	64	67	N.W. by W.		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	1.609	
Ι,		-33		111		3	17 5		67	N.w. by w.	1.629	{		
1	18.	-33	- 1	108		2		7	69	n.w. by w.	1.616	\ \ \017	1.603	
١ .	20	-33	- 1	108		3	17 5		69	n.w. by w.	1.624	ΙĮ		
1 2	90.		40	105		2	1	30	72	N.W. $\frac{1}{2}$ N.	1.546	·007	1.537	
1 ,	.	-29		105		3	1	8	72	N.W. $\frac{1}{2}$ N.	1.543	Ĭ,		
1 2	21.	-28		105		2	13 0		73	N.	1.484	-004	1.493	
۱ .	ا ء	-28		105		3	19 2	1	73	N.	1.510	Į.]
, ,	22.	-26				2	13 0		76	N.W.	1.483	}007	1.466	
l .	ا ء	-26		104		3	20 0		76	N.W.	1.462	ĮĮ.	-	(
1 2	23.		52	102		2	13 3		75	N.W.	1.418	}007	1.421	
l		-25		102		3	20 2		75	N.W.	1.439]		
2	24.	-24	50	101		2	13 3		76	N.W.	1.432	}006	1.415	
		-24		101		3	20 5		76	N.W.	1.410			
2	25.	-24		99		2	13 3		75	w.n.w.	1.435	}010	1.407	
ł		-24		99		3	21 0		75	w.n.w.	1.400	}		
2	27.	-23		95		2	14 2		78	w. by $n \cdot \frac{1}{3} n$.	1.350	\(\frac{1}{2}012	1.334	
1	1	-23	11	95	40	3	21 5	8	78	w. by n. ½ n.		17 - 012	1 301	
2	28.	-22	54	93	48	2	14 1	6	78	w. by n. $\frac{1}{2}$ n.		J012	1.337	
	1		54	93		3	22 0		79	w. by N. $\frac{1}{2}$ N.	1.338	7-012	1 991	
2	29.		19	91		2	15 0		77	W. 1 N.	1.291	1) .017	1.077	·
	-	-22		91		3	22 4		77	$W_{1} = \frac{1}{2} N_{1}$	1.297	\017	1.277	
3	30.	-22	17	89		2	14 5		80	$\hat{W} \cdot \frac{1}{2} N$.	1.296	15	1.000	
1		-22		89		3	22 2		81	$W \cdot \frac{1}{2} N \cdot$	1.314	-017	1.288	
	31.	-22		86		2	15 1		80	$W \cdot \frac{1}{2} N \cdot$	1.278	1	1.074	1
ľ		-22		86		$\tilde{3}$	22 3		80	$W \cdot \frac{1}{2} N$	1.304	-017	1.274	
		~~					1			2 2.0		J		

Lieut. Dayman's observations of the Magnetic Force. (Continued.)

Date.	Lat.	Long.	Weights.	Ángle of deflection.	Thermo- meter.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity. Hobarton = 1.800.	Remarks.
1845. Feb. 1.		84 17	grs.	15° 13′	81	$W \cdot \frac{1}{2} N \cdot$	1.275	}017	1.251	
. 3.		84 17 80 10	3 2	23 25 15 16	81 83	$\begin{array}{c c} W \cdot \frac{1}{2} N \cdot \\ W \cdot \frac{1}{4} N \cdot \end{array}$	1.262	} -:019	1.261	
4.		80 10 78 08	3 2	22 55 15 42	83 83	$W \cdot \frac{1}{4} N \cdot W \cdot \frac{3}{4} N \cdot$	1.288	$\left.\right\} - 015$	1.237	
5.		78 08 76 10	3 2	23 20 15 31	83 82	$W. \frac{3}{4} N.$ $W. \frac{3}{4} N.$	1.267 1.252	$\left\{015 \right\}$	1.236	,
6.		76 10 74 18	3 2	23 41 15 50	82 82	$W. \frac{3}{4} N.$ $W. \frac{3}{4} N.$	1·250 1·227	$\left.\right\}015$	1.216	
7.		74 18 72 20	3 2	23 58 15 49	82 81	$W \cdot \frac{3}{4} N \cdot W \cdot \frac{1}{2} N \cdot$	1·236 1·229	}016	1.211	
8.	$\begin{bmatrix} -22 & 33 \\ -22 & 41 \end{bmatrix}$	$\begin{array}{cc} 72 & 20 \\ 69 & 54 \end{array}$	3 2	24 11 15 38	81 ·	$\mathbf{W} \cdot \frac{1}{2} \mathbf{N} \cdot \mathbf{W}$	1·225 1·240	$\left. \begin{array}{c}018 \end{array} \right.$	1.215	
10.	$ \begin{array}{r rrr} -22 & 41 \\ -23 & 52 \end{array} $	69 54 64 59	3 2	24 13 15 58	81 84	w. w. ½ s.	1·223 1·217	$\left\{ \begin{array}{c} -013 \\022 \end{array} \right\}$	1.196	
	$ \begin{array}{rrr} -23 & 52 \\ -24 & 23 \end{array} $	$\begin{array}{c} 64 & 59 \\ 62 & 54 \end{array}$	3 2	24 20 16 13	84 83	$W. \frac{1}{2} S.$ $W. \frac{1}{2} S.$	1·218 1·199	$\begin{cases} -022 \\ -022 \end{cases}$	1.177	
12.	$ \begin{array}{r rrr} -24 & 23 \\ -24 & 50 \end{array} $	62 54 61 11	3 2	24 44 16 01	83 84	$W. \frac{1}{2} S.$ $W. \frac{1}{2} N.$	1·199 1·214	1		
	$ \begin{array}{r} -24 & 50 \\ -24 & 43 \end{array} $	61 11 59 46	3 2	24 22 16 17	84 85	$\begin{array}{c c} w \cdot \frac{1}{2} & N \cdot \\ w \cdot by & N \cdot \frac{1}{2} & N \cdot \end{array}$	1·216 1·194	}018	1.197	
	$ \begin{array}{r} -24 & 43 \\ -24 & 36 \end{array} $	$59 ext{ } 46 \\ 58 ext{ } 37$	3 2	24 47 16 23	85° 85	w. by N. $\frac{1}{2}$ N. w. by N. $\frac{1}{2}$ N.	1.197	}011	1.184	
	-24 36 $-25 13$	58 37 51 29	3 2	24 55 16 46	84 84	w. by N. $\frac{1}{2}$ N. w. $\frac{1}{2}$ N.	1·191 1·160	}011	1.178	
	$-25 13 \\ -25 42$	51 29 49 06	3 2	25 49 17 09	84 82	$W \cdot \frac{1}{2} N \cdot W \cdot$	1·152 1·135	-017	1.139	
20.	-25 42	49 06 42 18	3 2	26 16 17 43	81 81	W∙ W• ½ S•	1·133 1·100	-020	1.114	
21.	-28 15	42 18 39 06	3 2	26 44 17 46	81 81	$\mathbf{W} \cdot \frac{1}{2} \mathbf{S} \cdot \mathbf{W} \cdot$	1·116 1·097	$\Big \Big\} - \cdot 022$	1.086	
22.	-29 21	39 06 36 17	3 2	26 59 17 55	81 82	w. w. <u>1</u> n.	1·106 1·088	$\left \right\} - 020$	1.081	
24.	-30 10	36 17 32 21	3 2	27 07 18 29	82 83	$\begin{array}{c c} W \cdot \frac{1}{4} N \cdot \\ W \cdot \frac{1}{2} N \cdot \\ \end{array}$	1.101	018	1.076	•
25.	$-31\ 19$	32 21 29 34	3 2	28 01 18 59	83 82	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.068 1.029	016	1.046	
26.	-32 17	29 34	3 2	28 28 18 57	82 74	$\begin{array}{c c} & 3 & N \\ & \frac{3}{4} & N \\ & W \\ \end{array}$	1.052	$\begin{vmatrix} \\ \\014 \\ \\018 \end{vmatrix}$	1.026	
28.	-34 02	26 53	3 2	28 37 18 38	74 71	S.W. 1/2 W.	1.047	0 35	1.012	*
Mar. 1.	$ -34 \ 36$	25 23	3 2	28 22 19 27	71 79	S.W. $\frac{1}{2}$ W. W.N.W.	1.056	}030	1.021	
5.	-34 40	24 16	3 2	29 35 19 51	79 79 71	W.N.W. W.N.W. 1/2 N.	1.016 0.986	-007	1.004	
ı .	$\begin{bmatrix} -34 & 48 \\ -34 & 48 \end{bmatrix}$		3	30 46	70	$\begin{array}{c c} \text{N.W.} \ \overline{2} \ \text{N.} \\ \text{N.W.} \ \overline{\frac{1}{2}} \ \text{N.} \end{array}$	0.981	-000	0.984	

Observations of the Magnetic Declination, made on board Her Majesty's Ship Erebus, by Captain Sir James Clark Ross, between the Cape of Good Hope and Van Diemen Island.

Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Remarks.
1840. April 8.	$-35^{\circ}52^{\circ}$	18° 41	T. T. O.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	W. E.S.E. E.S.E.	-53 30	-2 13	$\begin{vmatrix} +30 & 33 \\ +29 & 39 \\ +29 & 37 \\ +29 & 37 \\ +30 & 08 \end{vmatrix}$	Compass C. H. used
10.	-36 11 -36 20	20 28	T. S. R. T.	+32 13 +30 44 +31 50 +31 39 +32 23	s.e. by e. s. s.e. $\frac{1}{2}$ s. s.e. $\frac{1}{2}$ s.	$egin{bmatrix} -53 & 40 \ -55 & 00 \end{bmatrix}$	$\begin{vmatrix} 0 & 00 \\ -1 & 45 \\ -1 & 48 \end{vmatrix}$	$egin{array}{cccccccccccccccccccccccccccccccccccc$	Į.
11.	-36 12 -36 21		T. S. O. T. T.	+32 02 $+30 03$ $+30 41$ $+29 56$ $+30 26$	s.s.e. $\frac{1}{2}$ e. s.w. s. by w. s. by w.		$\begin{vmatrix} +2 & 00 \\ +0 & 37 \\ +0 & 37 \end{vmatrix}$	$\begin{vmatrix} +30 & 39 \\ +32 & 03 \\ +31 & 18 \end{vmatrix}$	
	—36 28	21 15	S. T. R. T.	+30 20 $+30 17$ $+30 20$ $+30 14$ $+30 19$	S. S. S. S. $\frac{1}{2}$ E.	-55 30	0 00 0 00 0 00	$ \begin{vmatrix} +30 & 17 \\ +30 & 17 \\ +30 & 20 \\ +30 & 14 \\ +30 & 00 \end{vmatrix} +30 & 40$	
			O. S. T. R. T.	$ \begin{array}{rrrr} +31 & 00 \\ +30 & 41 \\ +31 & 11 \\ +31 & 29 \end{array} $	S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E. S.		$ \begin{vmatrix} -0 & 19 \\ -0 & 19 \\ -0 & 19 \\ 0 & 00 \end{vmatrix} $	$egin{array}{c c} +30 & 41 \\ +30 & 22 \\ +30 & 52 \\ +31 & 29 \\ \hline \end{array}$	
12.	—37 10	21 31	R. T. T. T.	+31 02 +30 01 +31 53 +32 09 +32 10	S. $\frac{1}{2}$ E. S. S. $\frac{1}{2}$ W. S. $\frac{1}{2}$ E. S. by E.		$\begin{vmatrix} 0 & 00 \\ + 0 & 19 \\ - 0 & 19 \end{vmatrix}$	+30 01	
			T. O. S. T.	+31 50 $+31 09$ $+31 16$ $+31 14$	s. by E. s. by E. s. by E. s. by E.	-56 00	$\begin{bmatrix} -0 & 38 \\ -0 & 38 \\ -0 & 38 \end{bmatrix}$	$\begin{vmatrix} +31 & 12 \\ +30 & 31 \\ +30 & 38 \\ +30 & 36 \\ +30 & 10 \end{vmatrix}$	
13.	-37 27 $-38 11$ $-38 20$	21 27	R. S. T. T.	+28 57 $+32 43 $ $+31 10 $ $+30 04 $ $+30 20$	s. by E. s.E. $\frac{1}{2}$ E. s.w. by w. s.w. s.w.	$\left.\begin{array}{c} \\ \\ \\ \end{array}\right\} -57 \ 30$	-2 16		
14. 15.	-39 55 $-41 00$ $-41 15$	22 01	T. T. S.	+30 20 $+29 51$ $+32 30$ $+31 20$	s.s.w. s.e. by s. s.e. by s.	$\left.\begin{array}{c} -59 & 30 \\ -59 & 40 \end{array}\right.$	$\begin{vmatrix} +1 & 18 \\ -2 & 04 \end{vmatrix}$	$\begin{vmatrix} +31 & 09 & +31 & 09 \\ +30 & 26 \\ +29 & 16 \end{vmatrix} +29 & 51$	1 .
16.	-41 24	24 32	T. T. S.	$+32 09 \\ +32 35 \\ +31 00$	S.S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ S. S.E. by S.	$\left \right _{-62\ 00}$	$\begin{bmatrix} -2 & 17 \\ -2 & 03 \end{bmatrix}$	$\begin{vmatrix} +30 & 23 \\ +30 & 18 \\ +28 & 57 \\ +20 & 50 \\ \end{vmatrix} +30 & 25$	
17.	-41 32 $-41 28$ $-41 50$		T. R. R. S.	+32 45 +32 41 +32 00 +31 48	S.S.E. \(\frac{1}{2}\) E. S.S.E. S.S.E. S.S.E.		$\begin{bmatrix} -1 & 24 \\ -1 & 24 \end{bmatrix}$	+30 39 +31 17 +30 36	
1,8.			T. T. S.	+34 43 +34 27 +34 43	S.S.E. S.S.E. S.S.E.		$\begin{vmatrix} -1 & 26 \\ -1 & 26 \\ -1 & 26 \end{vmatrix}$	$\begin{vmatrix} +33 & 17 \\ +33 & 01 \\ +33 & 17 \\ +33 & 37 \end{vmatrix}$	
25	$\begin{bmatrix} -43 & 24 \\ -46 & 31 \end{bmatrix}$		O. R. T. R.	+35 58 +33 58 +33 39 +35 44	s.s.e. s.s.e. s. by e. s.e.	$ \begin{vmatrix} 1 & 0 & 0 \\ -62 & 40 & 0 \\ -67 & 00 & 0 \end{vmatrix} $	$\begin{vmatrix} -1 & 26 \\ -0 & 45 \end{vmatrix}$	$egin{array}{c cccc} +34 & 32 \ +32 & 32 \ +32 & 54 \ +32 & 41 \ +32 & 41 \ \end{array} +32 & 41$	l
	$-46 \ 34$		T. T.	+31 44 +31 53	N.W. N.N.W.	$\left \begin{array}{c} -67 & 66 \\ -67 & 30 \end{array} \right $	+212	$\left \begin{array}{ccc} +33 & 16 \\ +33 & 56 \\ +33 & 00 \end{array} \right +33 \ 28$	1

Observations of Declination. (Continued.)

Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Remarks.
1840. April 30. May 1. 2.	-46 32	52 01 56 17 56 28	R. S. T. R. T.	$\begin{vmatrix} +37 & 06 \\ +36 & 34 \\ +33 & 48 \\ +33 & 34 \\ +32 & 21 \end{vmatrix}$	N. by E. ½ E. S.E. S.E. S.E. S.E.	$ \begin{cases} -6\mathring{7} & 30 \\ -67 & 30 \end{cases} $ $ \begin{cases} -67 & 50 \end{cases} $ $ \begin{cases} -68 & 30 \end{cases} $	+0 53 -3 07 -3 07 -3 07 -3 07 -3 15	$ \begin{vmatrix} +32 & 33 \\ +33 & 59 \end{vmatrix} + 33 & 16 \\ +33 & 27 \\ +30 & 41 \\ +30 & 27 \end{vmatrix} + 31 & 32 \\ +29 & 06 \\ +29 & 55 \end{vmatrix} + 29 & 00$	
	-47 18		R. R. R.	$\begin{vmatrix} +31 & 50 \\ +30 & 32 \\ +29 & 39 \\ +29 & 34 \end{vmatrix}$	s.e. by e. ½ e. s.e. by e. ½ e. s.e. by e. ½ e. s.e. by e. ½ e. s.e. by e. ½ e.	-72 30	-3 15 -4 41 -5 10	+25 38	
31. Aug. 2. 4.	$-47 34 \\ -47 45 \\ -47 40$	113 49	T. T. R.	$\begin{vmatrix} +16 & 39 \\ +17 & 58 \\ +15 & 26 \\ +15 & 11 \end{vmatrix}$	s.e. by $e. \frac{1}{2}e.$ e. by $s. \frac{1}{2}s.$ e. by $s. \frac{1}{2}s.$ e. $\frac{1}{2}s.$ e. $\frac{1}{2}s.$		-5 49 -5 51	+18 59 +11 29 + 9 34	
7.	—46 36	131 48	R. T. T. T. R. R. R. R. R.	+15 39 + 1 58 + 3 44 + 3 08 + 5 43 + 5 58 + 6 30 + 4 29	E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ N. E. by N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E.	-75 00	-5 35 -5 27 -5 35 -5 35 -5 43 -5 43 -5 43 -5 43	- 1 00	
	-46 13 -46 06	132 00 132 12	R.	$ \begin{vmatrix} + & 5 & 16 \\ + & 2 & 09 \\ + & 6 & 17 \\ + & 6 & 53 \\ + & 7 & 25 \\ - & 3 & 06 \end{vmatrix} $	E. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.	\right\}-75 00	-5 43 -5 35 -5 35 -5 35 -5 35 0 00	- 0 34	
10.	-44 23	141 11		- 4 19 - 3 12 - 3 12 - 4 01 - 3 39 - 4 24 - 2 01	E.N.E. E.N.E. E.N.E. E.N.E. E.N.E. E.N.E.	-73 00	—4 20		

The observers are distinguished by their initials as follows:-

R., Sir James Ross; S., Lieut. Sibbald; T., Mr. Tucker, Master; O., Mr. Oakley, Mate.

Observations of the Magnetic Inclination taken on board Her Majesty's Ship Erebus, by Captain Sir James Clark Ross, with Needle F. 1., between the Cape of Good Hope and Kerguelen Island.

	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Corrections.		·	·
Date.						Ship's attrac- tion.	Index.	Corrected Inclination.	Remarks.
-	$-3\overset{\circ}{5}$ $1\overset{\prime}{4}$		Direct.	$-5\overset{\circ}{4} \ 2\overset{\circ}{3} \\ -54 \ 30$	s. by E.	-04	-2.0	$\left. ight\} -54 32$	
8.	-35 48	18 47	Direct. S. Direct.		E.S.E. w. by s.	+23	-2.0	$\left \begin{array}{c} \\ \\ \end{array} \right = 54 \ 18$	
	-36 00		S. Direct. S.	$ \begin{vmatrix} -54 & 47 \\ -55 & 42 \\ -56 & 10 \end{vmatrix} $		+34	-2.0	igg igg -55 24	
	-36 07		Direct.	-55 49 $-55 51$	s.e. by s.	+02	-2.0	$\left.\begin{array}{c} -55 & 50 \end{array}\right.$	
11.	-36 29 ·	21 16	Direct. S. S.N. N.	$ \begin{array}{r} -55 & 30 \\ -55 & 36 \\ -55 & 26 \\ -55 & 14 \end{array} $	s.	-10	-2.0	$\left \begin{array}{c} -55 & 38 \end{array} \right $	
12.	-37 19	21 37	Direct. S. Direct.	$ \begin{vmatrix} -55 & 27 \\ -56 & 01 \\ -55 & 42 \end{vmatrix} $	s.	-10	-2.0		
			S. Direct.			-10	-20		-
	-38 11		Direct. S.	$-55 ext{ } 41 \\ -56 ext{ } 09$	w.s.w.	+22	-2.0	$\left.\right\} -55 35$	Much motion.
	-40 05		Direct.	$\begin{bmatrix} -56 & 27 \\ -56 & 19 \end{bmatrix}$	S.S.E.	-08	-2.0	$\left.\right\}$ -56 33	
	-40 29 $-41 24$		Direct. S. Direct.		s.e. by s.	-06	-2.0	$\left.\right\}$ -57 28	
4	_11 &1	20 00	S. S.N. N.	$ \begin{array}{r rrrr} -58 & 24 \\ -58 & 11 \\ -58 & 11 \end{array} $	Sille by Si	-08	-2.0	-58 21	
	-41 47		Direct. S.		S.S.E.	-15	-2.0	$\left \begin{array}{c} \\ \\ \end{array} \right = 58 43$	
18.	-43 02		Direct. S.	-59 01 $-59 20$	s.s.e.	-19	-2.0	$\left.\begin{array}{ c c c c c c c c c c c c c c c c c c c$	
	-43 07	28 43	S.N. N. Direct.			-20	-2.0	$\left \begin{array}{c} -59 & 37 \end{array} \right $	
	-44 19		Direct. S.	$ \begin{array}{r rrrr} -60 & 30 \\ -60 & 13 \end{array} $	s. by E.	-29	-2.0	$\left.\begin{array}{c} -60 & 52 \end{array}\right.$	
	-45 40		Direct.	$ \begin{array}{r rrrr} -61 & 41 \\ -62 & 01 \end{array} $	S.S.E.	-30	-2.0	$\left \right\} -62 \ 23$	
21.	-46 59		Direct. S.	$\begin{bmatrix} -63 & 28 \\ -63 & 32 \\ 62 & 50 \end{bmatrix}$	s.e. by s.	-28	-2.0	$\left \frac{1}{2} - 64 \ 00 \right $	-
22. 23.	-47 00 $-46 46$		Direct. S. Direct.		s.e. by s.	29	-2.0	$\left.\begin{array}{c} -64 & 30 \\ \end{array}\right.$	Much motion.
			S. Direct.		2.2. NJ 2.	-32	-2.0	-65 47	Very steady.
			Direct.	$\begin{vmatrix} -66 & 18 \\ -66 & 20 \end{vmatrix}$	S.E. ½ E.	-15	-2.0	$\left \begin{array}{c} \\ \end{array} \right -66 \ 36$	roly secany.
26.	-46 41	•	Direct.	$\begin{bmatrix} -67 & 00 \\ -67 & 06 \\ 67 & 21 \end{bmatrix}$	s.e. by s.	-36	-2.0	$\left.\right\} -67 \ 41$	
28.	-46 28	əz 31	Direct. S.	$\begin{vmatrix} -67 & 31 \\ -67 & 32 \end{vmatrix}$	W.S.W.	+03	-2.0	$\left \right\} -67 30$	

						Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1840. Apr. 29.			Direct.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ľ		-2.0	$\left67 29 \right $	
	-46 17 $-46 25$		Direct. S. Direct.	$ \begin{array}{r rrr} -66 & 20 \\ -66 & 27 \\ -66 & 26 \end{array} $	s.s.w. s. by E. ½ E.	-45	-2.0	$\left.\right\} -67 \ 10$	
	23 %		S. S.N.	$ \begin{array}{r rrrr} -66 & 39 \\ -66 & 40 \end{array} $		-47	-2.0	-67 30	
2.	—46 57	55 34	N. Direct. S.	$\begin{vmatrix} -67 & 00 \\ -67 & 37 \\ -67 & 51 \end{vmatrix}$	S.E.	-26	-2.0	$\left. \begin{array}{c} 1 \\ -68 \\ 12 \end{array} \right $	
3.	-47 19	59 10	Direct. S. S.N. N.		S.E.	-27	-2.0	$\left. \begin{array}{c} -68 & 42 \end{array} \right $	
4.	-47 40	62 25	Direct.	$\begin{bmatrix} -69 & 09 \\ -69 & 13 \\ -69 & 02 \end{bmatrix}$	S.E.	-28	-2.0	$\left.\right\} - 69 \ 37$	
	-48 36		Direct.		N.N.W.	+69	-2.0	\rightarrow -70 12	
	-48 36		Direct.	$\begin{vmatrix} -69 & 12 \\ -69 & 25 \\ 60 & 10 \end{vmatrix}$	s.w. by s.	-42	-2.0		
	-48 24	_	Direct.	-69 28	s.w.byw. $\frac{1}{2}$ w.	-08	-2.0	$\left.\right\} -69 \ 33$	
12.	-48 40	08 58	Direct. S. Direct. S.	$ \begin{array}{rrrrr} -71 & 47 \\ -72 & 03 \\ -69 & 46 \\ -69 & 59 \end{array} $	s.w.byw.½w.	-72 -08	-2·0 -2·0		

Abstract of Observations of the Magnetic Force between the Cape of Good Hope and Kerguelen Island, made in Her Majesty's Ships Erebus and Terror in 1840*.

Position.		Intensity.		Posi	tion.	Intensity.	
Lat.	Long.	Cape = 0.981.	Cape =1.000.	Lat.	Long.	Cape = 0.981.	Cape = 1.000.
-34 11 -37 44 -35 14 -36 04 -37 16 -36 16 -36 11 -35 48 -38 47 -36 35 -38 58 -40 05 -40 45 -38 13 -42 40 -41 24 -42 56 -40 29 -41 58 -44 28 -46 41	18 26 16 36 18 27 19 19 17 24 20 04 18 25 20 42 18 47 17 00 21 20 17 26 20 38 19 20 21 30 22 02 25 00 23 12 22 22 26 38 24 55 29 00	0.981 0.983 0.984 0.988 0.989 0.995 0.995 0.997 0.998 0.999 1.010 1.020 1.021 1.036 1.045 1.058 1.063 1.073 1.079 1.088 1.096 1.122	1.000† 1.003 1.004 1.008 1.009 1.015 1.016 1.017 1.018 1.019 1.030 1.040 1.041 1.057 1.066 1.079 1.084 1.100 1.110 1.118 1.114	-43 07 -47 00 -45 44 -46 45 -47 00 -46 46 -47 50 -47 01 -46 41 -46 28 -46 29 -46 25 -46 57 -46 18 -47 19 -47 41 -48 41 -48 39 -48 36 -48 36	28 43 38 48 34 16 40 05 37 14 43 48 42 41 45 20 46 10 50 52 52 43 52 26 52 01 55 39 52 04 59 10 62 59 68 54 68 57 69 07 69 21	1·134 1·170 1·171 1·183 1·186 1·230 1·232 1·261 1·269 1·277 1·288 1·314 1·323 1·326 1·328 1·377 1·459 1·465 1·471 1·488 1·489 1·490	1·157 1·193 1·194 1·206 1·209 1·255 1·257 1·286 1·294 1·302 1·316 1·340 1·349 1·352 1·354 1·404 1·487 1·493 1·499 1·517 1·518 1·520
$-46 00 \\ -44 19$	26 12 31 06	1·128 1·131	1·150 1·154	-48 30	69 52	1.497	1.527

^{*} Philosophical Transactions, 1842, p. 41. † On shore in Simon's Bay. ‡ On shore at Kerguelen Island.